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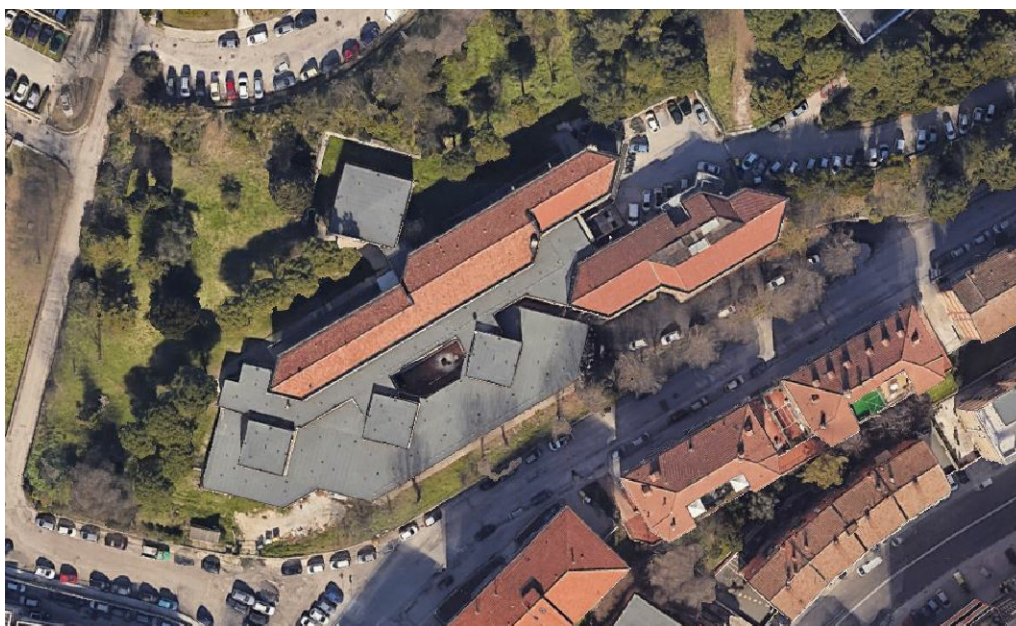
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Progetto Esecutivo dei Lavori di Miglioramento Sismico del Liceo Artistico "Mannucci" Via Michelangelo Buonarroti 12, ANCONA (AN) "Finanziato dall'Unione Europea - NextGenerationUE"

MISSIONE 4: ISTRUZIONE E RICERCA

Componente 1 - Potenziamento dell'offerta dei servizi: dagli asili nido alle università
Investimento 3.3: Piano di messa in sicurezza e riqualificazione dell'edilizia scolastica

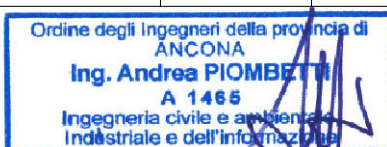


ELABORATO

RELAZIONE GENERALE ILLUSTRATIVA IN VARIANTE

No. DOC	Fase Progetto	Tipo	Ext.	Dimensioni foglio
b)	VARIANTE SUPPLETIVA	doc	doc	A4

REV.	DESCRIZIONE REVISIONE	DATA	AUTORE	VERIFICA	APPROVAZIONE
R00	Prima Emissione	28/10/2025	AM. Camilletti	A. Piombetti	A. Piombetti
R01					
R02					



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RELAZIONE GENERALE ILLUSTRATIVA IN VARIANTE

1. DESCRIZIONE DEGLI INTERVENTI IN VARIANTE

La presente relazione è riferita alla VARIANTE IN CORSO D'OPERA dell'intervento di ***Lavori di Miglioramento Sismico della scuola Liceo Artistico Edgardo Mannucci*** sita in Via Michelangelo Buonarroti n. 12 nel comune di Ancona.

L'intervento è finanziato con i fondi di cui al Piano Nazionale di Ripresa e Resilienza (PNRR) ed è individuato fra quelli di cui alla

Missione 4: ISTRUZIONE E RICERCA,

Componente 1 – Potenziamento dell'offerta dei servizi di istruzione: dagli asili nido alle Università
Investimento 3.3. - Piano di messa in sicurezza e riqualificazione dell'edilizia scolastica.

I lavori previsti nel progetto esecutivo sono prossimi all'ultimazione, essendo già stato eseguito il 96% circa dei lavori previsti. Sostanzialmente, resta da realizzare il distacco tra il corpo F e la segreteria oltre ad alcune opere di finitura e il ripristino delle aree di cantiere alla conformazione originaria.

L'area in cui sorge il liceo Mannucci presenta una forte pendenza e risulta intensamente alberata. Per l'esecuzione dei lavori si sono rese necessarie importanti sistemazioni del terreno per consentire l'accesso ai mezzi d'opera e la stabilizzazione dei percorsi di cantiere con materiali aridi e compatti. I lavori hanno cercato di conservare il più possibile le alberature preesistenti, limitando l'abbattimento anche rispetto a quanto previsto in progetto.

La conservazione dell'attuale conformazione dell'area cortiliva della scuola permetterebbe la fruizione delle aree esterne da parte di alcuni locali/laboratori consentendone uno sfogo all'aperto, che altrimenti sarebbe precluso considerando l'acclività del terreno. Anche l'esodo di alcune porzioni dell'edificio migliorerebbe e consentirebbe di sfruttare uno spazio esterno come aula verde, zona di incontro e attività didattiche comuni all'aperto. Infine, ma non meno importante, le stesse aree a verde che sono significative in termini di estensione, potranno essere mantenute con maggior facilità e quindi conservate ad un livello qualitativo superiore rispetto a quanto fatto nel passato.

Nella presente variante vengono progettate le opere necessarie alla fruizione in sicurezza degli spazi esterni mediante adeguate opere di sostegno, recinzioni e parapetti oltre alle necessarie pavimentazioni di alcune parti dei percorsi.

Le aree esterne che ora si intendono utilizzare erano precedentemente zone a verde. Ciò comporta un aggravio dei deflussi meteorici per cui si rende necessario, a seguito del calcolo dell'invarianza idraulica, la predisposizione di una o più vasche di laminazione.

2. DIMENSIONAMENTO DELLA VASCA DI LAMINAZIONE -PARTICOLARE 9

Con riferimento alla tavola grafica "TAV. A", le aree che vengono interessate dai lavori di sistemazione esterna e che quindi soggiacciono all'invarianza idraulica sono riassunti nei seguenti righi:

Pavimentazioni in cemento o comunque altamente impermeabili	= 141 m ²
Pavimentazioni in stabilizzato e ghiaietto	= 715 m ²
Prati e orti interessati dalle sistemazioni	= 300 m ²

Per un totale di superficie interessata di 1156 m².

Nella tabella seguente si riporta il calcolo per il dimensionamento della vasca di laminazione e della condotta di deflusso.

1) INDIVIDUAZIONE DELLE SUPERFICI SCOLANTI AFFERENTI ALLA VASC.			2) CALCOLO DELLA PORTATA AFFLUENTE		
Tetti normali in tegole	0.00	m ²	$\varphi = 0.90$	Q = 0.00	l/s
Pavimentazioni in asfalto e cubetti di porfido legati con cemento	141.00	m ²	$\varphi = 0.85$	Q = 1.44	l/s
Pavimentazioni in cubetti di porfido o formelle legati con sabbia	0.00	m ²	$\varphi = 0.70$	Q = 0.00	l/s
Pavimentazioni in macadam	715.00	m ²	$\varphi = 0.50$	Q = 4.29	l/s
Prati e orti (solo qualora effettivamente conferiti nella vasca)	300.00	m ²	$\varphi = 0.17$	Q = 0.61	l/s
TOTALE	1156.00	m²		TOTALE	6.34 l/s
3) SCARICO CONCESSO ALL'UTENTE PRIVATO					
Qscarico	2.31	l/s			
Portata da laminare	4.03	l/s			
4) CALCOLO DEL VOLUME DELLA VASCA DI LAMINAZIONI					
V vasca =	14501.52 l	14.50	m ³		
5) DIMENSIONAMENTO DEL TUBO DI CONTROLLO DI FLUSSO (scarico della vasca di laminazione)					
$A_{sez.tubo} = \frac{Q}{0.6 \cdot \sqrt{2 \cdot 9.81 \cdot h}}$	0.6	parametro idraulico fisso (adimensionale)			
		h { - tirante utile nella vasca di laminazione espresso in m. (vedi file Istruzioni", punto 3.5) - oppure, nel caso di vasca di laminazione dotata di pompa di sollevamento, tirante utile nel pozzetto con scarico di fondo tarato, espresso in m. (vedi file Istruzioni", punto 3.5.ter)			
		Q	Qscarico calcolata al punto 3)		
h =		1.00	m		
A _{sez.tubo} =		0.000869936	m ²		
Diametro = $2 \cdot \sqrt{A_{sez.tubo}/\pi}$		3.328	cm		

La vasca dovrà avere un volume di circa 15 m³ e una tubazione di deflusso di circa 33 mm di diametro che garantirà un deflusso posticipato del volume di acqua laminato dall'evento di pioggia. La vasca sarà completamente interrata e protetta superficialmente da un coperchio carrabile.

La vasca potrà essere costituita da una serie di contenitori di qualsiasi forma la cui capacità totale dovrà essere non inferiore ai 15 m³ previsti.

3. CALCOLO DELLE RINGHIERE IN ACCIAIO – ALLEGATO A – PARTICOLARE 6

Per la protezione dei nuovi percorsi in variante sono previste delle ringhiere in metallo.

Le ringhiere che costituiscono una semplice delimitazione dell'area e pertanto il loro superamento non costituisce un pericolo per l'incolumità delle persone, sono previste in orsogrill o in legno. Diversamente, le ringhiere che fungono da barriera e protezione contro la caduta dall'alto sono previste in acciaio e nel seguito si riporta il calcolo e il dimensionamento della ringhiera.

Il calcolo è fatto per un tratto rettilineo standard che prevede i fissaggi a terra su calcestruzzo di cemento.

La ringhiera è costituita da montanti in tubolare di acciaio 60x60x6 mm collegati in sommità da un corrimano tubo rettangolare 60x50x5 mm che rende solidali tra loro i montanti. Il corrimano è posto ad una quota dal calpestio di 110 cm. I montanti sono posti ad interasse di 1 m e il pannello interno, tra un montante e il successivo è composto da due piatti pieni rettangolari 50x10 mm che portano dei tondini lisci di diametro 10 mm, posti ad interasse non superiore a 10 cm.

La balaustra è illustrata nella tavola grafica TAV. B.

Nell' **allegato A**, si riporta il calcolo della ringhiera.

L'acciaio impiegato è S235.

Le ringhiere di separazione, realizzate con orsogrill o in legno sono fondate su un cordolo in c.a. le cui caratteristiche sono riportate nel **particolare 1 della TAV. B**.

4. CALCOLO DEL MURO A PROTEZIONE DEL CAMMINAMENTO PEDONALE ~ ALLEGATO B PARTICOLARE 3

In progetto è previsto un camminamento che ripristina un collegamento esterno che è stato demolito per consentire la costruzione dei primi 4 controventi denominati da n° 1 a n° 4.

Questo nuovo camminamento, già realizzato, è fondato su pali ed è costituito da una soletta in c.a. di 25 cm di spessore minimo.

Il progetto prevedeva l'espanto di tutte le alberature a monte del camminamento e la riprofilatura del terreno secondo un angolo stabile di natural pendio, rimuovendo la strada di cantiere di monte, rigenerando l'originario andamento del terreno.

Con la variante si prevede di mantenere la strada di cantiere a monte del camminamento, che consente di collegare le uscite del corpo H con l'ingresso secondario e con il nuovo accesso su strada, mantenere le alberature superstiti e soprattutto mantenere l'attuale scarpata creata con la costruzione del camminamento.

È dunque necessario realizzare un muro in c.a. che permetta di mantenere in essere l'attuale scarpata e consolidi il piede delle alberature superstiti. Questo nuovo muro si ancora sul camminamento realizzato su pali, costituito dalla soletta in c.a. di 25 cm di spessore che si poggia sui pali disposti a quinconce.

Si prevede di realizzare una serie di ancoraggi chimici e impostare il nuovo paramento verticale con uno spessore di 30 cm sulla soletta del camminamento.

Il getto verrà realizzato contro terra, pertanto il terreno in posto non subirà allentamenti.

Nel calcolo della spinta potrà essere considerato il valore della spinta attiva di un terreno granulare.

Nel calcolo sarà considerato lo spessore nominale del muro di 30 cm, quando nella realtà sarà maggiore in considerazione dell'andamento attuale della scarpata esistente.

Il calcolo del muro è riportato nell'Allegato B, mentre il muro e le caratteristiche del muro e le armature sono riportate nel particolare 3 della TAV. B.

5. AREA ESTERNA AL CORPO H – TAV. A

Esternamente al corpo H è stato realizzato un passaggio di cantiere con l'apporto di materiale granulare che ha consentito il passaggio dei pesanti mezzi di cantiere per servire gli interventi previsti e necessari per la realizzazione dei controventi denominati da n° 5 a n° 9.

Si intende mantenere questo spazio migliorando la finitura con un pavimento a cemento spazzolato o finitura al quarzo. Questa area potrà diventare un'aula all'aperto considerando che nel corpo H c'è un'aula da disegno.

Si prevede dunque la realizzazione di una soletta in c.a. con una canaletta di bordo che possa raccogliere le acque meteoriche che andranno convogliate, mediante una nuova linea fognaria, in fognatura, dopo essere stata indirizzata nella vasca di laminazione prevista.

La finitura del pavimento cementizio sarà del tipo "*spazzolato o a finitura al quarzo*" come quella già realizzata nel camminamento o nel piazzale antistante i laboratori.

6. RIPRISTINO DELLA PARTE ALTA DEL MURO DI SOSTEGNO A MONTE DEL CORPO H – PARTICOLARE 2

Esternamente al corpo H, l'area esterna di cui al punto precedente è presidiata da un muro di sostegno di notevole altezza. La parte alta di questo muro in realtà è un riporto in muratura posto sopra il vero muro di sostegno che è realizzato in c.a..

Il muro di sostegno non presenta lesioni, fuori piombo o altri segni. Appare dunque stabile e adeguato alla funzione che svolge.

Il rialzo in muratura presenta invece notevoli lesioni e distacchi. Questa parte dovrà essere rimossa per non costituire pericolo alla permanenza degli utenti della scuola nell'area esterna al corpo H.

Si prevede dunque la rimozione del sopralzo in muratura e la realizzazione di un fosso di guardia a monte e del muro di sostegno (vedi particolare 2 – TAV. B), da realizzarsi in c.a..

La funzione di questo canale di guardia è principalmente quello di regimare le acque di ruscellamento che percorrono il versante, ma al contempo determina una protezione e sostegno del terreno di monte. L'ancoraggio del canale di guardia verrà realizzato in testa al muro esistente e verrà fondato sul terreno a tergo del muro esistente. La sua presenza risulta stabilizzante per la rotazione di ribaltamento del muro esistente a seguito della spinta del terreno.

La stabilità allo scorrimento del muro esistente è garantita dalla presenza di cordoli di collegamento che uniscono la fondazione del muro di sostegno con il corpo H.

In sintesi, la realizzazione del canale di guardia risulta stabilizzante per il muro esistente in c.a..

L'altezza indicata nell'elaborato grafico è da considerarsi come altezza massima.

7. MURETTI CONTROTERRA A PROTEZIONE DEI CONTROVENTI DA N° 5 A N° 9

PARTICOLARE 4

I 5 controventi denominati da 5 a 9 insistono su una parte del versante particolarmente ripido. È dunque necessario proteggere il piede dei controventi mediante una piccola opera in c.a. che eviti che il terreno possa scivolare verso il piede dei controventi e insidiare gli ancoraggi degli stessi.

Questi muretti avranno una forma a “C”, un’altezza di 150 cm e saranno ancorati ai plinti dei controventi. Lo spessore sarà di 25 cm. Gli ancoraggi saranno realizzati con ancoraggi chimici e barre in acciaio B450C diametro 14 mm. La dimensione ridotta in altezza, la conformazione in pianta e soprattutto la funzione svolta consente di astenersi dal calcolo statico.

8. INGRESSO CARRABILE DA VIA G. VERDI – PARTICOLARI 7 E 8 ~ TAV. B

Attualmente il cantiere è alimentato da un ingresso carrabile posto lungo via G. Verdi, in prossimità dell’ingresso della Regione.

È volontà dell’Amministrazione mantenere tale ingresso carrabile che sarà costituito da un cancello ad ante, sorretto lateralmente da due colonne in acciaio fissate ad un muro di recinzione in c.a..

Il muro di recinzione verrà realizzato all’interno della proprietà per determinare lungo via Verdi una piazzola di sosta che consentirà la sosta del mezzo in ingresso durante l’apertura del cancello senza ostruire il transito lungo via Verdi.

Il muretto in c.a. che si andrà a realizzare avrà una sua fondazione superficiale in c.a. e sarà sormontato da una recinzione in orsogril (particolari 7-8).

Lungo via G. Verdi, l’area cortiliva della scuola è delimitata da una recinzione con rete metallica a rombo, plastificata, che in vari punti è divelta. Si prevede la sostituzione e il ripristino della continuità della recinzione lungo tutta via G. Verdi.

9. ALLUNGAMENTO DI DUE FINESTRE ESISTENTI -PARTICOLARE 5

Al piano ammezzato, nell’aula 21B sono esistenti due finestre alte che aprono verso il cavedio, oltre ad una porta che consente l’uscita sul cavedio stesso.

L’intervento in variante consiste nell’allungare dette finestre mantenendo la larghezza attuale ma aumentando la loro altezza fino a raggiungere un parapetto di 1 m da terra.

Questa modifica viene realizzata mediante il taglio di precisione della parete in c.a. esistente e l’installazione di due nuovi infissi.

La modifica di queste due aperture non cambia in modo apprezzabile la rigidezza della parete e non ne riduce la resistenza. Infatti, la rigidezza della parete è data dalla somma delle rigidezze dei maschi murari che non vengono modificati e quindi essa non cambia.

Per quanto attiene la resistenza essa subisce una modifica che non è significativa.

La deformabilità della parete non viene ridotta dall'intervento.

Pertanto, non si prevedono interventi di natura strutturale.

10. REDAZIONE COMPUTO METRICO DI VARIANTE

Il *computo metrico estimativo* di variante è stato redatto ricavando le misurazioni dagli elaborati di variante. Tutti i prezzi delle singole lavorazioni utilizzati per la quantificazione economica dell'intervento sono stati desunti o dai prezzi di appalto o dai sottoelencati prezzi al fine di avere un corretto valore di costruzione dell'opera:

ELENCO PREZZI MARCHE 2022/1 – Aggiornamento infrannuale

Approvato con D.G.R. n. 1001 del 01/08/2022. Contiene capitolo prezzi sicurezza, costo della sicurezza, costo della manodopera e capitolo relativo ai prodotti conformi ai Criteri Ambientali Minimi di cui al DM 11.10.2017. Contiene aggiornamento tabella procedura collaborativa

11. ONERI SPECIALI DELLA SICUREZZA

In considerazione dei lavori in più da eseguirsi e previsti nella presente variante, è stato aggiornato il computo dei costi aggiuntivi della sicurezza.

12. INDICAZIONI SUL CRONOPROGRAMMA DEI LAVORI

Per quanto attiene la programmazione temporale dei lavori, considerando che i lavori di appalto sono prossimi al termine, i lavori, compresi quelli di variante dovranno essere ultimati entro il **31 gennaio 2026**.

13. CONCLUSIONI

La presente variante contempla tutte le richieste dell'Amministrazione e mantiene il costo della variante, comprensivo delle spese tecniche, entro il 15% dell'appalto.

Il direttore dei lavori
Dott. Ing. Andrea Piombetti

ALLEGATO A

CALCOLO RINGHIERA IN ACCIAIO

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1. – RELAZIONE DI CALCOLO

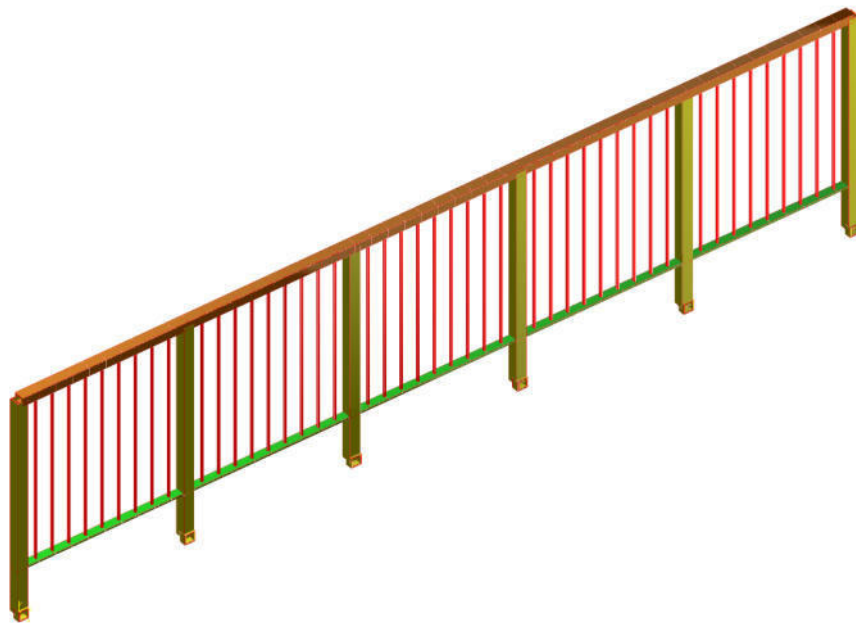
La presente relazione è riferita alla verifica strutturale di una balaustra in acciaio che funge da parapetto lungo un percorso a terra che costeggia una zona a quota più bassa del percorso.

Le caratteristiche geometriche sono descritte nell'elaborato grafico TAV. B.

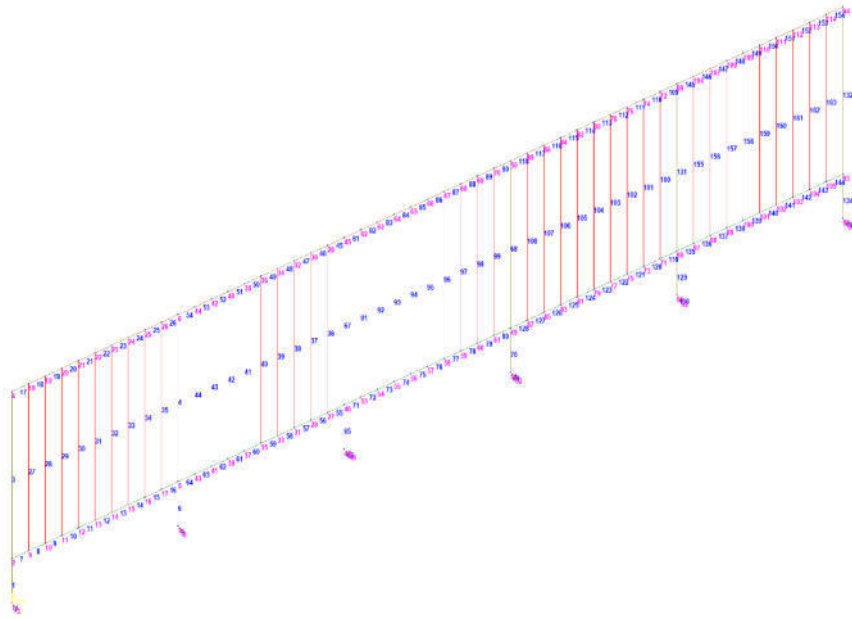
I carichi considerati sono il peso proprio ed i permanenti.

Per quanto attiene al carico accidentale, con riferimento alla tabella Tab.3.1.II – *Valori dei sovraccarichi per le diverse categorie d'uso delle costruzioni*, per gli ambienti suscettibili di affollamento dove i carichi orizzontali lineari H_k sono assunti pari a $2,0 \text{ kN/ml} = 2,0 \text{ daN/cm}$.

Per il calcolo della balaustra è stato effettuato una modellazione parziale ma significativa della struttura che si riporta nella slide seguente.



Vista assonometria - **Modello solido balaustra**



NUMERAZIONE NODI - ELEMENTI

Al piede dei montanti, c'è il collegamento in orizzontale con la piastra di fissaggio. La piastra è simulata come un incastro perfetto.

La piastra è a sua volta fissata alla soletta in c.a. mediante 4 ancoraggi chimici con barre di diametro 16 mm, due superiori e uno inferiore.

Si effettua unicamente la verifica statica delle membrature.

Per quanto non specificato si rimanda agli elaborati grafici allegati.

2. COMBINAZIONI DELLE AZIONI E SCENARI DI CONTINGENZA (P.TO 2.5.3 D.M. 17-01-18)

Le combinazioni di calcolo considerate sono quelle previste dal D.M. 17.01.2018 per i vari stati limite e per le varie azioni e tipologie costruttive.

In particolare :

Per gli SLU:

$$F_d = \gamma_g G_k + \gamma_p P_k + \gamma_q \cdot \left[Q_{1k} + \sum_{i=2}^{i=n} (\psi_{0i} Q_{ik}) \right]$$

Per gli SLE

combinazioni rare:

$$F_d = G_k + P_k + Q_{1k} + \sum_{i=2}^{i=n} (\psi_{0i} Q_{ik})$$

combinazioni frequenti:

$$F_d = G_k + P_k + \psi_{11} Q_{1k} + \sum_{i=2}^{i=n} (\psi_{2i} Q_{ik})$$

combinazioni quasi permanenti:

$$F_d = G_k + P_k + \sum_{i=1}^{i=n} (\psi_{2i} Q_{ik})$$

Dove i coefficienti parziali inglobano gli eventuali coefficienti di modello.

Per le combinazioni sismiche per gli SLU ed SLD:

$$\gamma_I \cdot E + G_k + P_k + \sum (\psi_{2i} \cdot Q_{ki})$$

Dalla tabella 2.5.I prospetto1 del **D.M. 17.01.2018** si ricavano i coefficienti ψ^i da considerare , visto che la destinazione d'uso della struttura è quella per la civile abitazione si ha:

Azione	ψ_0	ψ_1	ψ_2
A - Abitazione	0.7	0.5	0.3
H - Coperture	0.0	0.0	0.0
Vento	0.6	0.2	0.0
Neve (a quota < 1000 m)	0.5	0.2	0
Variazione Termica	0.6	0.5	0

I coefficienti parziali di sicurezza per le verifiche SLU sono:

	Azioni Permanenti	Azioni Variabili
	γ_g	γ_q
Effetto sfavorevole	1.3	1.5

Nel seguito si riporta le schermate di input relativa alla determinazione delle combinazioni .



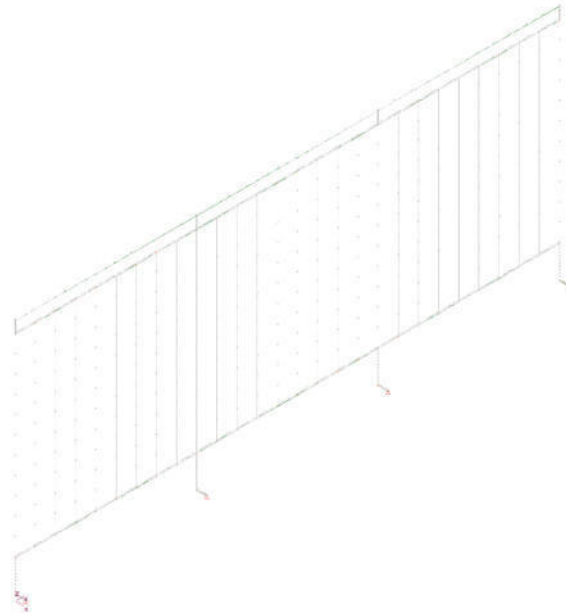
Combinazione SLU

Sono state inoltre considerate le combinazioni dello SLD.

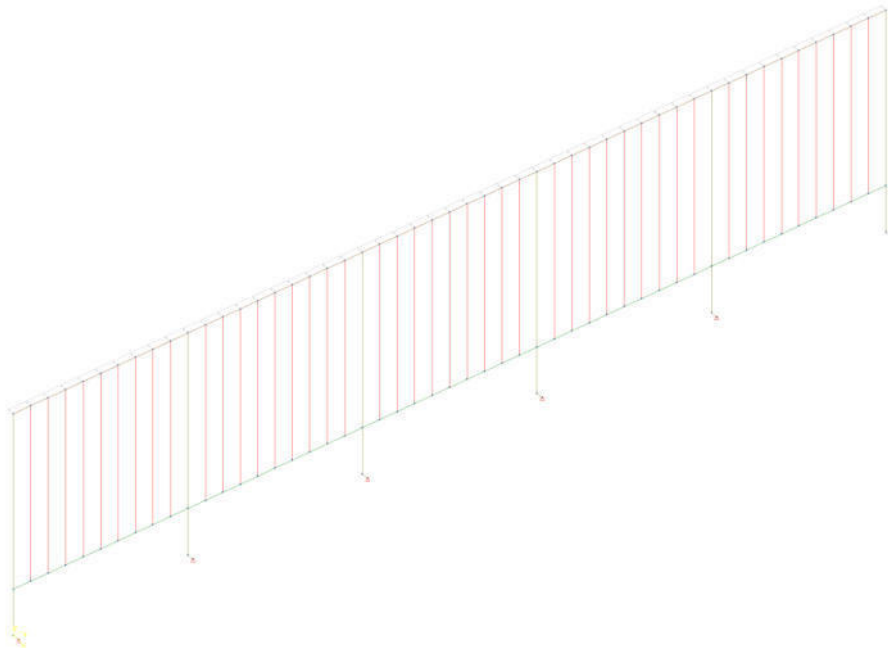
3. CONDIZIONE DI CARICO ELEMENTARE – CASI DI CARICO

L'applicazione dei carichi viene effettuata mediante l'inserimento di carichi di carico elementari (casi di carico) che saranno poi combinati secondo le combinazioni statiche e sismiche viste precedentemente.

Nel seguito si riportano le schermate dei casi di carico elementari



Caso di carico 1 – peso proprio strutture



Caso di carico 3 – carichi variabili (accidentale)

4. MISURA DI SICUREZZA – VERIFICHE GLOBALI

Il metodo di verifica della sicurezza adottato è quello degli Stati Limite (SL) che prevede due insiemi di verifiche rispettivamente per gli stati limite ultimi SLU (SLV) e gli stati limite di esercizio SLE (SLD).

La sicurezza è quindi garantita progettando i vari elementi resistenti in modo da assicurare che la loro resistenza di calcolo sia sempre maggiore della corrispondente domanda in termini di azioni di calcolo.

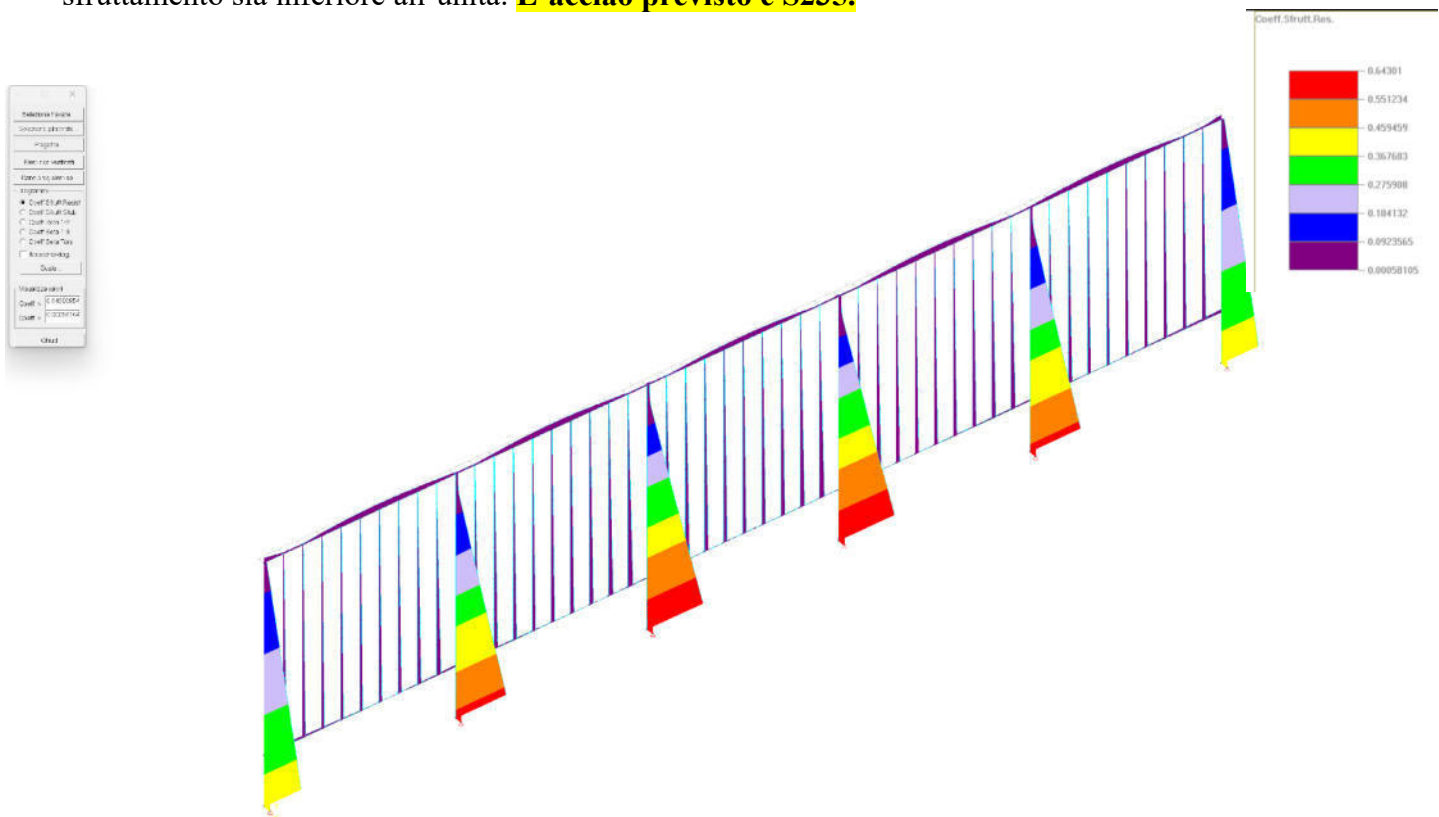
Per ogni stato limite deve essere rispettata la condizione:

$$E_d < R_d$$

Dove E_d è il valore di progetto dell'azione mentre R_d è il valore di progetto della resistenza.

Per la determinazione del modello e dei relativi coefficienti è stato seguito l'Approccio 2.

Nelle slides seguenti sono riportati i coefficienti di verifica delle singole membrature che compongono le due strutture. La verifica allo SLU è da ritenersi soddisfatta qualora il coefficiente di sfruttamento sia inferiore all'unità. **L'acciaio previsto è S235.**



Verifica Coefficiente di sfruttamento del materiale soddisfatta $0,64 \leq 1$

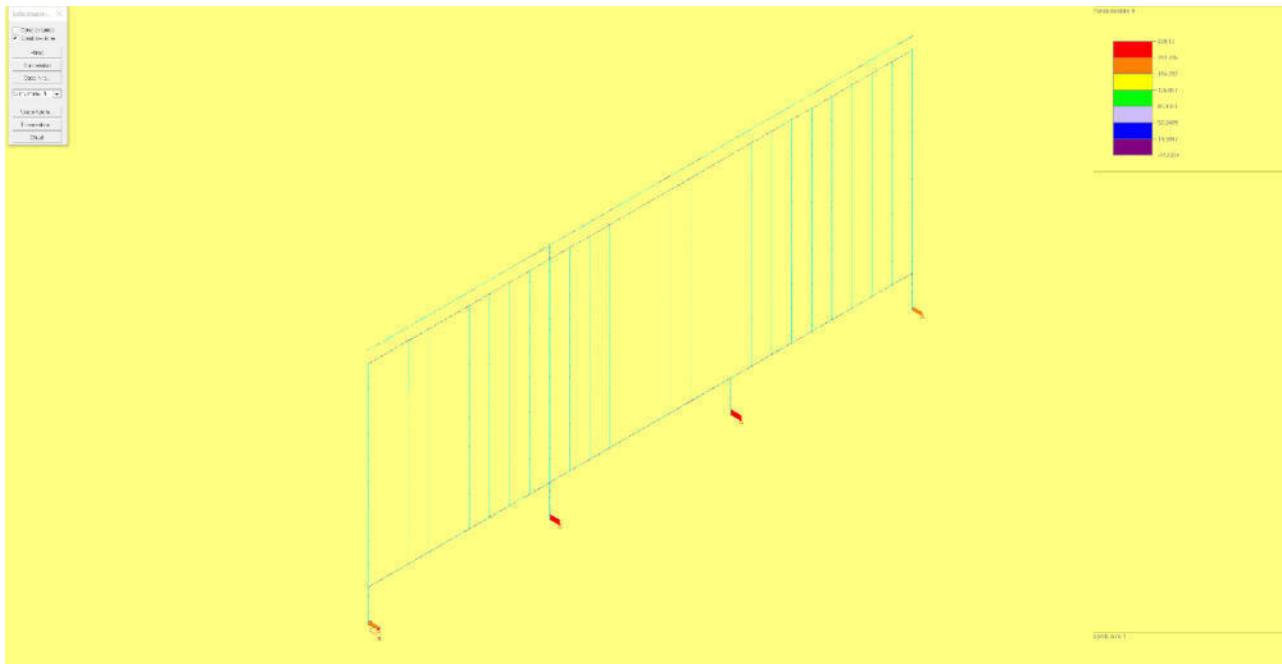
5. MISURA DELLA SICUREZZA – VERIFICHE LOCALI

Nel seguito si riportano le verifiche dei collegamenti interni tra i vari elementi che compongono la struttura e dei vincoli esterni.

Tutta la balaustra è saldata. Le uniche verifiche che si effettuano nel seguito sono le seguenti:

A.) Verifica dei bulloni di fissaggio della piastra al supporto.

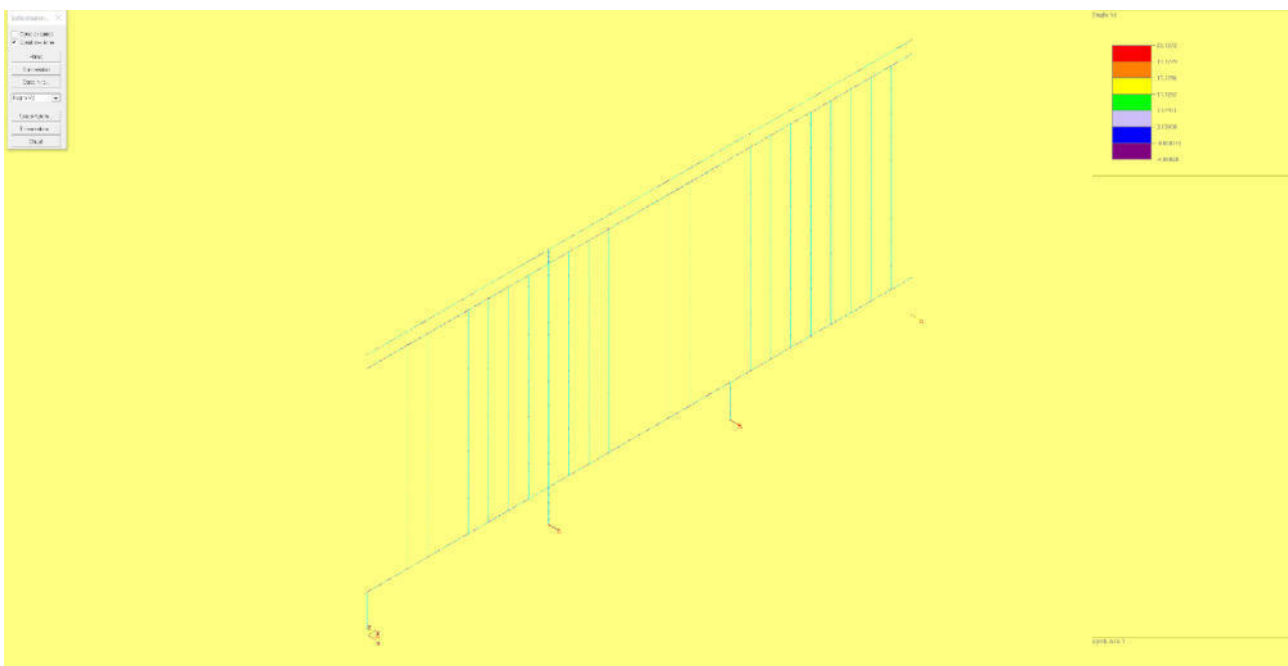
Nel seguito si riportano le slide delle sollecitazioni inerenti la combinazione di carico più gravosa allo stato limite ultimo (comb. 1) per le verifiche locali in condizioni statiche.



SOLLECITAZIONE ASSIALE (N - daN) COMB 1

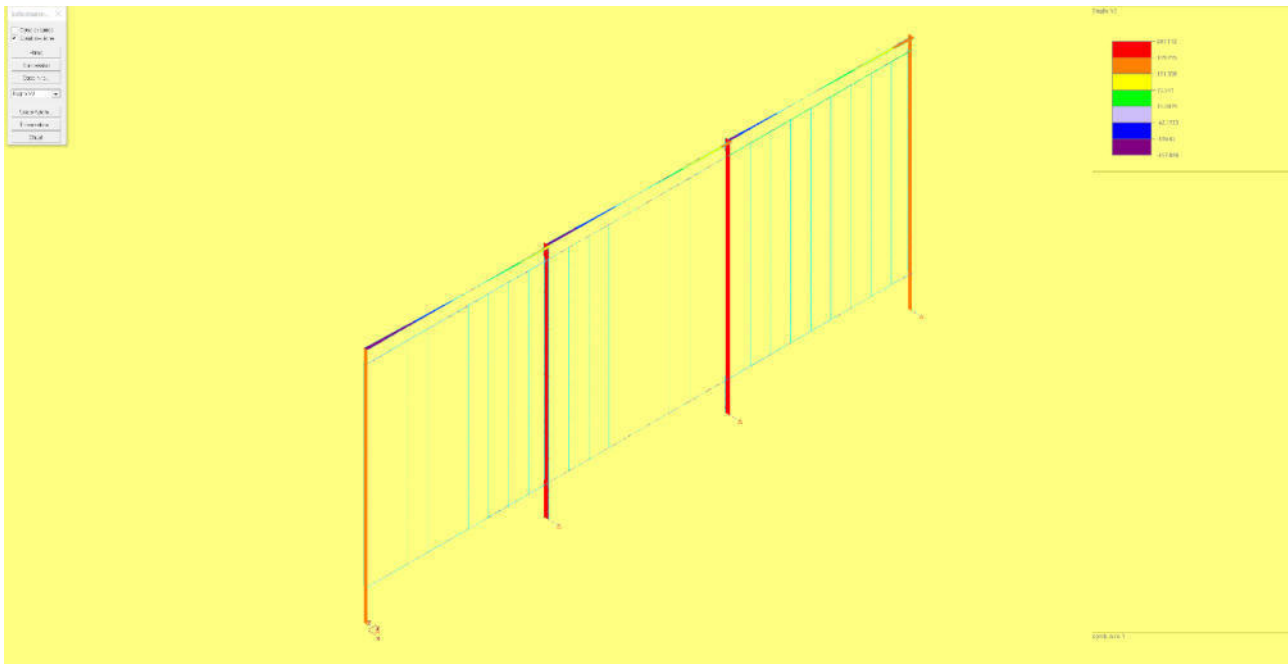
La massima azione di compressione è nel collegamento ed è pari a :

239 daN di trazione;



SOLLECITAZIONE DI TAGLIO (V2 - daN) - COMB 1

Il taglio V2 è trascurabile.

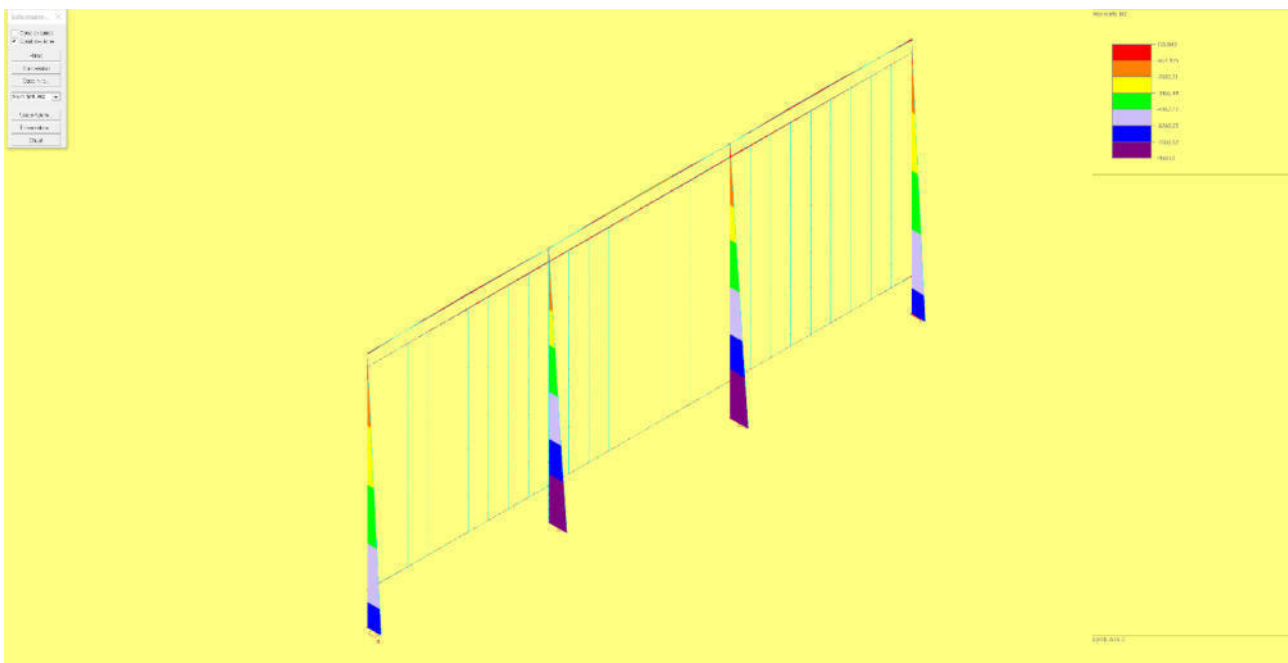


SOLLECITAZIONE DI TAGLIO (V_3 - DAN) - COMB 1

Il Taglio V_3 è 247 da N.

In conclusione il taglio non è presente significativamente.

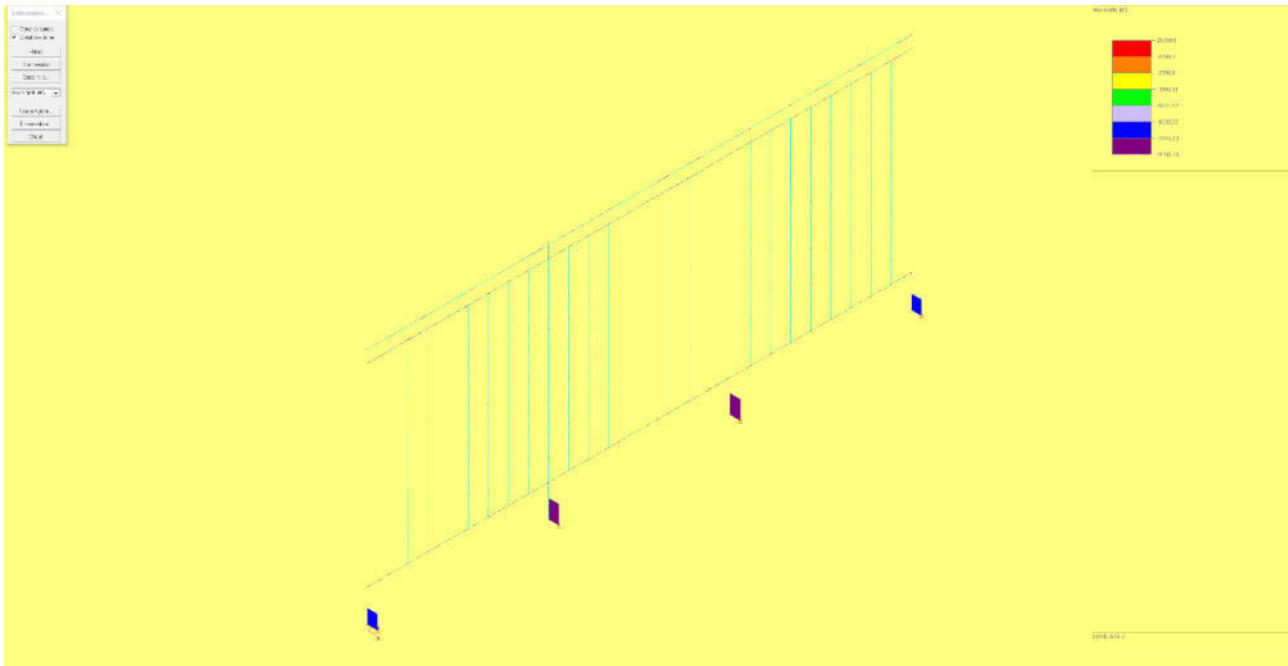
Momento flettente.



SOLLECITAZIONE MOMENTO FLETTENTE (M_2 - DAN CM) - COMB 1 STATICA

Il momento flettente M_2 , al piede dei montanti vale : $M_2 = 9070 \text{ daN} \times \text{cm} = 90,7 \text{ daN} \times \text{m}$

Tale momento si ribalta come momento negli attacchi.



SOLLECITAZIONE MOMENTO FLETTENTE (M_3 – daN cm) - COMB 1 STATICA

$$M_3 = 9158 \text{ daN} \times \text{cm} = 91,6 \text{ daN} \times \text{m}$$

Riassumendo ai fini delle verifiche delle giunzioni all'attacco con la piastra, per la combinazione statica, sono significative le seguenti sollecitazioni:

Azione normale di trazione : **239 daN** ;

Azione flettente : **91,6 daN x m**;

Azione di taglio : **trascurabile daN** .

- verifica dei bulloni di fissaggio della piastra al supporto

Il valore del momento flettente, unica azione significativa, è pari a:

$$M=91,6 \text{ daN m} = 9158 \text{ daN Cm}$$

Questa azione si ripartisce a trazione sulle due barre superiori e a compressione nella piastra per contatto. Per semplicità di calcolo si considera la distanza (d) tra le barre superiori e la barra inferiore, da cui il valore dell'azione di trazione su ogni barra tesa sarà inferiore al valore seguente:

$$\text{Azione normale di trazione: } N_{Ed} = M/(2 \times d) = 9158/(2 \times 9) = 508 \text{ daN}$$

La barra DI VERIFICA ha una sezione di 8 mm, acciaio 8.8.

Per i bulloni resistenti a trazione si ha (p.to 4.2.8.1.1 ntc-2018)

$$F_{t,Rd} = 0,9 f_{tb} A_{res} / \gamma_{M2} = 0,9 \times 8000 \times 0,50 / 1,25 = 28800 \text{ N} = 2880 \text{ daN} \quad [4.2.62]$$

Dove

f_{tb} = è la tensione di rottura del perno e pari a $f_{tb}=8000 \text{ daN/cm}^2$;

A= area del perno in cmq pari a 0,50 cmq;

γ_{M2} = un coefficiente di sicurezza pari a 1,25 (tab.4.2.XII)

Da ciò deriva la verifica è ampiamente soddisfatta:

$$N_{Ed} = 508 \text{ daN} < 2880 \text{ daN} = F_{t,Rd}$$

Resta ora da verificare la lunghezza di ancoraggio del perno nel calcestruzzo.

La verifica dell'ancoraggio nel calcestruzzo si riduce a verificare se è garantita la sollecitazione di progetto:

$$F_{t,Ed} = \text{trazione} = 508 + 239/3 = 587 \text{ daN};$$

$$F_{v,Ed} = \text{taglio} = 0 \text{ daN}.$$

Il foro del fissaggio chimico è 20 mm, profondo 15 cm. La resistenza del calcestruzzo è assunto pari a C 20/25.

Il valore della resistenza di calcolo del calcestruzzo è (p.to 4.1.2.1.1.1):

$$f_{cd} = \alpha_{cc} * f_{ck} / \gamma_c$$

dove

α_{cc} : coefficiente riduttivo per le resistenze di lunga durata = 0,85;

f_{ck} : resistenza caratteristica cilindrica a compressione del cls a 28 gg;

γ_c : coefficiente parziale di sicurezza relativo al calcestruzzo = 1,5;

da cui si ottengono i seguenti valori di resistenza di calcolo del calcestruzzo

<i>Classe di resistenza del calcestruzzo</i>	<i>Resistenza caratteristica a compressione su cubi del cls a 28 gg</i>	<i>Resistenza caratteristica cilindrica f_{ck} a compressione del cls a 28 gg</i>	<i>Resistenza di calcolo a compressione $[N/mm^2]$</i>	<i>Resistenza di calcolo a trazione $[N/mm^2]$</i>
C20/25	25 N/mm²	20 N/mm²	11,33	1,03

$f_{cd} = 11,33 \text{ N/mm}^2$ resistenza a compressione di progetto;

$f_{ctd} = 1,03 \text{ N/mm}^2$ resistenza a trazione di progetto;

$f_{bd} = 2,25 \times 1 \times 1 \times f_{ctk} = 2,25 \times 1 \times 1 \times 0,7 \times 0,3 \times (f_{ck})^{2/3} = 3,48 \text{ N/mm}^2$ resistenza tangenziale di aderenza di progetto;

quindi le resistenze di progetto risultano:

resistenza a taglio del calcestruzzo entro i fori;

$$F_{vb,Rd} = d \times l \times f_{cd} = 2 \text{ cm} \times 15 \text{ cm} \times 113 \text{ daN/cm}^2 = 3390 \text{ daN};$$

resistenza a trazione degli ancoraggi per aderenza del cls

$$F_{tb,Rd} = A_l \times l \times f_{bd} = 2 \text{ cm} \times 3,14 \times 15 \text{ cm} \times 34,8 \text{ daN/cm}^2 = \mathbf{3278 \text{ daN}} ;$$

e la verifica risulta soddisfatta

$$F_{v,Ed} / F_{vb,Rd} = 247/3390 = 0,07 < 1 \text{ Verifica soddisfatta}$$

$$F_{t,Ed} / F_{tb,Rd} = 587 / 3278 = 0,18 < 1 \text{ Verifica soddisfatta}$$

dato che si è in presenza combinata di trazione e taglio, si applica la seguente formula di verifica:

$$\frac{F_{v,Ed}}{F_{v,Rd}} + \frac{F_{t,Ed}}{1,4 F_{t,Rd}} = 247/3390 + 587/(1,4 \times 3278) = 0,07 + 0,13 = 0,20 < 1 \quad (\text{Verifica soddisfatta})$$

6. - RELAZIONE DI CALCOLO DELLA STRUTTURA (PER IL CODICE DI CALCOLO UTILIZZATO)

Normativa di riferimento

- [1] N.T.C. 17/01/18 Norme tecniche per le costruzioni
[2] Eurocodici approvati dal Comitato Europeo di Normazione in forma di Euro Norma (EN)
[3] Istruzioni CNR 10024/86 Analisi mediante elaboratore: impostazione e redazione delle relazioni di calcolo

Criteri di analisi della sicurezza e metodi di analisi strutturale

La verifica della sicurezza degli elementi strutturali avviene con il metodo agli stati limite.

I metodi impiegati per l' analisi strutturale sono i seguenti :

- per carichi statici: metodo degli spostamenti

- carichi sismici: analisi statica equivalente, oppure analisi dinamica modale con spettro di risposta

Spostamenti e azioni sono calcolati con il metodo agli elementi finiti (F.E.M.)

Il metodo degli elementi finiti si basa sulla schematizzazione di una struttura come insieme di elementi di varie geometrie e caratteristiche, connessi l'un l'altro solo in corrispondenza di un numero determinato di punti chiamati 'nodi'. Tali nodi, definiti da tre coordinate rispetto ad un sistema di riferimento cartesiano globale, vengono contrassegnati da un identificatore numerico ('numerazione nodale') crescente a partire da 1.

Anche gli elementi, risultano a loro volta individuati da un identificatore numerico crescente.

Incognite del problema (metodo degli spostamenti) sono assunte le 6 componenti di spostamento di ogni nodo, riferite alla terna globale (traslazioni secondo X,Y,Z, rotazioni attorno X,Y,Z) escluse naturalmente quelle impedita dai vincoli imposti alla struttura.

Il metodo permette di giungere all' impostazione di un sistema di equazioni algebriche lineari, nelle sopra citate componenti di spostamento (gradi di liberta') i cui termini noti sono costituiti dai carichi agenti sulla struttura opportunamente concentrati nei nodi:

$K \cdot u = F$

dove K = matrice di rigidezza
 u = vettore spostamenti nodali
 F = vettore forze nodali

Dagli spostamenti risultanti dalla risoluzione del sistema vengono quindi dedotte le sollecitazioni e/o le tensioni in punti caratteristici di ogni elemento, riferite generalmente ad una terna locale all' elemento stesso.

Sistema di riferimento globale

Il sistema di riferimento impiegato, per nodi ed elementi e tutti gli altri dati strutturali, e' costituito da una terna cartesiana destrorsa XYZ.

Si assume che l'asse Z sia verticale ed orientato verso l'alto.

Modellazione della struttura e dei vincoli

La struttura e' modellata come insieme di 'elementi', tra loro collegati in punti chiamati 'nodi'. Gli elementi sono del tipo:

Elem. monodimensionali (una dimensione prevalente sulle altre due)

- aste
- travi, pilastri
- molle

Elementi bidimensionali (due dimensioni prevalenti sulla terza):

- setti, piastre
- membrane

Elementi tridimensionali (tre dimensioni paragonabili):

- plinti

asta : elemento lineare a sezione costante ed asse rettilineo, reagente a solo sforzo assiale.

Nello spazio 3-D l'elemento asta ha 3 gradi di libert  ai nodi cui corrispondono tre componenti di spostamento di traslazione in ognuno dei suoi due nodi di estremit  ed un solo valore della tensione e della forza assiale.

trave: elem. monodimensionale reagente con 6 caratteristiche di sollecitazione (forza assiale, 2 forze di taglio, 2 momenti flettenti, momento torcente), ad ognuna delle due estremit .

L'elemento trave   prismatico, ossia a sezione costante ed asse rettilineo.

Con il termine travi si intendono elementi non verticali.

Con il termine pilastri si intendono elementi verticali.

molla: elemento agente come molla estensionale o rotazionale di opportuna rigidezza, usato per schematizzare vincoli elastici o rigidi, anche in direzioni non coincidenti con quelle della terna globale.

setto/piastra: elemento 2-D, di forma triangolare o quadrangolare, reagente ad azioni nel proprio piano (azioni membranali) e ad azioni fuori dal proprio piano (azioni flettenti e taglianti).

Questo elemento   usato per rappresentare ad es. pareti verticali, muri di sostegno, platee di fondazione.

membrana: elemento piano 2-D, triangolare o quadrangolare, che reagisce a soli sforzi di membrana.

Questo elemento   ad es. usato per rappresentare il comportamento degli impalcati (solai) nei riguardi delle azioni orizzontali.

plinto: elemento 3-D, viene tradotto in un certo numero di molle traslazionali e rotazionali, che ne schematizzano il comportamento nell'ipotesi che il plinto costituisca un corpo rigido che collega il piede del pilastro ed il terreno modellato alla Winkler.

Fatte le seguenti definizioni (le direzioni 1, 2 sono quelle dei lati dell'area d'impronta del plinto):

K costante normale di sottofondo (misurata ad es. Kg/cm³)

A area d'impronta del plinto

J1 momento d'inerzia dell'area di base intorno a dir. 1

J2 momento d'inerzia dell'area di base intorno a dir. 2

s spostamento verticale del plinto

r1 rotazione del plinto intorno alla direzione 1

r2 rotazione del plinto intorno alla direzione 2

F forza

M momento

$F = K * A * s \implies$ rigidezza molla verticale $= K * A$

$M1 = K * J1 * r1 \implies$ rigidezza molla rotazionale 1 $= K * J1$

$M2 = K * J2 * r2 \implies$ rigidezza molla rotazionale 2 $= K * J2$

Per una descrizione pi  sintetica della struttura, gli elementi sono riuniti

in 'macro-elementi'.

Per macro-elementi, si intende il raggruppamento di piu' elementi, non necessariamente dello stesso tipo, in modo da formare delle parti riconoscibili ed identificabili all'interno della struttura.

-travata : allineamento di travi non verticali (anche ad asse spezzato)

-pilastrata: allineamento di pilastri verticali

-telaio : insieme di travi, pilastri posti in un piano verticale

-muro : insieme di elementi setto/piastra posti in un piano qualsiasi, aventi lo stesso spessore.

-impalcato : insieme di nodi, travi e membrane disposti di solito, ma non necessariamente in un piano orizzontale.

Origine e caratteristiche del codice di calcolo adottato

Il solutore e' il seguente:

- ALGOR SUPERSAP della Algor Interactive Systems, Inc. Pittsburgh, PA, USA

Il programma SUPERSAP applica il metodo degli elementi finiti a strutture di forma qualunque, comunque caricate e vincolate, il cui comportamento e' solitamente considerato lineare (per le eccezioni vedi in seguito)

Si intende con cio' parlare sia di linearita' materiale (proporzionalita' tra tensioni e deformazioni), sia di linearita' geometrica (proporzionalita' tra carichi e spostamenti).

Effettua il calcolo sia in campo statico sia in campo dinamico.

Nel primo caso la routine di risoluzione opera secondo l'algoritmo di Gauss sulla matrice globale suddivisa in blocchi memorizzati su memoria periferica.

Nel secondo caso si puo' optare per un'analisi modale o per una integrazione diretta passo-passo delle equazioni del moto.

I carichi possono essere specificati sia come azioni concentrate applicate ai nodi, sia come forze (o momenti) concentrate o distribuite o variazioni agenti all'interno del singolo elemento.

E' importante sottolineare che il solutore ALGOR SUPERSAP e' stato sottoposto con esito positivo e relativa certificazione, alle prove NAFEMS (test di confronto della National Agency for Finite Element Methods and Standards, in Inghilterra).

Modellazione delle azioni

Le azioni sono modellate secondo due modalita':

1) Azioni nodali

Sono forze o momenti concentrati nei nodi del modello strutturale (oppure cedimenti impressi).

Per ogni carico nodale si riporta il numero del caso di carico relativo ed i valori delle componenti riferite alla terna globale.

2) Carichi agenti sugli elementi

Si tratta di carichi locali agli elementi (carichi distribuiti lungo l'asse di travi, pressioni agenti sulla superficie di setti, variazioni termiche etc).

I carichi possono essere assegnati anche per zone di carico.

Cio' accade quando si carica un impalcato per zone; per zona si intende una regione poligonale, convessa o concava, senza vuoti, individuata dai relativi vertici, che possono essere nodi di estremita' di travi, oppure nodi a setti. Il programma individua, in modo automatico, le eventuali travi e/o pareti, disposte lungo il contorno della poligonale di carico, in modo da ripartire su di esse, il peso proprio, il permanente portato ed il carico accidentale, gravanti sulla zona.

La ripartizione dei carichi avviene con il criterio delle aree di influenza : l'areola elementare e' un quadrilatero avente due lati paralleli alla direzione di orditura del solaio e due lati dati dalle intercette sul contorno della poligonale di carico; il carico gravante sull'areola viene ripartito al 50% tra i due elementi strutturali (travi e/o pareti) disposti lungo i due lati non paralleli alla direzione d'orditura del solaio.

Modellazione strutturale, dei materiali ed interazione terreno-struttura

Le analisi possono essere sia condotte in regime di linearità materiale (proporzionalità tra tensioni e deformazioni), e di linearità geometrica (proporzionalità tra carichi e spostamenti), sia considerando aspetti non lineari del comportamento strutturale, quali:

- presenza di elementi reagenti solo a trazione o solo a compressione
- analisi degli effetti geometrici del 2° ordine con il metodo dei tagli fittizi
- analisi di instabilità globale per la ricerca del moltiplicatore critico dei carichi.

Nei riguardi dell'interazione terreno-struttura, il terreno è modellato come suolo elastico alla Winkler, sia che le strutture di fondazione siano travi (travi su suolo elastico), platee di fondazione (piastre su suolo elastico) o plinti.

Analisi sismica

L'analisi sismica della struttura può essere eseguita con 2 metodi:

- analisi statica equivalente (con solutore statico)
- analisi dinamica modale con spettro di risposta (con solutore dinamico) con gli spettri di progetto definiti dalla Normativa di Riferimento

Con l'analisi statica equiv. il calcolo sismico della struttura si riduce ad una verifica statica conseguente alla applicazione di forze orizzontali (componente ondulatoria dell'azione sismica) e verticali (componente sussultoria del sisma), applicate nel baricentro delle masse gravanti sulla struttura.

Per il sistema di forze distribuite lungo l'altezza dell'edificio si assume una distribuzione lineare degli spostamenti.

La forza da applicare a ciascun piano è data dalla formula seguente:

$$F_i = F_h (z_i W_i) / \sum (z_j W_j)$$

dove: $F_h = S_d(T_1) W l/g$

F_i è la forza da applicare al piano i

W_i e W_j sono i pesi delle masse ai piani i e j rispettivamente

z_i e z_j sono le altezze dei piani i e j rispetto alle fondazioni

$S_d(T_1)$ è l'ordinata dello spettro di risposta di progetto da normativa

W è il peso complessivo della costruzione

l è un coeff. pari a 0,85 se l'edificio ha almeno 3 piani e se $T_1 < 2T_C$, pari a 1,0 in tutti gli altri casi.

g è l'accelerazione di gravità.

Per edifici aventi massa e rigidità distribuite in modo circa simmetrico in pianta, inscrivibile in un rettangolo con rapporto dei lati inferiore a 4, gli effetti torsionali accidentali, possono essere considerati amplificando le sollecitazioni, calcolate con la suddetta distribuzione, in ogni elemento resistente con il fattore (d) risultante dalla seguente espressione:

$$d = 1 + 0.6 x / l_e$$

dove: x = distanza dell'elemento resistente vert. dal baricentro geometrico dell'edificio, misurata perpendicolarmente alla direzione dell'azione sismica considerata

l_e è la distanza tra i due elementi resistenti più lontani, misurata allo stesso modo.

Nei riguardi delle azioni sismiche per gli edifici dotati di orizzontamenti realizzati con i comuni solai, gli orizzontamenti possono essere modellati con piani rigidi.

In questo programma, più realisticamente, si modellano gli impalcati con elementi membrana, di spessore pari allo spessore effettivo del solaio e con un modulo elastico che è quello di fatto attribuibile al solaio.

Le forze orizzontali sismiche sono sempre introdotte come forze nodali, determinando le incidenze di ciascun nodo (gli elementi che convergono in esso) e le relative aliquote di competenza dei 'pesi' degli elementi.

Verifiche degli elementi strutturali

Le verifiche sono effettuate con riferimento all'involuppo delle condizioni di carico (tutti i casi di carico e le combinazioni previste).

In fase di verifica si distinguono i seguenti elementi:

- aste soggette a solo sforzo assiale
- travi prevalentemente soggette a flessione e taglio;
 si distinguono travi in elevazione e di fondazione
- pilastri soggetti a presso(o tenso)-flessione deviata
- setti/piastre si distingue il comportamento a lastra e a piastra
- plinti si distinguono i plinti snelli ed i plinti tozzi

7. RELAZIONE SUI MATERIALI

ACCIAIO LAMINATO (P.TO 11.3.4)

Acciaio impiegato è del tipo S235 controllato in stabilimento.

La resistenza di calcolo dell'acciaio si determina secondo la seguente relazione:

$$f_{yd} = \frac{f_{yk}}{\gamma_s} = \frac{2350}{1.05} = 2240 \text{ daN/cm}^2$$

Con

$f_y = 235 \text{ N/mm}^2$; (tensione caratteristica di snervamento);
 $f_t = 360 \text{ N/mm}^2$ (tensione caratteristica di rottura).

Acciaio (p.to 11.3.4)

Modulo elastico	= 210.000 N/mm ²
Modulo di elasticità trasversale	= G= E/[2(1+v)] = 80769 N/mm ²
Coefficiente di Poisson	v = 0.30
Coefficiente di espansione termica lineare	$\alpha = 12 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$
Densità	= 7850 Kg/mc

SALDATURE

Saldature a cordone d'angolo.

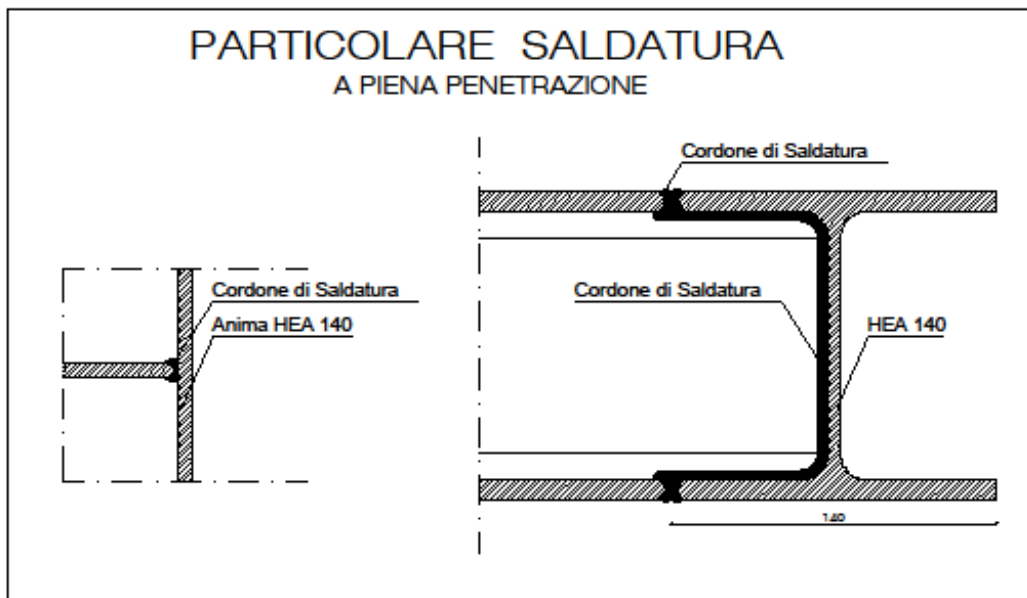
Il progetto prevede saldature delle strutture principali effettuate in officina e in opera con saldatrice elettrica a filo continuo; la saldatura a cordone d'angolo dovrà presentare una classe caratterizzata da ragionevole assenza di difetti interni e da assenza di incrinature interne o da cricche da strappo sui lembi dei cordoni. I lembi al momento della saldatura dovranno essere regolari, lisci, esenti da incrostazioni, ruggine, scaglie, grassi, vernici, irregolarità locali da umidità. I cordoni si dovranno presentare regolari e qualsiasi ripresa dovrà preventivamente richiedere l'asportazione del materiale d'apporto difettoso.

La saldatura degli acciai dovrà avvenire con uno dei procedimenti all'arco elettrico codificati secondo la norma UNI EN ISO 4063:2001.

Sono richieste caratteristiche di duttilità, snervamento, resistenza e tenacità in zona fusa e in zona termica alterata non inferiore a quelle del materiale di base.

Nell'esecuzione delle saldature dovranno inoltre essere rispettate le norme UNI EN 1011:2005 parti 1 e 2 per gli acciai ferritici e della parte 3 per gli acciai inossidabili. Per la preparazione dei lembi si applicherà, salvo casi particolari, la norma UNI EN ISO 9692-1:2005

Le saldature saranno a piena penetrazione, come indicato al punto 4.2.8.2.1 delle norme tecniche e illustrato nello schema allegato.



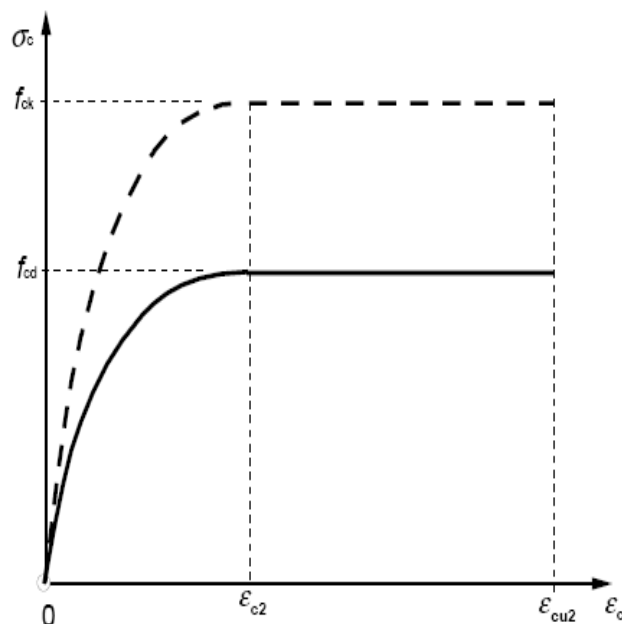
BULLONATURE

Bulloni ad alta resistenza: **Viti classe 8.8 – Dadi classe 8**

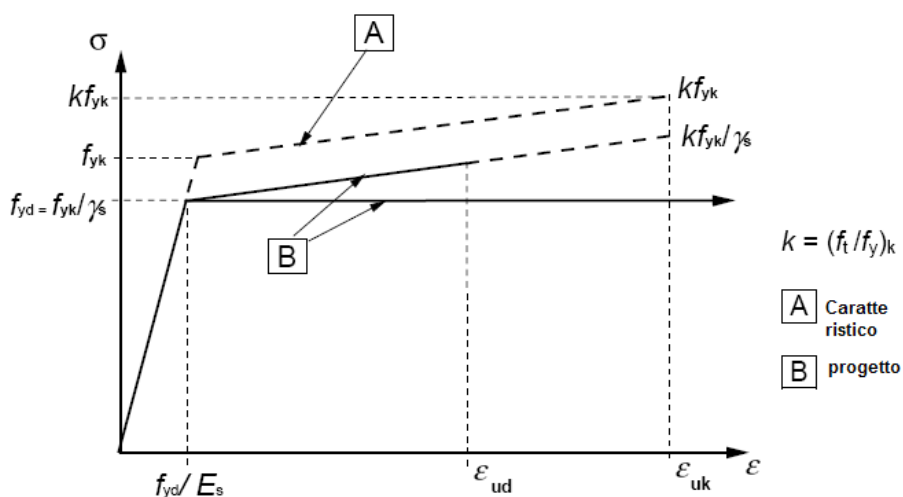
Bulloni con caratteristiche dimensionali conformi alle norme UNI EN ISO 4016:2002 e UNI 5592:1968, con viti appartenenti alla classe 8.8 e dadi di classe 8, così come indicato nella norma UNI EN ISO 898-1:2001.

Tensione caratteristica di snervamento	$f_{yb} = 649$	N/mm ²
Tensione caratteristica di rottura	$f_{tb} = 800$	N/mm ²

Per le altre caratteristiche meccaniche e fisiche del calcestruzzo si rimanda al tabulato di calcolo.

I LEGAMI COSTITUTIVI UTILIZZATI SONO:**- LEGAME PARABOLA RETTANGOLO PER IL CALCESTRUZZO****LEGAME COSTITUTIVO DI PROGETTO DEL CALCESTRUZZO**

Il valore ε_{cu2} nel caso di analisi non lineari sarà valutato in funzione dell'effettivo grado di confinamento esercitato dalle staffe sul nucleo di calcestruzzo.

- LEGAME ELASTICO PREFETTAMENTE PLASTICO O INCRUDENTE O DUTTILITA' LIMITATA PER L'ACCIAIO**LEGAME COSTITUTIVO DI PROGETTO ACCIAIO PER C.A.**

8. ALLEGATI

- i. Elaborati di calcolo.

9. BIBLIOGRAFIA E NORMATIVE DI RIFERIMENTO

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Norme per la disciplina delle opere in conglomerato cementizio, normale e precompresso ed a struttura metallica.
- ISTRUZIONI CNR 10024/86 ANALISI MEDIANTE ELABORATORE: IMPOSTAZIONE E REDAZIONE DELLE RELAZIONI DI CALCOLO
- LEGGE NR. 64 DEL 02/02/1974.
PROVVEDIMENTI PER LE COSTRUZIONI CON PARTICOLARI PRESCRIZIONI PER LE ZONE SISMICHE.
- D.M. 9 GENNAIO 1996
NORME TECNICHE PER IL CALCOLO, L' ESECUZIONE ED IL COLLAUDO DELLE STRUTTURE IN CEMENTO ARMATO NORMALE E PRECOMPRESSO E PER LE STRUTTURE METALLICHE
- D.M. 16 GENNAIO 1996
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ANALISI MEDIANTE ELABORATORE: IMPOSTAZIONE E REDAZIONE DELLE RELAZIONI DI CALCOLO
- CIRCOLARE MINISTERO LL.PP. 15 OTTOBRE 1996 N. 252 AA.GG./S.T.C.
ISTRUZIONI PER L'APPLICAZIONE DELLE NORME TECNICHE DI CUI AL D.M. 9 GENNAIO 1996
- CIRCOLARE MINISTERO LL.PP. 10 APRILE 1997 N. 65/AA.GG.
- ISTRUZIONI PER L'APPLICAZIONE DELLE NORME TECNICHE PER LE COSTRUZIONI IN ZONE SISMICHE DI CUI AL D.M. 16 GENNAIO 1996
- D.M. 14/09/05 NORME TECNICHE PER LE COSTRUZIONI
- O. P.C.M. 3274/2003 e s.m.i. come Norma di Dettaglio per le azioni sismiche
- D.M. 17/01/18 NORME TECNICHE PER LE COSTRUZIONI
- CIRCOLARE 2 febbraio 2009 , n. 617 C.S.LL.PP.

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*          CIVILSOFT v.windows 7.84
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* prodotto e distribuito da ASG srl PIACENZA Tel 0523/337389- info@aesegi.it
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*          RELAZIONE DI CALCOLO
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Normativa di riferimento

- [1] N.T.C. 17/01/2018 Norme tecniche per le costruzioni
 [3] Eurocodici approvati dal Comitato Europeo di Normazione in forma di Euro Norma (EN)

Criteri di analisi della sicurezza e metodi di analisi strutturale

La verifica della sicurezza degli elementi strutturali avviene con il metodo agli stati limite.

I metodi impiegati per l'analisi strutturale sono i seguenti :

-per carichi statici: metodo degli spostamenti

-carichi sismici: analisi statica , oppure

analisi dinamica modale con spettro di risposta

Spostamenti e azioni sono calcolati con il metodo agli elementi finiti(F.E.M.)
 Il metodo degli elementi finiti si basa sulla schematizzazione di una struttura come insieme di elementi di varie geometrie e caratteristiche, connessi l'un l'altro solo in corrispondenza di un numero determinato di punti chiamati 'nodi'.

Tali nodi, definiti da tre coordinate rispetto ad un sistema di riferimento cartesiano globale, vengono contrassegnati da un identificatore numerico ('numerazione nodale') crescente a partire da 1.

Anche gli elementi, risultano a loro volta individuati da un identificatore numerico crescente.

Incognite del problema (metodo degli spostamenti) sono assunte le 6 componenti di spostamento di ogni nodo, riferite alla terna globale (traslazioni secondo X,Y,Z, rotazioni attorno X,Y,Z) escluse naturalmente quelle impedita dai vincoli imposti alla struttura.

Il metodo permette di giungere all' impostazione di un sistema di equazioni algebriche lineari, nelle sopra citate componenti di spostamento (gradi di liberta')i cui termini noti sono costituiti dai carichi agenti sulla struttura opportunamente concentrati nei nodi:

$$K * u = F \quad \text{dove} \quad K = \text{matrice di rigidezza} \\ u = \text{vettore spostamenti nodali} \\ F = \text{vettore forze nodali}$$

Dagli spostamenti risultanti dalla risoluzione del sistema vengono quindi dedotte le sollecitazioni e/o le tensioni in punti caratteristici di ogni elemento, riferite generalmente ad una terna locale all' elemento stesso.

Sistema di riferimento globale

Il sistema di riferimento impiegato, per nodi ed elementi e tutti gli altri dati strutturali, e' costituito da una terna cartesiana destrorsa XYZ.

Si assume che l' asse Z sia verticale ed orientato verso l'alto.

Modellazione della struttura e dei vincoli

La struttura e' modellata come insieme di 'elementi', tra loro collegati in punti chiamati 'nodi'. Gli elementi sono del tipo:

Elem. monodimensionali (una dimensione prevalente sulle altre due)

- aste
- travi,pilastri
- molle

Elementi bidimensionali (due dimensioni prevalenti sulla terza):

- setti,piastre
- membrane

Elementi tridimensionali (tre dimensioni paragonabili):

- plinti

asta : elemento lineare a sezione costante ed asse rettilineo, reagente a solo sforzo assiale.

Nello spazio 3-D l' elemento asta ha 3 gradi di liberta' ai nodi cui corrispondono tre componenti di spostamento di traslazione in ognuno dei suoi due nodi di estremita'ed un solo valore della tensione e della forza assiale.

trave: elem. monodimensionale reagente con 6 caratteristiche di sollecitazione (forza assiale,2 forze di taglio,2 momenti flettenti,momento torcente) , ad ognuna delle due estremita'.

L' elemento trave e' prismatico, ossia a sezione costante ed asse rettilineo.

Con il termine travi si intendono elementi non verticali.

Con il termine pilastri si intendono elementi verticali.

molla: elemento agente come molla estensionale o rotazionale di opportuna rigidezza, usato per schematizzare vincoli elastici o rigidi, anche in direzioni non coincidenti con quelle della terna globale.

setto/piastra: elemento 2-D, di forma triangolare o quadrangolare, reagente ad azioni nel proprio piano (azioni membranali) e ad azioni fuori dal proprio piano (azioni flettenti e taglianti). Questo elemento e' usato per rappresentare ad es. pareti verticali,muri di sostegno, platee di fondazione.

membrana: elemento piano 2-D,triangolare o quadrangolare, che reagisce a soli sforzi di membrana. Questo elemento e' ad es.usato per rappresentare il comportamento degli impalcati (solai) nei riguardi delle azioni orizzontali.

plinto: elemento 3-D,viene tradotto in un certo numero di molle traslazionali e rotazionali, che ne schematizzano il comportamento nell' ipotesi che il plinto costituisca un corpo rigido che collega il piede del

pilastrino ed il terreno modellato alla Winkler.
Fatte le seguenti definizioni (le direzioni 1, 2 sono quelle dei lati dell' area d' impronta del plinto):

K	costante normale di sottofondo (misurata ad es. Kg/cm3)
A	area d' impronta del plinto
J1	momento d' inerzia dell'area di base intorno a dir. 1
J2	momento d' inerzia dell'area di base intorno a dir. 2
s	spostamento verticale del plinto
r1	rotazione del plinto intorno alla direzione 1
r2	rotazione del plinto intorno alla direzione 2
F	forza
M	momento

F	=	K * A * s	==>	rigidezza molla verticale	=	K * A
M1	=	K * J1 * r1	==>	rigidezza molla rotazionale 1	=	K * J1
M2	=	K * J2 * r2	==>	rigidezza molla rotazionale 2	=	K * J2

Per una descrizione piu' sintetica della struttura, gli elementi sono riuniti in 'macro-elementi'.
Per macro-elementi, si intende il raggruppamento di piu' elementi, non necessariamente dello stesso tipo, in modo da formare delle parti riconoscibili ed identificabili all' interno della struttura.

-travata : allineamento di travi non verticali (anche ad asse spezzato)
-pilastrata: allineamento di pilastrini verticali
-telaio : insieme di travi, pilastrini posti in un piano verticale
-muro : insieme di elementi sotto/piastra posti in un piano qualsiasi, aventi lo stesso spessore.
-impalcato : insieme di nodi, travi e membrane disposti di solito, ma non necessariamente in un piano orizzontale.

Origine e caratteristiche del codice di calcolo adottato

I solutori attualmente interfacciati con CIVILSOFT sono i seguenti:

- Xfinest di HarpaCeas srl, Milano, Italia
- ALGOR SUPERSAP di Algor Interactive Systems, Inc. Pittsburgh, PA, USA

Entrambi i solutori applicano il metodo degli elementi finiti a strutture di forma qualunque, comunque caricate e vincolate, il cui comportamento e' solitamente considerato lineare (per le eccezioni vedi in seguito)
Si intende con cio' parlare sia di linearita' materiale (proporzionalita' tra tensioni e deformazioni), sia di linearita' geometrica (proporzionalita' tra carichi e spostamenti).
Effettua il calcolo sia in campo statico sia in campo dinamico.
Nel primo caso la routine di risoluzione opera secondo l' algoritmo di Gauss sulla matrice globale suddivisa in blocchi memorizzati su memoria periferica.
Nel secondo caso si puo' optare per un'analisi modale o per una integrazione diretta passo-passo delle equazioni del moto.
I carichi possono essere specificati sia come azioni concentrate applicate ai nodi, sia come forze (o momenti) concentrate o distribuite o variazioni agenti all' interno del singolo elemento.
Il solutore Xfinest e' dotato di apposito manuale di validazione come descritto nella dichiarazione di affidabilita' del codice stesso, fornita con la licenza del programma.
Il solutore ALGOR SUPERSAP e' stato sottoposto con esito positivo e relativa certificazione, alle prove NAFEMS (test di confronto della National Agency for Finite Element Methods and Standards, in Inghilterra).

Modellazione delle azioni

Le azioni sono modellate secondo due modalita':

1) Azioni nodali
Sono forze o momenti concentrati nei nodi del modello strutturale (oppure cedimenti impressi).
Per ogni carico nodale si riporta il numero del caso di carico relativo ed i valori delle componenti riferite alla terna globale.
2) Carichi agenti sugli elementi
Si tratta di carichi locali agli elementi (carichi distribuiti lungo l'asse di travi, pressioni agenti sulla superficie di setti, variazioni termiche etc).

I carichi possono essere assegnati anche per zone di carico.
Cio' accade quando si carica un impalcato per zone; per zona si intende una regione poligonale, convessa o concava, senza vuoti, individuata dai relativi vertici, che possono essere nodi di estremita' di travi, oppure nodi a setti.

Il programma individua, in modo automatico, le eventuali travi e/o pareti, disposte lungo il contorno della poligonale di carico, in modo da ripartire su di esse, il peso proprio, il permanente portato ed il carico accidentale, gravanti sulla zona.

La ripartizione dei carichi avviene con il criterio delle aree di influenza : l'areola elementare e' un quadrilatero avente due lati paralleli alla direzione di orditura del solaio e due lati dati dalle intercette sul contorno della poligonale di carico; il carico gravante sull' areola viene ripartito al 50% tra i due elementi strutturali (travi e/o pareti) disposti lungo i due lati non paralleli alla direzione d' orditura del solaio.

Modellazione strutturale, dei materiali ed interazione terreno-struttura

Le analisi possono essere sia condotte in regime di linearita' materiale (proporzionalita' tra tensioni e deformazioni), e di linearita' geometrica (proporzionalita' tra carichi e spostamenti), sia considerando aspetti non lineari del comportamento strutturale, quali:

- presenza di elementi reagenti solo a trazione o solo a compressione
- analisi degli effetti geometrici del 2o ordine con il metodo dei tagli fittizi
- analisi di instabilita' globale per la ricerca del moltiplicatore critico dei carichi .

Nei riguardi dell' interazione terreno-struttura, il terreno e' modellato come suolo elastico alla Winkler, sia che le strutture di fondazione siano travi (travi su suolo elastico), platee di fondazione (piastre su suolo elastico) o plinti.

Analisi sismica

L'analisi sismica della struttura puo' essere eseguita con 2 metodi:

- analisi statica
- analisi dinamica modale con spettro di risposta con gli spettri di progetto definiti dalla Normativa di Riferimento

Con l'analisi statica il calcolo sismico della struttura si riduce ad una verifica statica conseguente alla applicazione di forze orizzontali (componente ondulatoria dell' azione sismica) e verticali (componente sussultoria del sisma), applicate nel baricentro delle masse gravanti sulla struttura.
Per il sistema di forze distribuite lungo l'altezza dell' edificio si assume

una distribuzione lineare degli spostamenti.
 La forza da applicare a ciascun piano data dalla formula seguente:
 $F_i = F_h (z_i W_i) / S (z_j W_j)$
 dove: $F_h = S_d(T_1) W l/g$
 F_i la forza da applicare al piano i
 W_i e W_j sono i pesi delle masse ai piani i e j rispettivamente
 z_i e z_j sono le altezze dei piani i e j rispetto alle fondazioni
 $S_d(T_1)$ l'ordinata dello spettro di risposta di progetto da normativa
 W il peso complessivo della costruzione
 l un coeff.pari a 0,85 se l'edificio ha almeno 3 piani e se $T_1 < 2T_C$
 , pari a 1,0 in tutti gli altri casi.
 g l'accelerazione di gravità .
 Per edifici aventi massa e rigidità distribuite in modo circa simmetrico
 in pianta, inscrivibile in un rettangolo con rapporto dei lati inferiore a 4,
 gli effetti torsionali accidentali, possono essere considerati amplificando
 le sollecitazioni, calcolate con la suddetta distribuzione, in ogni elemento
 resistente con il fattore (d) risultante dalla seguente espressione:
 $d = 1 + 0.6 x / L_e$
 dove: x = distanza dell'elemento resistente vert. dal baricentro geometrico
 dell'edificio, misurata perpendicolarmente alla direzione dell'azione
 sismica considerata
 L_e la distanza tra i due elementi resistenti pi lontani, misurata
 allo stesso modo.
 Nei riguardi delle azioni sismiche per gli edifici dotati di orizzontamenti
 realizzati con i comuni solai, gli orizzontamenti possono essere modellati
 con piani rigidi.
 In questo programma, piu' realisticamente, si modellano gli impalcati
 con elementi membrana, di spessore pari allo spessore effettivo del solaio
 e con un modulo elastico che e' quello di fatto attribuibile al solaio.
 Le forze orizzontali sismiche sono sempre introdotte come forze nodali,
 determinando le incidenze di ciascun nodo (gli elementi che convergono in
 esso) e le relative aliquote di competenza dei 'pesi' degli elementi.

Verifiche degli elementi strutturali

Le verifiche sono effettuate con riferimento all'involuppo delle condizioni
 di carico (tutti i casi di carico e le combinazioni previste).
 In fase di verifica si distinguono i seguenti elementi:
 - aste soggette a solo sforzo assiale
 - travi prevalentemente soggette a flessione e taglio;
 si distinguono travi in elevazione e di fondazione
 - pilastri soggetti a presso(o tenso)-flessione deviata
 - setti/piastrre si distingue il comportamento a lastra e a piastra
 - plinti si distinguono i plinti snelli ed i plinti tozzi

DESCRIZIONE TABELLA DATI NODALI

Di seguito si riportano le spiegazioni delle sigle usate nella
 tabella DATI NODALI.
 Per ogni nodo identificato da un numero sono scritte le condizioni
 di vincolo delle sue 6 componenti di movimento (traslazioni lungo
 gli assi X, Y, Z globali, rotazioni attorno agli assi X, Y, Z
 globali; codice = 0 componente libera, codice = 1 comp. impedita),
 le sue tre coordinate rispetto alla terna di assi globale e la
 temperatura in gradi centigradi.

NODO : Numero identificativo del nodo
 n.ro
 Tx : Codice di vincolamento per la traslazione in direzione X
 = 0 consentita, = 1 impedita
 Ty : Codice di vincolamento per la traslazione in direzione Y
 = 0 consentita, = 1 impedita
 Tz : Codice di vincolamento per la traslazione in direzione Z
 = 0 consentita, = 1 impedita
 Rx : Codice di vincolamento per la rotazione intorno all' asse X
 = 0 consentita, = 1 impedita
 Ry : Codice di vincolamento per la rotazione intorno all' asse Y
 = 0 consentita, = 1 impedita
 Rz : Codice di vincolamento per la rotazione intorno all' asse Z
 = 0 consentita, = 1 impedita
 X : Coordinata cartesiana X del nodo
 Y : Y
 Z : Z
 TEMP : Temperatura del nodo in gradi centigradi

Nota : sistema di riferimento globale

Il sistema di riferimento impiegato, per nodi ed elementi e tutti
 gli altri dati strutturali, e' una terna cartesiana XYZ destra.
 Si assume che l' asse Z sia verticale ed orientato verso l'alto.

Nota : nodi di orientamento per travi e pilastri

Nella lista dei nodi sono compresi anche gli eventuali nodi K,
 inseriti automaticamente dal programma ed utilizzati per orientare
 spazialmente travi e/o pilastri; tali nodi hanno i codici di
 vincolamento uguali ad 1, e coordinate di valore 1.e+14 (coord. Y
 o coordinata Z).

DESCRIZIONE TABELLA DATI VINCOLI ELASTICI

Di seguito si riportano le spiegazioni delle sigle usate nella
 tabella DATI VINCOLI ELASTICI:

NODO. n.ro numero del nodo cui e' applicato il vincolo elastico
 DIR. X componente x vettore linea d' azione del vincolo
 DIR. Y componente y vettore linea d' azione del vincolo
 DIR. Z componente z vettore linea d' azione del vincolo
 RIG. ROT. valore della rigidità rotazionale del vincolo
 RIG. TRASL. valore della rigidità traslazionale del vincolo

DATI DI INGRESSO : TABELLA DATI NODALI

NODO n.ro	Tx	Ty	Tz	Rx	Ry	Rz	X (cm)	Y (cm)	Z (cm)	Temp (C)
1	0	0	0	0	0	0	0.00	0.00	0.00	0
2	0	0	0	0	0	0	0.00	0.00	27.00	0
3	1	1	1	1	1	1	4.00	0.00	0.00	0
4	0	0	0	0	0	0	0.00	0.00	129.00	0
5	0	0	0	0	0	0	0.00	100.00	27.00	0
6	0	0	0	0	0	0	0.00	100.00	129.00	0
7	0	0	0	0	0	0	0.00	100.00	0.00	0
8	1	1	1	1	1	1	4.00	100.00	0.00	0
9	0	0	0	0	0	0	0.00	10.00	27.00	0
10	0	0	0	0	0	0	0.00	20.00	27.00	0
11	0	0	0	0	0	0	0.00	30.00	27.00	0

12	0	0	0	0	0	0	0.00	40.00	27.00	0
13	0	0	0	0	0	0	0.00	50.00	27.00	0
14	0	0	0	0	0	0	0.00	60.00	27.00	0
15	0	0	0	0	0	0	0.00	70.00	27.00	0
16	0	0	0	0	0	0	0.00	80.00	27.00	0
17	0	0	0	0	0	0	0.00	90.00	27.00	0
18	0	0	0	0	0	0	0.00	10.00	129.00	0
19	0	0	0	0	0	0	0.00	20.00	129.00	0
20	0	0	0	0	0	0	0.00	30.00	129.00	0
21	0	0	0	0	0	0	0.00	40.00	129.00	0
22	0	0	0	0	0	0	0.00	50.00	129.00	0
23	0	0	0	0	0	0	0.00	60.00	129.00	0
24	0	0	0	0	0	0	0.00	70.00	129.00	0
25	0	0	0	0	0	0	0.00	80.00	129.00	0
26	0	0	0	0	0	0	0.00	90.00	129.00	0
27	0	0	0	0	0	0	0.00	190.00	27.00	0
28	0	0	0	0	0	0	0.00	190.00	129.00	0
29	0	0	0	0	0	0	0.00	180.00	27.00	0
30	0	0	0	0	0	0	0.00	180.00	129.00	0
31	0	0	0	0	0	0	0.00	170.00	27.00	0
32	0	0	0	0	0	0	0.00	170.00	129.00	0
33	0	0	0	0	0	0	0.00	160.00	27.00	0
34	0	0	0	0	0	0	0.00	160.00	129.00	0
35	0	0	0	0	0	0	0.00	150.00	27.00	0
36	0	0	0	0	0	0	0.00	150.00	129.00	0
37	0	0	0	0	0	0	0.00	140.00	27.00	0
38	0	0	0	0	0	0	0.00	140.00	129.00	0
39	0	0	0	0	0	0	0.00	130.00	27.00	0
40	0	0	0	0	0	0	0.00	130.00	129.00	0
41	0	0	0	0	0	0	0.00	120.00	27.00	0
42	0	0	0	0	0	0	0.00	120.00	129.00	0
43	0	0	0	0	0	0	0.00	110.00	27.00	0
44	0	0	0	0	0	0	0.00	110.00	129.00	0
45	0	0	0	0	0	0	0.00	200.00	129.00	0
46	0	0	0	0	0	0	0.00	200.00	27.00	0
47	0	0	0	0	0	0	0.00	200.00	0.00	0
48	1	1	1	1	1	1	4.00	200.00	0.00	0
49	0	0	0	0	0	0	0.00	300.00	27.00	0
50	0	0	0	0	0	0	0.00	300.00	129.00	0
51	0	0	0	0	0	0	0.00	300.00	0.00	0
52	1	1	1	1	1	1	4.00	300.00	0.00	0
53	0	0	0	0	0	0	0.00	210.00	27.00	0
54	0	0	0	0	0	0	0.00	220.00	27.00	0
55	0	0	0	0	0	0	0.00	230.00	27.00	0
56	0	0	0	0	0	0	0.00	240.00	27.00	0
57	0	0	0	0	0	0	0.00	250.00	27.00	0
58	0	0	0	0	0	0	0.00	260.00	27.00	0
59	0	0	0	0	0	0	0.00	270.00	27.00	0
60	0	0	0	0	0	0	0.00	280.00	27.00	0
61	0	0	0	0	0	0	0.00	290.00	27.00	0
62	0	0	0	0	0	0	0.00	210.00	129.00	0
63	0	0	0	0	0	0	0.00	220.00	129.00	0
64	0	0	0	0	0	0	0.00	230.00	129.00	0
65	0	0	0	0	0	0	0.00	240.00	129.00	0
66	0	0	0	0	0	0	0.00	250.00	129.00	0
67	0	0	0	0	0	0	0.00	260.00	129.00	0
68	0	0	0	0	0	0	0.00	270.00	129.00	0
69	0	0	0	0	0	0	0.00	280.00	129.00	0
70	0	0	0	0	0	0	0.00	290.00	129.00	0
71	0	0	0	0	0	0	0.00	390.00	27.00	0
72	0	0	0	0	0	0	0.00	390.00	129.00	0
73	0	0	0	0	0	0	0.00	380.00	27.00	0
74	0	0	0	0	0	0	0.00	380.00	129.00	0
75	0	0	0	0	0	0	0.00	370.00	27.00	0
76	0	0	0	0	0	0	0.00	370.00	129.00	0
77	0	0	0	0	0	0	0.00	360.00	27.00	0
78	0	0	0	0	0	0	0.00	360.00	129.00	0
79	0	0	0	0	0	0	0.00	350.00	27.00	0
80	0	0	0	0	0	0	0.00	350.00	129.00	0
81	0	0	0	0	0	0	0.00	340.00	27.00	0
82	0	0	0	0	0	0	0.00	340.00	129.00	0
83	0	0	0	0	0	0	0.00	330.00	27.00	0
84	0	0	0	0	0	0	0.00	330.00	129.00	0
85	0	0	0	0	0	0	0.00	320.00	27.00	0
86	0	0	0	0	0	0	0.00	320.00	129.00	0
87	0	0	0	0	0	0	0.00	310.00	27.00	0
88	0	0	0	0	0	0	0.00	310.00	129.00	0
89	0	0	0	0	0	0	0.00	400.00	129.00	0
90	0	0	0	0	0	0	0.00	400.00	27.00	0
91	0	0	0	0	0	0	0.00	400.00	0.00	0
92	1	1	1	1	1	1	4.00	400.00	0.00	0
93	0	0	0	0	0	0	0.00	500.00	27.00	0
94	0	0	0	0	0	0	0.00	500.00	129.00	0
95	0	0	0	0	0	0	0.00	500.00	0.00	0
96	1	1	1	1	1	1	4.00	500.00	0.00	0
97	0	0	0	0	0	0	0.00	410.00	27.00	0
98	0	0	0	0	0	0	0.00	420.00	27.00	0
99	0	0	0	0	0	0	0.00	430.00	27.00	0
100	0	0	0	0	0	0	0.00	440.00	27.00	0
101	0	0	0	0	0	0	0.00	450.00	27.00	0
102	0	0	0	0	0	0	0.00	460.00	27.00	0
103	0	0	0	0	0	0	0.00	470.00	27.00	0
104	0	0	0	0	0	0	0.00	480.00	27.00	0
105	0	0	0	0	0	0	0.00	490.00	27.00	0
106	0	0	0	0	0	0	0.00	410.00	129.00	0
107	0	0	0	0	0	0	0.00	420.00	129.00	0
108	0	0	0	0	0	0	0.00	430.00	129.00	0
109	0	0	0	0	0	0	0.00	440.00	129.00	0
110	0	0	0	0	0	0	0.00	450.00	129.00	0
111	0	0	0	0	0	0	0.00	460.00	129.00	0
112	0	0	0	0	0	0	0.00	470.00	129.00	0
113	0	0	0	0	0	0	0.00	480.00	129.00	0
114	0	0	0	0	0	0	0.00	490.00	129.00	0

DESCRIZIONE TABELLA DATI TRAVI

Di seguito si riportano le spiegazioni delle sigle usate nella tabella DATI TRAVI:

ELEM. n.ro numero dell' elemento trave
NODO I numero del nodo iniziale della trave
NODO J numero del nodo finale della trave
BETA ANGOLO angolo in gradi sessagesimali per l'orientamento della trave
SVINC I codice di rilascio per l' estremo i della trave
SVINC J codice di rilascio per l' estremo j della trave
SEZ. n.ro numero della sezione costituente la trave
MAT. n.ro numero del materiale costituente la trave
FOND. codice per identificare le travi di fondazione su
 suolo alla Winkler: 0 ==> trave in elevazione

1 ==> trave di fondazione
K TERR. modulo di Winkler del terreno
FILO I codice del tipo di filo fisso per il nodo i
FILO J codice del tipo di filo fisso per il nodo j
elem.secondario se appare questa scritta allora l'elemento e' secondario
nel senso del p.to 7.2.3 NTC 2018

Per la descrizione del significato dei codici di filo fisso, usati per le travi, si rimanda alla documentazione fornita con il programma.

Il codice 0, lascia immutata la posizione dell' asse della trave. Per i codici da 1 a 2, il programma calcola gli scostamenti DX e DY del filo fisso rispetto all' asse baricentrico della trave. Il codice 9, si usa quando gli scostamenti DX e DY, sono digitati direttamente.

Nel caso di travi inclinate rispetto ad XY, per avere l'effetto dei codici 1 e 2, basta ragionare per continuita' ruotando, in senso antiorario il segmento che rappresenta l' asse della trave.

Sistema di riferimento locale per travi :
definizione asse locale 1 : dal nodo I al nodo J
si definisce un terzo nodo, detto nodo K, in base all'angolo BETA in modo che se BETA=0, il nodo K si trova nel piano verticale che comprende la trave, diversamente tale piano ruota dell'angolo BETA
definizione assi locali 2, 3: definiti i nodi I, J, si traccia il piano passante per la retta I-J e per il nodo K; l' intersezione di tale piano con il piano normale ad I-J (piano della sezione della trave), individua l' asse 2 rivolto sempre dalla parte del nodo K; l' asse 3 e' definito in direzione e verso se si impone che la terna sia destrorsa.

Codici di rilascio (o svincolamento) per travi :
Vi e' un codice di rilascio per ognuno dei 6 gradi di liberta' dei 2 nodi estremi dell' elemento: se il codice e' 0, l' estremo della trave risulta solidale con la restante struttura nei riguardi di movimenti lungo l'asse locale considerato; se il codice vale 1, invece risulta sconnesso.

I codici di rilascio sono espressi nel riferimento locale.

DATI DI INGRESSO : TABELLA DATI TRAVI

ELEM. n.ro	NODO I	NODO J	BETA ANGOLO	SVINC. I	SVINC. J	SEZ n.ro	MAT n.ro	FOND.	K TERR. (Kg/cm3)	FILO I J
2	1	3	0.0	000000	000000	3	1	0	0.0	0 0
5	7	8	0.0	000000	000000	3	1	0	0.0	0 0
7	2	9	0.0	000000	000000	1	1	0	0.0	0 0
8	9	10	0.0	000000	000000	1	1	0	0.0	0 0
9	10	11	0.0	000000	000000	1	1	0	0.0	0 0
10	11	12	0.0	000000	000000	1	1	0	0.0	0 0
11	12	13	0.0	000000	000000	1	1	0	0.0	0 0
12	13	14	0.0	000000	000000	1	1	0	0.0	0 0
13	14	15	0.0	000000	000000	1	1	0	0.0	0 0
14	15	16	0.0	000000	000000	1	1	0	0.0	0 0
15	16	17	0.0	000000	000000	1	1	0	0.0	0 0
16	17	5	0.0	000000	000000	1	1	0	0.0	0 0
17	4	18	0.0	000000	000000	5	1	0	0.0	0 0
18	18	19	0.0	000000	000000	5	1	0	0.0	0 0
19	19	20	0.0	000000	000000	5	1	0	0.0	0 0
20	20	21	0.0	000000	000000	5	1	0	0.0	0 0
21	21	22	0.0	000000	000000	5	1	0	0.0	0 0
22	22	23	0.0	000000	000000	5	1	0	0.0	0 0
23	23	24	0.0	000000	000000	5	1	0	0.0	0 0
24	24	25	0.0	000000	000000	5	1	0	0.0	0 0
25	25	26	0.0	000000	000000	5	1	0	0.0	0 0
26	26	6	0.0	000000	000000	5	1	0	0.0	0 0
45	28	45	0.0	000000	000000	5	1	0	0.0	0 0
46	30	28	0.0	000000	000000	5	1	0	0.0	0 0
47	32	30	0.0	000000	000000	5	1	0	0.0	0 0
48	34	32	0.0	000000	000000	5	1	0	0.0	0 0
49	36	34	0.0	000000	000000	5	1	0	0.0	0 0
50	38	36	0.0	000000	000000	5	1	0	0.0	0 0
51	40	38	0.0	000000	000000	5	1	0	0.0	0 0
52	42	40	0.0	000000	000000	5	1	0	0.0	0 0
53	44	42	0.0	000000	000000	5	1	0	0.0	0 0
54	6	44	0.0	000000	000000	5	1	0	0.0	0 0
55	27	46	0.0	000000	000000	1	1	0	0.0	0 0
56	29	27	0.0	000000	000000	1	1	0	0.0	0 0
57	31	29	0.0	000000	000000	1	1	0	0.0	0 0
58	33	31	0.0	000000	000000	1	1	0	0.0	0 0
59	35	33	0.0	000000	000000	1	1	0	0.0	0 0
60	37	35	0.0	000000	000000	1	1	0	0.0	0 0
61	39	37	0.0	000000	000000	1	1	0	0.0	0 0
62	41	39	0.0	000000	000000	1	1	0	0.0	0 0
63	43	41	0.0	000000	000000	1	1	0	0.0	0 0
64	5	43	0.0	000000	000000	1	1	0	0.0	0 0
66	47	48	0.0	000000	000000	3	1	0	0.0	0 0
69	51	52	0.0	000000	000000	3	1	0	0.0	0 0
71	46	53	0.0	000000	000000	1	1	0	0.0	0 0
72	53	54	0.0	000000	000000	1	1	0	0.0	0 0
73	54	55	0.0	000000	000000	1	1	0	0.0	0 0
74	55	56	0.0	000000	000000	1	1	0	0.0	0 0
75	56	57	0.0	000000	000000	1	1	0	0.0	0 0
76	57	58	0.0	000000	000000	1	1	0	0.0	0 0
77	58	59	0.0	000000	000000	1	1	0	0.0	0 0
78	59	60	0.0	000000	000000	1	1	0	0.0	0 0
79	60	61	0.0	000000	000000	1	1	0	0.0	0 0
80	61	49	0.0	000000	000000	1	1	0	0.0	0 0
81	45	62	0.0	000000	000000	5	1	0	0.0	0 0
82	62	63	0.0	000000	000000	5	1	0	0.0	0 0
83	63	64	0.0	000000	000000	5	1	0	0.0	0 0
84	64	65	0.0	000000	000000	5	1	0	0.0	0 0
85	65	66	0.0	000000	000000	5	1	0	0.0	0 0
86	66	67	0.0	000000	000000	5	1	0	0.0	0 0
87	67	68	0.0	000000	000000	5	1	0	0.0	0 0
88	68	69	0.0	000000	000000	5	1	0	0.0	0 0
89	69	70	0.0	000000	000000	5	1	0	0.0	0 0
90	70	50	0.0	000000	000000	5	1	0	0.0	0 0
109	72	89	0.0	000000	000000	5	1	0	0.0	0 0
110	74	72	0.0	000000	000000	5	1	0	0.0	0 0
111	76	74	0.0	000000	000000	5	1	0	0.0	0 0
112	78	76	0.0	000000	000000	5	1	0	0.0	0 0
113	80	78	0.0	000000	000000	5	1	0	0.0	0 0
114	82	80	0.0	000000	000000	5	1	0	0.0	0 0
115	84	82	0.0	000000	000000	5	1	0	0.0	0 0
116	86	84	0.0	000000	000000	5	1	0	0.0	0 0
117	88	86	0.0	000000	000000	5	1	0	0.0	0 0

118	50	88	0.0	000000	000000	5	1	0	0.0	0	0
119	71	90	0.0	000000	000000	1	1	0	0.0	0	0
120	73	71	0.0	000000	000000	1	1	0	0.0	0	0
121	75	73	0.0	000000	000000	1	1	0	0.0	0	0
122	77	75	0.0	000000	000000	1	1	0	0.0	0	0
123	79	77	0.0	000000	000000	1	1	0	0.0	0	0
124	81	79	0.0	000000	000000	1	1	0	0.0	0	0
125	83	81	0.0	000000	000000	1	1	0	0.0	0	0
126	85	83	0.0	000000	000000	1	1	0	0.0	0	0
127	87	85	0.0	000000	000000	1	1	0	0.0	0	0
128	49	87	0.0	000000	000000	1	1	0	0.0	0	0
130	91	92	0.0	000000	000000	3	1	0	0.0	0	0
133	95	96	0.0	000000	000000	3	1	0	0.0	0	0
135	90	97	0.0	000000	000000	1	1	0	0.0	0	0
136	97	98	0.0	000000	000000	1	1	0	0.0	0	0
137	98	99	0.0	000000	000000	1	1	0	0.0	0	0
138	99	100	0.0	000000	000000	1	1	0	0.0	0	0
139	100	101	0.0	000000	000000	1	1	0	0.0	0	0
140	101	102	0.0	000000	000000	1	1	0	0.0	0	0
141	102	103	0.0	000000	000000	1	1	0	0.0	0	0
142	103	104	0.0	000000	000000	1	1	0	0.0	0	0
143	104	105	0.0	000000	000000	1	1	0	0.0	0	0
144	105	93	0.0	000000	000000	1	1	0	0.0	0	0
145	89	106	0.0	000000	000000	5	1	0	0.0	0	0
146	106	107	0.0	000000	000000	5	1	0	0.0	0	0
147	107	108	0.0	000000	000000	5	1	0	0.0	0	0
148	108	109	0.0	000000	000000	5	1	0	0.0	0	0
149	109	110	0.0	000000	000000	5	1	0	0.0	0	0
150	110	111	0.0	000000	000000	5	1	0	0.0	0	0
151	111	112	0.0	000000	000000	5	1	0	0.0	0	0
152	112	113	0.0	000000	000000	5	1	0	0.0	0	0
153	113	114	0.0	000000	000000	5	1	0	0.0	0	0
154	114	94	0.0	000000	000000	5	1	0	0.0	0	0

DESCRIZIONE TABELLA DATI PILASTRI

Di seguito si riportano le spiegazioni delle sigle usate nella tabella DATI PILASTRI:

ELEM. N.RO numero dell' elemento pilastro
NODO I numero del nodo iniziale del pilastro
NODO J numero del nodo finale del pilastro
BETA ANGOLO angolo in gradi sessagesimali per l'orientamento del pilastro
SVINC I codice di rilascio per l' estremo i del pilastro
SVINC J codice di rilascio per l' estremo j del pilastro
SEZ. n.ro numero della sezione costituente il pilastro
MAT. n.ro numero del materiale costituente il pilastro
FOND. campo non utilizzato per i pilastri
FILO I codice del tipo di filo fisso per il nodo i
FILO J codice del tipo di filo fisso per il nodo j
elem.secondario se appare questa scritta allora l'elemento e' secondario
nel senso del p.to 7.2.3 NTC 2018

Fili fissi di pilastri:

Per la descrizione del significato dei codici di filo fisso, si rimanda alla documentazione fornita con il programma.

Per i codici da 1 a 8, il programma calcola gli scostamenti DX e DY del filo fisso rispetto all' asse baricentrico del pilastro.

Il codice 0, lascia immutata la posizione dell' asse del pilastro.

Il codice 9, si usa quando gli scostamenti DX e DY, sono digitati direttamente.

Sistema di riferimento locale per pilastri:

definizione asse locale 1 : dal nodo I al nodo J
si definisce un terzo nodo, detto nodo K, in base all'angolo BETA in modo che se BETA=0, il nodo K si trova nel piano definito dal pilastro e dalla direzione Y, diversamente tale piano ruota dell' angolo BETA

definizione assi locali 2, 3: definiti i nodi I, J, e' possibile tracciare il piano passante per la retta I-J e per il nodo K; la intersezione di tale piano con il piano normale ad I-J (piano della sezione della trave), individua l' asse 2 rivolto sempre dalla parte del nodo K; l' asse 3 risulta a questo punto definito in direzione e verso poiche' si impone che la terna sia destrorsa.

Codici di rilascio (o svincolamento) per pilastri:

Vi e' un codice di rilascio per ognuno dei 6 gradi di liberta' dei 2 nodi estremi dell' elemento: se il codice e' 0, l' estremo del pilastro risulta solidale con la restante struttura nei riguardi di movimenti lungo l'asse locale considerato; se il codice vale 1, invece risulta sconnesso.

I codici di rilascio sono espressi nel riferimento locale.

DATI DI INGRESSO : TABELLA DATI PILASTRI

ELEM. n.ro	NODO I	NODO J	BETA ANGOLO	SVINC. I	SVINC. J	SEZ n.ro	MAT n.ro	FOND.	FILO I	FILO J
1	1	2	0.0	000000	000000	3	1	0	0	0
3	2	4	0.0	000000	000000	3	1	0	0	0
4	5	6	0.0	000000	000000	3	1	0	0	0
6	7	5	0.0	000000	000000	3	1	0	0	0
27	9	18	0.0	000000	000000	2	1	0	0	0
28	10	19	0.0	000000	000000	2	1	0	0	0
29	11	20	0.0	000000	000000	2	1	0	0	0
30	12	21	0.0	000000	000000	2	1	0	0	0
31	13	22	0.0	000000	000000	2	1	0	0	0
32	14	23	0.0	000000	000000	2	1	0	0	0
33	15	24	0.0	000000	000000	2	1	0	0	0
34	16	25	0.0	000000	000000	2	1	0	0	0
35	17	26	0.0	000000	000000	2	1	0	0	0
36	27	28	0.0	000000	000000	2	1	0	0	0
37	29	30	0.0	000000	000000	2	1	0	0	0
38	31	32	0.0	000000	000000	2	1	0	0	0
39	33	34	0.0	000000	000000	2	1	0	0	0
40	35	36	0.0	000000	000000	2	1	0	0	0
41	37	38	0.0	000000	000000	2	1	0	0	0
42	39	40	0.0	000000	000000	2	1	0	0	0
43	41	42	0.0	000000	000000	2	1	0	0	0
44	43	44	0.0	000000	000000	2	1	0	0	0
65	47	46	0.0	000000	000000	3	1	0	0	0
67	46	45	0.0	000000	000000	3	1	0	0	0
68	49	50	0.0	000000	000000	3	1	0	0	0
70	51	49	0.0	000000	000000	3	1	0	0	0
91	53	62	0.0	000000	000000	2	1	0	0	0
92	54	63	0.0	000000	000000	2	1	0	0	0
93	55	64	0.0	000000	000000	2	1	0	0	0

94	56	65	0.0	000000	000000	2	1	0	0	0
95	57	66	0.0	000000	000000	2	1	0	0	0
96	58	67	0.0	000000	000000	2	1	0	0	0
97	59	68	0.0	000000	000000	2	1	0	0	0
98	60	69	0.0	000000	000000	2	1	0	0	0
99	61	70	0.0	000000	000000	2	1	0	0	0
100	71	72	0.0	000000	000000	2	1	0	0	0
101	73	74	0.0	000000	000000	2	1	0	0	0
102	75	76	0.0	000000	000000	2	1	0	0	0
103	77	78	0.0	000000	000000	2	1	0	0	0
104	79	80	0.0	000000	000000	2	1	0	0	0
105	81	82	0.0	000000	000000	2	1	0	0	0
106	83	84	0.0	000000	000000	2	1	0	0	0
107	85	86	0.0	000000	000000	2	1	0	0	0
108	87	88	0.0	000000	000000	2	1	0	0	0
129	91	90	0.0	000000	000000	3	1	0	0	0
131	90	89	0.0	000000	000000	3	1	0	0	0
132	93	94	0.0	000000	000000	3	1	0	0	0
134	95	93	0.0	000000	000000	3	1	0	0	0
155	97	106	0.0	000000	000000	2	1	0	0	0
156	98	107	0.0	000000	000000	2	1	0	0	0
157	99	108	0.0	000000	000000	2	1	0	0	0
158	100	109	0.0	000000	000000	2	1	0	0	0
159	101	110	0.0	000000	000000	2	1	0	0	0
160	102	111	0.0	000000	000000	2	1	0	0	0
161	103	112	0.0	000000	000000	2	1	0	0	0
162	104	113	0.0	000000	000000	2	1	0	0	0
163	105	114	0.0	000000	000000	2	1	0	0	0

DESCRIZIONE TABELLA DATI INCASTRATI PARZIALI TRAVI

Di seguito si riportano le spiegazioni delle sigle usate nella tabella DATI INCASTRATI PARZIALI TRAVI:

ELEM. n.ro numero dell' elemento trave
 NODO I numero del nodo iniziale della trave
 NODO J numero del nodo finale della trave
 SVINC PARZ. I coeff.moltiplicativi rigidezza flessionale al nodo I
 SVINC PARZ. J coeff.moltiplicativi rigidezza flessionale al nodo J

I coefficienti moltiplicativi della rigidezza flessionale per i nodi I,J della trave, sono riferiti alle rotazioni R2, R3 rispettivamente intorno agli assi 2, 3 della terna locale in I,J.
 Il valore max dei coefficienti e' 1., corrispondente alla situazione di incastro.

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DATI DI INGRESSO : TABELLA INCASTRATI PARZIALI TRAVI

ELEM.	NODO	NODO	SVINCOLI PARZIALI			
n.ro	I	J	I(R2)	I(R3)	J(R2)	J(R3)

DESCRIZIONE TABELLA FILI FISSI TRAVI

Di seguito si riportano le spiegazioni delle sigle usate nella tabella FILI FISSI TRAVI (o SETTI):

ELEM. n.ro numero dell' elemento trave
 SEZ. n.ro numero della sezione costituente la trave
 ZI coordinata Z (quota) del nodo iniziale I della trave
 ZJ coordinata Z (quota) del nodo finale J della trave
 FILO I codice del tipo di filo fisso per il nodo iniziale I
 FILO J codice del tipo di filo fisso per il nodo finale J
 DXI scostamenti DX del filo fisso rispetto all' asse
 baricentrico della trave nel nodo iniziale I
 DXJ scostamenti DX del filo fisso rispetto all' asse
 baricentrico della trave nel nodo finale J
 DYI scostamenti DY del filo fisso rispetto all' asse
 baricentrico della trave nel nodo iniziale I
 DYJ scostamenti DY del filo fisso rispetto all' asse
 baricentrico della trave nel nodo finale J

nota : questa tabella e' valida anche per i setti purché al posto del n.ro di SEZIONE si metta lo SPESSORE, e come quote ZI e ZF si mettano le quote minima e massima del setto.

DESCRIZIONE TABELLA FILI FISSI PILASTRI

Di seguito si riportano le spiegazioni delle sigle usate nella tabella FILI FISSI PILASTRI:

ELEM.n.ro numero dell' elemento pilastro
 SEZ. n.ro numero della sezione costituente il pilastro
 XI coordinata X (in pianta) del filo fisso del pilastro
 YI coordinata Y (in pianta) del filo fisso del pilastro
 FILO I codice del tipo di filo fisso per il nodo iniziale I
 FILO J codice del tipo di filo fisso per il nodo finale J
 nota: per i pilastri FILO I = FILO J
 ANG. valore , in gradi, dell' angolo di rotazione del
 pilastro intorno all' asse globale Z (verticale),
 positiva se antiorario.
 DXI scostamento DX del filo fisso rispetto all' asse
 baricentrico del pilastro nei nodi I e J
 DYI scostamento DY del filo fisso rispetto all' asse
 baricentrico del pilastro nei nodi I e J

=====

DATI DI INGRESSO : FILI FISSI TRAVI

ELEM.	SEZ	ZI	ZJ	FILO	DXI	DYI	DXJ	DYJ
n.ro	n.ro	(cm)	(cm)	I J	(cm)	(cm)	(cm)	(cm)
2	3	0.00	0.00	0 0	0.00	-0.00	0.00	-0.00
5	3	0.00	0.00	0 0	0.00	-0.00	0.00	-0.00
7	1	27.00	27.00	0 0	0.00	-0.00	0.00	-0.00
8	1	27.00	27.00	0 0	0.00	-0.00	0.00	-0.00
9	1	27.00	27.00	0 0	0.00	-0.00	0.00	-0.00
10	1	27.00	27.00	0 0	0.00	-0.00	0.00	-0.00
11	1	27.00	27.00	0 0	0.00	-0.00	0.00	-0.00
12	1	27.00	27.00	0 0	0.00	-0.00	0.00	-0.00
13	1	27.00	27.00	0 0	0.00	-0.00	0.00	-0.00
14	1	27.00	27.00	0 0	0.00	-0.00	0.00	-0.00
15	1	27.00	27.00	0 0	0.00	-0.00	0.00	-0.00
16	1	27.00	27.00	0 0	0.00	-0.00	0.00	-0.00
17	5	129.00	129.00	0 0	0.00	-0.00	0.00	-0.00
18	5	129.00	129.00	0 0	0.00	-0.00	0.00	-0.00
19	5	129.00	129.00	0 0	0.00	-0.00	0.00	-0.00
20	5	129.00	129.00	0 0	0.00	-0.00	0.00	-0.00
21	5	129.00	129.00	0 0	0.00	-0.00	0.00	-0.00

65	3	0.00	200.00	0	0	0.00	0.00	0.00
67	3	0.00	200.00	0	0	0.00	0.00	0.00
68	3	0.00	300.00	0	0	0.00	0.00	0.00
70	3	0.00	300.00	0	0	0.00	0.00	0.00
91	2	0.00	210.00	0	0	0.00	0.00	0.00
92	2	0.00	220.00	0	0	0.00	0.00	0.00
93	2	0.00	230.00	0	0	0.00	0.00	0.00
94	2	0.00	240.00	0	0	0.00	0.00	0.00
95	2	0.00	250.00	0	0	0.00	0.00	0.00
96	2	0.00	260.00	0	0	0.00	0.00	0.00
97	2	0.00	270.00	0	0	0.00	0.00	0.00
98	2	0.00	280.00	0	0	0.00	0.00	0.00
99	2	0.00	290.00	0	0	0.00	0.00	0.00
100	2	0.00	390.00	0	0	0.00	0.00	0.00
101	2	0.00	380.00	0	0	0.00	0.00	0.00
102	2	0.00	370.00	0	0	0.00	0.00	0.00
103	2	0.00	360.00	0	0	0.00	0.00	0.00
104	2	0.00	350.00	0	0	0.00	0.00	0.00
105	2	0.00	340.00	0	0	0.00	0.00	0.00
106	2	0.00	330.00	0	0	0.00	0.00	0.00
107	2	0.00	320.00	0	0	0.00	0.00	0.00
108	2	0.00	310.00	0	0	0.00	0.00	0.00
129	3	0.00	400.00	0	0	0.00	0.00	0.00
131	3	0.00	400.00	0	0	0.00	0.00	0.00
132	3	0.00	500.00	0	0	0.00	0.00	0.00
134	3	0.00	500.00	0	0	0.00	0.00	0.00
155	2	0.00	410.00	0	0	0.00	0.00	0.00
156	2	0.00	420.00	0	0	0.00	0.00	0.00
157	2	0.00	430.00	0	0	0.00	0.00	0.00
158	2	0.00	440.00	0	0	0.00	0.00	0.00
159	2	0.00	450.00	0	0	0.00	0.00	0.00
160	2	0.00	460.00	0	0	0.00	0.00	0.00
161	2	0.00	470.00	0	0	0.00	0.00	0.00
162	2	0.00	480.00	0	0	0.00	0.00	0.00
163	2	0.00	490.00	0	0	0.00	0.00	0.00

=====

DATI DI INGRESSO : MACRO ELEMENTI

=====

N.RO TRAVATE : 8

N.RO PILASTRATE : 51

=====

DATI DI INGRESSO : MACRO ELEMENTI

=====

TRAVATA n.ro	COMPOSIZIONE									
1	2									
2	5									
3	66									
4	69									
5	130									
6	133									
7	7 -	8 -	9 -	10 -	11 -	12 -	13 -			
	14 -	15 -	16 -	64 -	63 -	62 -	61 -	60 -		
	59 -	58 -	57 -	56 -	55 -	71 -	72 -	73 -		
	74 -	75 -	76 -	77 -	78 -	79 -	80 -	128 -		
	127 -	126 -	125 -	124 -	123 -	122 -	121 -	120 -		
	119 -	135 -	136 -	137 -	138 -	139 -	140 -	141 -		
	142 -	143 -	144							
8	17 -	18 -	19 -	20 -	21 -	22 -	23 -			
	24 -	25 -	26 -	54 -	53 -	52 -	51 -	50 -		
	49 -	48 -	47 -	46 -	45 -	81 -	82 -	83 -		
	84 -	85 -	86 -	87 -	88 -	89 -	90 -	118 -		
	117 -	116 -	115 -	114 -	113 -	112 -	111 -	110 -		
	109 -	145 -	146 -	147 -	148 -	149 -	150 -	151 -		
	152 -	153 -	154							

=====

DATI DI INGRESSO : MACRO ELEMENTI

=====

PILASTRATA COMPOSIZIONE

n.ro

1	1 -	3
2	27	
3	28	
4	29	
5	30	
6	31	
7	32	
8	33	
9	34	
10	35	
11	6 -	4
12	44	
13	43	
14	42	
15	41	
16	40	
17	39	
18	38	
19	37	
20	36	
21	65 -	67
22	91	
23	92	
24	93	
25	94	
26	95	
27	96	
28	97	
29	98	
30	99	
31	70 -	68
32	108	
33	107	
34	106	
35	105	
36	104	
37	103	
38	102	
39	101	
40	100	
41	129 -	131
42	155	

```

43      156
44      157
45      158
46      159
47      160
48      161
49      162
50      163
51      134 - 132

```

DESCRIZIONE TABELLA DATI SEZIONI PRISMATICHE

Di seguito si riportano le spiegazioni delle sigle usate nelle tabelle DATI SEZIONI PRISMATICHE. Le tipologie previste sono:

- | | | |
|----------------------|---------------|---------------------|
| 1. Rettangolare | 5. a T | 9. ad U |
| 2. Rettangolare cava | 6. a doppio T | 10. Poligonale |
| 3. Circolare | 7. a croce | 11. Poligonale cava |
| 4. Circolare cava | 8. ad L | |

Le sezioni sono riferite al sistema di riferimento 'locale', nel piano trasversale di travi, pilastri ed aste (assi locali 2, 3). Nelle tabelle sono usate sigle il cui significato e' illustrato nella documentazione fornita con il programma.

Aree ed inerzie sono nel rif. locale:

```

AREA  area della sezione
JT    inerzia torsionale
J2    inerzia flessionale intorno asse 2
J3    inerzia flessionale intorno asse 3
W2/Z2 modulo resistenza elastico/plastico intorno asse 2
W3/Z3 modulo resistenza elastico/plastico intorno asse 3

```

Le 'basi' (b,bi,...) sono parallele all'asse locale 3 della sez.
Le 'altezze' (h,ht,..) sono parallele all'asse locale 2 della sez.
Le sezioni poligonali sono descritte con le coordinate, rispetto agli assi locali 2 e 3, dei vertici della sezione.

DATI DI INGRESSO : TABELLA DATI SEZIONI PRISMATICHE

SEZIONI "RETTANGOLARI"

SEZ. n.ro	b (cm)	h (cm)	rot (gradi)
1	5.0	1.0	0.0
2	1.0	1.0	0.0
4	6.0	1.0	0.0

DATI DI INGRESSO : TABELLA DATI SEZIONI PRISMATICHE

SEZIONI "RETTANGOLARI CAVE"

SEZ. n.ro	b (cm)	h (cm)	bi (cm)	hi (cm)	rot (gradi)
3	6.0	6.0	4.8	4.8	0.0
5	6.0	5.0	5.0	4.0	0.0

DATI DI INGRESSO : SEZIONI

```

SEZ.
n.ro
1  RETT. b=5.  h=1.
2  RETT. b=1.  h=1.
3  RC 6x6/4.8x4.8
4  RETT. b=6.  h=1.
5  RC 6x5/5x4

```

DATI DI INGRESSO : AREE ED INERZIE NEL RIFERIMENTO LOCALE

SEZ. n.ro	AREA (cm2)	J2 (cm4)	J3 (cm4)	JT (cm4)	W2 (cm3)	W3 (cm3)	Z2 (cm3)	Z3 (cm3)
1	5.0	10	0	1	4.2	0.8	6.3	1.3
2	1.0	0	0	0	0.2	0.2	0.3	0.3
3	13.0	64	64	94	21.3	21.3	26.4	26.4
4	6.0	18	1	2	6.0	1.0	9.0	1.5
5	10.0	48	36	61	16.1	14.3	20.0	17.5

DESCRIZIONE TABELLA DATI MATERIALI

Di seguito si riportano le spiegazioni delle sigle usate nelle tabelle DATI MATERIALI.

```

MAT. n.ro    numero identificativo del materiale  ( >= 1 )
PESO SPEC.   peso dell' unita' di volume del materiale
ALFA T       coefficiente di dilatazione termica
E            modulo di elasticita'
POISSON      coefficiente di contrazione laterale impedita
NOME         descrizione del materiale  ( max. 11 caratteri)

```

DATI DI INGRESSO : TABELLA DATI MATERIALI

MAT. n.ro	PESO SPEC. (Kg/cm3)	ALFA T (1/C)	E (Kg/cm2)	POISSON	NOME
1	0.00785	0.000010	2100000.0	0.3	acciaio

DESCRIZIONE TABELLE DATI CARICHI

I carichi sono organizzati in 'condizioni di carico, a loro volta suddivise in:
1) casi di carico
2) combinazioni dei casi di carico
Nell' ambito di una generica condizione di carico possono esserci:
- carichi nodali (compresi cedimenti, variazioni termiche nodali)
- carichi sugli elementi (comprese variazioni termiche)

TABELLA DATI CASI DI CARICO E COMBINAZIONI

CASO	numero del caso di carico
n.ro	
DESCRIZIONE	descrizione sintetica del caso di carico
COMB.	numero della combinazione del caso di carico
n.ro	
DESCRIZIONE	composizione della combinazione; per ogni caso di carico coinvolto nella combinazione, viene riportato il relativo numero ed il valore del coefficiente moltiplicativo ('peso del caso di carico nella combinazione) .

CASI DI CARICO

CASO n.ro	DESCRIZIONE
1	c.d.c. 1 peso proprio
2	c.d.c. 2: permanente
3	c.d.c. 3: sovraccarico

COMB. n.ro	DESCRIZIONE
---------------	-------------

```
1      1*1.3 + 2*1.3 + 3*1.5
2      1*1 + 2*1 + 3*1
3      1*1 + 2*1 + 3*0.5
4      1*1 + 2*1 + 3*0.3
```

Di seguito si riportano le spiegazioni delle sigle usate nella tabella DATI CARICHI NODALI.

Relativamente ad ogni caso di carico, sono elencate, per ogni nodo non completamente vincolato, i valori delle 6 componenti di carico (3 forze e 3 momenti) riferite alla terna globale:

NODO	numero del nodo di applicazione del carico				
n.ro					
Fx	componente della forza in direzione				X
Fy					Y
Fz					Z
Mx	componente del momento in direzione				X
My					Y
Mz					Z

Nota: per componente del momento in una direzione, si intende la componente del vettore asse-momento in quella direzione.
La componente F_x della forza e' positiva se concorde con l'asse X ; analogamente per F_y , F_z .
La componente M_x del momento e' positiva se concorde con l'asse X ; analogamente per M_y , M_z .

Di seguito si riportano le spiegazioni delle sigle usate nella tabella DATI CEDIMENTI NODALI.

NODO	numero del nodo di applicazione del cedimento					
n.ro						
Tx	componente	del	cedimento	lineare	in	X
Ty						Y
Tz						Z
Rx	componente	del	cedimento	angolare	intorno ad	X
Ry						Y
Rz						Z

Di seguito si riportano le spiegazioni delle sigle usate nella tabella DATI CARICHI TRAVI E PILASTRI. Relativamente ad ogni caso di carico, vengono elencate, per ogni trave, le seguenti grandezze:

ELEM./	numero dell' elemento						
TRATTO	numero del tratto di carico sull' elemento						
x _i	ascissa del 1° estremo del tratto di carico						
x _f		2°					
Fx _i	componente della forza in direzione X nel 1° estremo						
Fy _i					Y		
Fz _i					Z		
Fx _f	componente della forza in direzione X nel 2° estremo						
Fy _f					Y		
Fz _f					Z		
Mx _i	componente del momento in direzione X nel 1° estremo						
My _i					Y		
Mz _i					Z		
Mx _f	componente del momento in direzione X nel 2° estremo						
My _f					Y		
Mz _f					Z		

Nota: Quando, in stampa, appare la lettera 'L' (i.e. locale) accanto ad numero del tratto di carico, significa che i carichi sono espressi nel riferimento locale; pertanto in tal caso i simboli hanno il seguente significato:

Fxi	componente della forza in direzione	1	nel 1o	estremo
Fyi	"	2	"	"
Fzi	"	3	"	"
Fxf	componente della forza in direzione	1	nel 2o	estremo
Fyf	"	2	"	"
Fzf	"	3	"	"
Mxi	componente del momento in direzione	1	nel 1o	estremo
Mvi	"	2	"	"

TABELLA DATI CARICHI TERMICI NODALI

NODO	numero del nodo
n.ro	
Temp	temperatura del nodo in gradi centigradi

Di seguito si riportano le spiegazioni delle sigle usate nella tabella DATI CARICHI TERMICI TRAVI E PILASTRI. Relativamente ad ogni caso di carico termico, vengono elencate per ogni trave, le seguenti grandezze:

ELEM.	numero dell' elemento									
DT uniforme	delta T costante sull' intero elemento									
DT nodo I	delta T nel nodo I									
DT nodo J	delta T nel nodo J									
DT da 2- a 2+ nodo I	delta T nel nodo I lungo l' asse locale 2									
DT da 2- a 2+ nodo J						J				
DT da 3- a 3+ nodo I						I				3
DT da 3- a 3+ nodo J						J				

Di seguito si riportano le spiegazioni delle sigle usate nella tabella DATI CARICHI TERMICI SETTI.

Relativamente ad ogni caso di carico, vengono elencate, per ogni trave, le seguenti grandezze:

ELEM.	numero dell' elemento sotto
DT uniforme	variazione di temperatura uniforme sull' elemento
DT spessore	variazione di temperatura lineare dall'intradosso all' estradosso dell' elemento.

ELEM/ TRATTO	xi xf	Fxi Fxf	Fyi Fyf	Fzi Fzf	Mxi Mxf	Myi Myf	Mzi Mzf
n.ro	(m)	(Kg/m)	(Kg/m)	(Kg/m)	(Kgmm/m)	(Kgmm/m)	(Kgmm/m)
2/ 1	0.00	0.00	0.00	-10.17	0.00	0.00	0.00
	0.04	0.00	0.00	-10.17	0.00	0.00	0.00
5/ 1	0.00	0.00	0.00	-10.17	0.00	0.00	0.00
	0.04	0.00	0.00	-10.17	0.00	0.00	0.00
7/ 1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
	0.10	0.00	0.00	-3.92	0.00	0.00	0.00
8/ 1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
	0.10	0.00	0.00	-3.92	0.00	0.00	0.00
9/ 1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
	0.10	0.00	0.00	-3.92	0.00	0.00	0.00
10/ 1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
	0.10	0.00	0.00	-3.92	0.00	0.00	0.00
11/ 1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
	0.10	0.00	0.00	-3.92	0.00	0.00	0.00
12/ 1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
	0.10	0.00	0.00	-3.92	0.00	0.00	0.00
13/ 1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
	0.10	0.00	0.00	-3.92	0.00	0.00	0.00
14/ 1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
	0.10	0.00	0.00	-3.92	0.00	0.00	0.00
15/ 1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
	0.10	0.00	0.00	-3.92	0.00	0.00	0.00
16/ 1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
	0.10	0.00	0.00	-3.92	0.00	0.00	0.00
17/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
18/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
19/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
20/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
21/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
22/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
23/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
24/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
25/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
26/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
45/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
46/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
47/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
48/ 1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
	0.10	0.00	0.00	-7.85	0.00	0.00	0.00
49/ 1	0.00	0.00					

[illegible]

		0.10	0.00	0.00	-3.92	0.00	0.00	0.00
143/	1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
		0.10	0.00	0.00	-3.92	0.00	0.00	0.00
144/	1	0.00	0.00	0.00	-3.92	0.00	0.00	0.00
		0.10	0.00	0.00	-3.92	0.00	0.00	0.00
145/	1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
		0.10	0.00	0.00	-7.85	0.00	0.00	0.00
146/	1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
		0.10	0.00	0.00	-7.85	0.00	0.00	0.00
147/	1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
		0.10	0.00	0.00	-7.85	0.00	0.00	0.00
148/	1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
		0.10	0.00	0.00	-7.85	0.00	0.00	0.00
149/	1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
		0.10	0.00	0.00	-7.85	0.00	0.00	0.00
150/	1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
		0.10	0.00	0.00	-7.85	0.00	0.00	0.00
151/	1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
		0.10	0.00	0.00	-7.85	0.00	0.00	0.00
152/	1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
		0.10	0.00	0.00	-7.85	0.00	0.00	0.00
153/	1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
		0.10	0.00	0.00	-7.85	0.00	0.00	0.00
154/	1	0.00	0.00	0.00	-7.85	0.00	0.00	0.00
		0.10	0.00	0.00	-7.85	0.00	0.00	0.00

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DATI DI INGRESSO : TABELLA CARICHI TRAVI CASO DI CARICO 3

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		0.10	-200.00	0.00	0.00	0.00	0.00	0.00
147/	1	0.00	-200.00	0.00	0.00	0.00	0.00	0.00
		0.10	-200.00	0.00	0.00	0.00	0.00	0.00
148/	1	0.00	-200.00	0.00	0.00	0.00	0.00	0.00
		0.10	-200.00	0.00	0.00	0.00	0.00	0.00
149/	1	0.00	-200.00	0.00	0.00	0.00	0.00	0.00
		0.10	-200.00	0.00	0.00	0.00	0.00	0.00
150/	1	0.00	-200.00	0.00	0.00	0.00	0.00	0.00
		0.10	-200.00	0.00	0.00	0.00	0.00	0.00
151/	1	0.00	-200.00	0.00	0.00	0.00	0.00	0.00
		0.10	-200.00	0.00	0.00	0.00	0.00	0.00
152/	1	0.00	-200.00	0.00	0.00	0.00	0.00	0.00
		0.10	-200.00	0.00	0.00	0.00	0.00	0.00
153/	1	0.00	-200.00	0.00	0.00	0.00	0.00	0.00
		0.10	-200.00	0.00	0.00	0.00	0.00	0.00
154/	1	0.00	-200.00	0.00	0.00	0.00	0.00	0.00
		0.10	-200.00	0.00	0.00	0.00	0.00	0.00

DESCRIZIONE TABELLA SPOSTAMENTI E ROTAZIONI NODALI

Di seguito si riportano le spiegazioni delle sigle usate nella tabella SPOSTAMENTI E ROTAZIONI NODALI. Relativamente ad ogni condizione di carico esaminata, vengono elencati per ogni nodo non completamente vincolato, i valori delle 6 componenti di spostamento (3 traslazioni e 3 rotazioni) riferite alla terna globale.

NODO : Numero identificativo del nodo

n.ro

Tx : spostamento del nodo in direzione X

Ty : ' ' ' ' ' ' Y

Tz : ' ' ' ' ' ' Z

Rx : rotazione del nodo intorno all' asse X

Ry : ' ' ' ' ' ' Y

Rz : ' ' ' ' ' ' Z

Nota : sistema di riferimento globale

Il sistema di riferimento impiegato, per nodi ed elementi e tutti gli altri dati strutturali, e' una terna cartesiana XYZ destra. Si assume che l' asse Z sia verticale ed orientato verso l'alto.

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RISULTATI : CASO DI CARICO 1 : SPOSTAMENTI E ROTAZIONI NODALI

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NODO n.ro	Tx (cm)	Ty (cm)	Tz (cm)	Rx (gradi)	Ry (gradi)	Rz (gradi)
1	-0.0000	0.0000	-0.0000	0.0000	-0.0001	-0.0000
2	-0.0000	-0.0000	-0.0000	0.0002	-0.0001	0.0000
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	-0.0002	0.0000	-0.0001	-0.0012	-0.0001	0.0000
5	-0.0001	-0.0000	-0.0000	0.0000	-0.0001	0.0000
6	-0.0002	0.0000	-0.0001	0.0001	-0.0001	0.0000
7	0.0000	-0.0000	-0.0000	0.0000	-0.0001	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
9	-0.0000	-0.0000	-0.0003	-0.0023	-0.0001	0.0000
10	-0.0000	-0.0000	-0.0007	-0.0017	-0.0001	0.0000
11	-0.0000	-0.0000	-0.0009	-0.0012	-0.0001	0.0000
12	-0.0000	-0.0000	-0.0011	-0.0005	-0.0001	0.0000
13	-0.0000	-0.0000	-0.0011	0.0002	-0.0001	0.0000
14	-0.0000	-0.0000	-0.0010	0.0009	-0.0001	0.0000
15	-0.0000	-0.0000	-0.0008	0.0013	-0.0001	0.0000
16	-0.0000	-0.0000	-0.0005	0.0015	-0.0001	0.0000
17	-0.0001	-0.0000	-0.0003	0.0017	-0.0001	0.0000
18	-0.0002	0.0000	-0.0003	-0.0017	-0.0001	0.0000
19	-0.0002	0.0000	-0.0006	-0.0016	-0.0001	0.0000
20	-0.0002	0.0000	-0.0009	-0.0012	-0.0001	0.0000
21	-0.0002	0.0000	-0.0010	-0.0005	-0.0001	0.0000
22	-0.0002	0.0000	-0.0011	0.0002	-0.0001	0.0000
23	-0.0002	0.0000	-0.0010	0.0009	-0.0001	0.0000
24	-0.0002	0.0000	-0.0007	0.0014	-0.0001	0.0000
25	-0.0002	0.0000	-0.0005	0.0015	-0.0001	0.0000
26	-0.0002	0.0000	-0.0002	0.0011	-0.0001	0.0000
27	-0.0001	-0.0000	-0.0002	0.0014	-0.0001	-0.0000
28	-0.0002	0.0000	-0.0002	0.0008	-0.0001	0.0000
29	-0.0001	-0.0000	-0.0004	0.0011	-0.0001	-0.0000
30	-0.0002	0.0000	-0.0004	0.0011	-0.0001	0.0000
31	-0.0001	-0.0000	-0.0006	0.0010	-0.0001	-0.0000
32	-0.0002	0.0000	-0.0006	0.0010	-0.0001	0.0000
33	-0.0001	-0.0000	-0.0007	0.0005	-0.0001	-0.0000
34	-0.0002	0.0000	-0.0007	0.0006	-0.0001	0.0000
35	-0.0001	-0.0000	-0.0008	-0.0000	-0.0001	-0.0000
36	-0.0002	0.0000	-0.0008	-0.0000	-0.0001	0.0000
37	-0.0001	-0.0000	-0.0007	-0.0006	-0.0001	-0.0000
38	-0.0002	0.0000	-0.0007	-0.0006	-0.0001	0.0000
39	-0.0001	-0.0000	-0.0006	-0.0010	-0.0001	0.0000
40	-0.0002	0.0000	-0.0006	-0.0010	-0.0001	0.0000
41	-0.0001	-0.0000	-0.0004	-0.0011	-0.0001	0.0000
42	-0.0002	0.0000	-0.0004	-0.0011	-0.0001	0.0000
43	-0.0001	-0.0000	-0.0002	-0.0013	-0.0001	0.0000
44	-0.0002	0.0000	-0.0002	-0.0008	-0.0001	0.0000
45	-0.0002	0.0000	-0.0001	-0.0000	-0.0001	0.0000
46	-0.0001	-0.0000	-0.0000	0.0000	-0.0001	0.0000
47	-0.0000	-0.0000	-0.0000	0.0000	-0.0001	0.0000
48	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
49	-0.0001	0.0000	-0.0000	-0.0000	-0.0001	-0.0000
50	-0.0002	-0.0000	-0.0001	0.0000	-0.0001	-0.0000
51	-0.0000	0.0000	-0.0000	-0.0000	-0.0001	-0.0000
52	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
53	-0.0001	-0.0000	-0.0002	-0.0014	-0.0001	0.0000
54	-0.0001	-0.0000	-0.0004	-0.0012	-0.0001	0.0000
55	-0.0001	-0.0000	-0.0006	-0.0010	-0.0001	0.0000
56	-0.0001	-0.0000	-0.0008	-0.0006	-0.0001	0.0000
57	-0.0001	0.0000	-0.0008	0.0000	-0.0001	0.0000
58	-0.0001	0.0000	-0.0008	0.0006	-0.0001	-0.0000
59	-0.0001	0.0000	-0.0006	0.0010	-0.0001	-0.0000
60	-0.0001	0.0000	-0.0004	0.0012	-0.0001	-0.0000
61	-0.0001	0.0000	-0.0002	0.0014	-0.0001	-0.0000
62	-0.0002	0.0000	-0.0002	-0.0009	-0.0001	0.0000
63	-0.0002	0.0000	-0.0004	-0.0012	-0.0001	0.0000
64	-0.0002	0.0000	-0.0006	-0.0010	-0.0001	0.0000
65	-0.0002	0.0000	-0.0007	-0.0006	-0.0001	0.0000
66	-0.0002	0.0000	-0.0008	0.0000	-0.0001	0.0000
67	-0.0002	-0.0000	-0.0007	0.0006	-0.0001	-0.0000
68	-0.0002	-0.0000	-0.0006	0.0010	-0.0001	-0.0000
69	-0.0002	-0.0000	-0.0004	0.0012	-0.0001	-0.0000
70	-0.0002	-0.0000	-0.0002	0.0009	-0.0001	-0.0000

RISULTATI : CASO DI CARICO 2 : SPOSTAMENTI E ROTAZIONI NODALI

[illegible]

68	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
69	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
70	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
71	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
72	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
73	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
74	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
75	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
76	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
77	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
78	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
79	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
80	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
81	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
82	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
83	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
84	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
85	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
86	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
87	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
88	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
89	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
90	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
91	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
92	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
93	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
94	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
95	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
96	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
97	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
98	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
99	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
100	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
101	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
102	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
103	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
104	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
105	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
106	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
107	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
108	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
109	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
110	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
111	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
112	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
113	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
114	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
=====						
RISULTATI : CASO DI CARICO 3 : SPOSTAMENTI E ROTAZIONI NODALI						
=====						
NODO n.ro	Tx (cm)	Ty (cm)	Tz (cm)	Rx (gradi)	Ry (gradi)	Rz (gradi)
1	-0.0000	-0.0001	-0.0010	-0.0000	-0.0285	0.0023
2	-0.0559	-0.0000	-0.0010	-0.0001	-0.2027	0.0295
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	-0.7788	0.0000	-0.0010	-0.0001	-0.5196	0.1548
5	-0.0758	-0.0000	-0.0014	-0.0000	-0.2732	0.0149
6	-1.0129	0.0000	-0.0014	-0.0001	-0.6471	0.0935
7	-0.0000	-0.0000	-0.0014	-0.0000	-0.0389	0.0012
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
9	-0.0604	-0.0000	-0.0010	-0.0002	-0.2391	0.0223
10	-0.0638	-0.0000	-0.0010	-0.0002	-0.2682	0.0164
11	-0.0662	-0.0000	-0.0011	-0.0002	-0.2910	0.0117
12	-0.0679	-0.0000	-0.0011	-0.0003	-0.3080	0.0082
13	-0.0692	-0.0000	-0.0012	-0.0003	-0.3191	0.0060
14	-0.0701	-0.0000	-0.0012	-0.0003	-0.3243	0.0051
15	-0.0710	-0.0000	-0.0013	-0.0002	-0.3232	0.0055
16	-0.0721	-0.0000	-0.0013	-0.0002	-0.3150	0.0072
17	-0.0736	-0.0000	-0.0013	-0.0002	-0.2988	0.0103
18	-0.8064	0.0000	-0.0010	-0.0001	-0.5322	0.1608
19	-0.8346	0.0000	-0.0010	-0.0002	-0.5448	0.1611
20	-0.8624	0.0000	-0.0011	-0.0002	-0.5575	0.1569
21	-0.8892	0.0000	-0.0011	-0.0003	-0.5702	0.1492
22	-0.9143	0.0000	-0.0012	-0.0003	-0.5829	0.1392
23	-0.9377	0.0000	-0.0012	-0.0003	-0.5957	0.1279
24	-0.9590	0.0000	-0.0013	-0.0002	-0.6085	0.1166
25	-0.9784	0.0000	-0.0013	-0.0002	-0.6214	0.1064
26	-0.9963	0.0000	-0.0013	-0.0002	-0.6343	0.0983
27	-0.0832	-0.0000	-0.0015	-0.0000	-0.3365	0.0023
28	-1.1142	0.0000	-0.0015	-0.0000	-0.7078	0.0270
29	-0.0829	-0.0000	-0.0015	-0.0001	-0.3610	0.0012
30	-1.1091	0.0000	-0.0015	-0.0001	-0.7010	0.0316
31	-0.0827	-0.0000	-0.0015	-0.0001	-0.3764	0.0008
32	-1.1030	0.0000	-0.0015	-0.0001	-0.6941	0.0396
33	-0.0825	-0.0000	-0.0015	-0.0001	-0.3840	0.0011
34	-1.0952	0.0000	-0.0015	-0.0001	-0.6873	0.0497
35	-0.0823	-0.0000	-0.0014	-0.0001	-0.3842	0.0020
36	-1.0855	0.0000	-0.0014	-0.0001	-0.6805	0.0609
37	-0.0818	-0.0000	-0.0014	-0.0001	-0.3773	0.0036
38	-1.0739	0.0000	-0.0014	-0.0001	-0.6738	0.0721
39	-0.0810	-0.0000	-0.0014	-0.0001	-0.3634	0.0056
40	-1.0604	0.0000	-0.0014	-0.0001	-0.6671	0.0820
41	-0.0798	-0.0000	-0.0014	-0.0001	-0.3420	0.0083
42	-1.0454	0.0000	-0.0014	-0.0001	-0.6604	0.0896
43	-0.0781	-0.0000	-0.0014	-0.0001	-0.3123	0.0114
44	-1.0294	0.0000	-0.0014	-0.0001	-0.6538	0.0938
45	-1.1188	0.0000	-0.0015	-0.0000	-0.7147	0.0267
46	-0.0837	-0.0000	-0.0015	-0.0000	-0.3017	0.0042
47	-0.0000	-0.0000	-0.0015	-0.0000	-0.0430	0.0003
48	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
49	-0.0837	0.0000	-0.0015	0.0000	-0.3017	-0.0042
50	-1.1188	-0.0000	-0.0015	0.0000	-0.7147	-0.0267
51	-0.0000	0.0000	-0.0015	0.0000	-0.0430	-0.0003
52	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
53	-0.0844	-0.0000	-0.0015	-0.0000	-0.3402	0.0036
54	-0.0849	-0.0000	-0.0015	-0.0000	-0.3683	0.0028
55	-0.0854	-0.0000	-0.0015	-0.0000	-0.3875	0.0019
56	-0.0856	-0.0000	-0.0015	-0.0000	-0.3986	0.0010
57	-0.0857	0.0000	-0.0015	0.0000	-0.4023	-0.0000
58	-0.0856	0.0000	-0.0015	0.0000	-0.3986	-0.0010
59	-0.0854	0.0000	-0.0015	0.0000	-0.3875	-0.0019
60	-0.0849	0.0000	-0.0015	0.0000	-0.3683	-0.0028
61	-0.0844	0.0000	-0.0015	0.0000	-0.3402	-0.0036
62	-1.1237	0.0000	-0.0015	-0.0000	-0.7146	0.0281
63	-1.1284	0.0000	-0.0015	-0.0000	-0.7144	0.0250
64	-1.1322	0.0000	-0.0015	-0.0000	-0.7143	0.0185

65	-1.1347	0.0000	-0.0015	-0.0000	-0.7143	0.0098
66	-1.1356	-0.0000	-0.0015	0.0000	-0.7142	-0.0000
67	-1.1347	-0.0000	-0.0015	0.0000	-0.7143	-0.0098
68	-1.1322	-0.0000	-0.0015	0.0000	-0.7143	-0.0185
69	-1.1284	-0.0000	-0.0015	0.0000	-0.7144	-0.0250
70	-1.1237	-0.0000	-0.0015	0.0000	-0.7146	-0.0281
71	-0.0781	0.0000	-0.0014	0.0001	-0.3123	-0.0114
72	-1.0294	-0.0000	-0.0014	0.0001	-0.6538	-0.0938
73	-0.0798	0.0000	-0.0014	0.0001	-0.3420	-0.0083
74	-1.0454	-0.0000	-0.0014	0.0001	-0.6604	-0.0896
75	-0.0810	0.0000	-0.0014	0.0001	-0.3634	-0.0056
76	-1.0604	-0.0000	-0.0014	0.0001	-0.6671	-0.0820
77	-0.0818	0.0000	-0.0014	0.0001	-0.3773	-0.0036
78	-1.0739	-0.0000	-0.0014	0.0001	-0.6738	-0.0721
79	-0.0823	0.0000	-0.0014	0.0001	-0.3842	-0.0020
80	-1.0855	-0.0000	-0.0014	0.0001	-0.6805	-0.0609
81	-0.0825	0.0000	-0.0015	0.0001	-0.3840	-0.0011
82	-1.0952	-0.0000	-0.0015	0.0001	-0.6873	-0.0497
83	-0.0827	0.0000	-0.0015	0.0001	-0.3764	-0.0008
84	-1.1030	-0.0000	-0.0015	0.0001	-0.6941	-0.0396
85	-0.0829	0.0000	-0.0015	0.0001	-0.3610	-0.0012
86	-1.1091	-0.0000	-0.0015	0.0001	-0.7010	-0.0316
87	-0.0832	0.0000	-0.0015	0.0000	-0.3365	-0.0023
88	-1.1142	-0.0000	-0.0015	0.0000	-0.7078	-0.0270
89	-1.0129	-0.0000	-0.0014	0.0001	-0.6471	-0.0935
90	-0.0758	0.0000	-0.0014	0.0000	-0.2732	-0.0149
91	-0.0000	0.0000	-0.0014	0.0000	-0.0389	-0.0012
92	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
93	-0.0559	0.0000	-0.0010	0.0001	-0.2027	-0.0295
94	-0.7788	-0.0000	-0.0010	0.0001	-0.5196	-0.1548
95	-0.0000	0.0001	-0.0010	0.0000	-0.0285	-0.0023
96	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
97	-0.0736	0.0000	-0.0013	0.0002	-0.2988	-0.0103
98	-0.0721	0.0000	-0.0013	0.0002	-0.3150	-0.0072
99	-0.0710	0.0000	-0.0013	0.0002	-0.3232	-0.0055
100	-0.0701	0.0000	-0.0012	0.0003	-0.3243	-0.0051
101	-0.0692	0.0000	-0.0012	0.0003	-0.3191	-0.0060
102	-0.0679	0.0000	-0.0011	0.0003	-0.3080	-0.0082
103	-0.0662	0.0000	-0.0011	0.0002	-0.2910	-0.0117
104	-0.0638	0.0000	-0.0010	0.0002	-0.2682	-0.0164
105	-0.0604	0.0000	-0.0010	0.0002	-0.2391	-0.0223
106	-0.9963	-0.0000	-0.0013	0.0002	-0.6343	-0.0983
107	-0.9784	-0.0000	-0.0013	0.0002	-0.6214	-0.1064
108	-0.9590	-0.0000	-0.0013	0.0002	-0.6085	-0.1166
109	-0.9377	-0.0000	-0.0012	0.0003	-0.5957	-0.1279
110	-0.9143	-0.0000	-0.0012	0.0003	-0.5829	-0.1392
111	-0.8892	-0.0000	-0.0011	0.0003	-0.5702	-0.1492
112	-0.8624	-0.0000	-0.0011	0.0002	-0.5575	-0.1569
113	-0.8346	-0.0000	-0.0010	0.0002	-0.5448	-0.1611
114	-0.8064	-0.0000	-0.0010	0.0001	-0.5322	-0.1608

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RISULTATI : COMBINAZIONE 1 : SPOSTAMENTI E ROTAZIONI NODALI

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NODO n.ro	Tx (cm)	Ty (cm)	Tz (cm)	Rx (gradi)	Ry (gradi)	Rz (gradi)
1	-0.0000	-0.0001	-0.0015	-0.0001	-0.0428	0.0034
2	-0.0839	-0.0001	-0.0015	0.0001	-0.3042	0.0442
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	-1.1684	0.0000	-0.0016	-0.0017	-0.7795	0.2322
5	-0.1138	-0.0001	-0.0021	-0.0000	-0.4099	0.0224
6	-1.5197	0.0000	-0.0022	0.0000	-0.9708	0.1402
7	-0.0000	-0.0001	-0.0020	0.0000	-0.0585	0.0017
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
9	-0.0907	-0.0001	-0.0019	-0.0033	-0.3587	0.0335
10	-0.0957	-0.0001	-0.0024	-0.0025	-0.4025	0.0246
11	-0.0994	-0.0001	-0.0028	-0.0018	-0.4367	0.0176
12	-0.1020	-0.0001	-0.0031	-0.0011	-0.4621	0.0123
13	-0.1038	-0.0001	-0.0032	-0.0001	-0.4788	0.0090
14	-0.1052	-0.0001	-0.0031	0.0008	-0.4866	0.0076
15	-0.1066	-0.0001	-0.0029	0.0014	-0.4849	0.0082
16	-0.1082	-0.0001	-0.0026	0.0017	-0.4727	0.0108
17	-0.1105	-0.0001	-0.0023	0.0020	-0.4483	0.0155
18	-1.2099	0.0000	-0.0020	-0.0024	-0.7984	0.2412
19	-1.2522	0.0000	-0.0024	-0.0024	-0.8173	0.2417
20	-1.2939	0.0000	-0.0028	-0.0019	-0.8363	0.2353
21	-1.3340	0.0000	-0.0030	-0.0011	-0.8554	0.2238
22	-1.3718	0.0000	-0.0031	-0.0001	-0.8745	0.2087
23	-1.4068	0.0000	-0.0031	0.0008	-0.8937	0.1919
24	-1.4388	0.0000	-0.0029	0.0014	-0.9129	0.1750
25	-1.4679	0.0000	-0.0026	0.0017	-0.9322	0.1596
26	-1.4947	0.0000	-0.0023	0.0012	-0.9515	0.1475
27	-0.1248	-0.0000	-0.0025	0.0017	-0.5049	0.0035
28	-1.6716	0.0000	-0.0025	0.0010	-1.0619	0.0405
29	-0.1244	-0.0000	-0.0028	0.0014	-0.5416	0.0018
30	-1.6640	0.0000	-0.0027	0.0014	-1.0516	0.0475
31	-0.1241	-0.0000	-0.0030	0.0011	-0.5648	0.0012
32	-1.6547	0.0000	-0.0030	0.0012	-1.0413	0.0594
33	-0.1239	-0.0000	-0.0032	0.0006	-0.5761	0.0017
34	-1.6431	0.0000	-0.0031	0.0006	-1.0311	0.0746
35	-0.1235	-0.0000	-0.0032	-0.0002	-0.5764	0.0031
36	-1.6286	0.0000	-0.0032	-0.0002	-1.0209	0.0914
37	-0.1227	-0.0000	-0.0031	-0.0009	-0.5662	0.0053
38	-1.6112	0.0000	-0.0031	-0.0009	-1.0108	0.1081
39	-0.1216	-0.0000	-0.0029	-0.0014	-0.5452	0.0085
40	-1.5910	0.0000	-0.0028	-0.0015	-1.0008	0.1230
41	-0.1197	-0.0001	-0.0026	-0.0016	-0.5131	0.0124
42	-1.5684	0.0000	-0.0026	-0.0016	-0.9908	0.1345
43	-0.1172	-0.0001	-0.0023	-0.0019	-0.4686	0.0170
44	-1.5443	0.0000	-0.0023	-0.0012	-0.9808	0.1408
45	-1.6785	0.0000	-0.0024	-0.0001	-1.0722	0.0401
46	-0.1256	-0.0000	-0.0023	0.0000	-0.4527	0.0062
47	-0.0000	-0.0000	-0.0023	0.0000	-0.0646	0.0005
48	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
49	-0.1256	0.0000	-0.0023	-0.0000	-0.4527	-0.0062
50	-1.6785	-0.0000	-0.0024	0.0001	-1.0722	-0.0401
51	-0.0000	0.0000	-0.0023	-0.0000	-0.0646	-0.0005
52	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
53	-0.1266	-0.0000	-0.0025	-0.0019	-0.5105	0.0053
54	-0.1275	-0.0000	-0.0028	-0.0016	-0.5526	0.0042
55	-0.1281	-0.0000	-0.0031	-0.0013	-0.5814	0.0029
56	-0.1285	-0.0000	-0.0033	-0.0008	-0.5980	0.0015
57	-0.1286	0.0000	-0.0034	0.0000	-0.6035	-0.0000
58	-0.1285	0.0000	-0.0033	0.0008	-0.5980	-0.0015
59	-0.1281	0.0000	-0.0031	0.0013	-0.5814	-0.0029
60	-0.1275	0.0000	-0.0028	0.0016	-0.5526	-0.0042
61	-0.1266	0.0000	-0.0025	0.0019	-0.5105	-0.0053

62	-1.6858	0.0000	-0.0025	-0.0012	-1.0720	0.0422
63	-1.6929	0.0000	-0.0028	-0.0016	-1.0718	0.0375
64	-1.6986	0.0000	-0.0030	-0.0014	-1.0716	0.0278
65	-1.7024	0.0000	-0.0032	-0.0008	-1.0715	0.0147
66	-1.7037	-0.0000	-0.0033	0.0000	-1.0715	-0.0000
67	-1.7024	-0.0000	-0.0032	0.0008	-1.0715	-0.0147
68	-1.6986	-0.0000	-0.0030	0.0014	-1.0716	-0.0278
69	-1.6929	-0.0000	-0.0028	0.0016	-1.0718	-0.0375
70	-1.6858	-0.0000	-0.0025	0.0012	-1.0720	-0.0422
71	-0.1172	0.0001	-0.0023	0.0019	-0.4686	-0.0170
72	-1.5443	-0.0000	-0.0023	0.0012	-0.9808	-0.1408
73	-0.1197	0.0001	-0.0026	0.0016	-0.5131	-0.0124
74	-1.5684	-0.0000	-0.0026	0.0016	-0.9908	-0.1345
75	-0.1216	0.0000	-0.0029	0.0014	-0.5452	-0.0085
76	-1.5910	-0.0000	-0.0028	0.0015	-1.0008	-0.1230
77	-0.1227	0.0000	-0.0031	0.0009	-0.5662	-0.0053
78	-1.6112	-0.0000	-0.0031	0.0009	-1.0108	-0.1081
79	-0.1235	0.0000	-0.0032	0.0002	-0.5764	-0.0031
80	-1.6286	-0.0000	-0.0032	0.0002	-1.0209	-0.0914
81	-0.1239	0.0000	-0.0032	-0.0006	-0.5761	-0.0017
82	-1.6431	-0.0000	-0.0031	-0.0006	-1.0311	-0.0746
83	-0.1241	0.0000	-0.0030	-0.0011	-0.5648	-0.0012
84	-1.6547	-0.0000	-0.0030	-0.0012	-1.0413	-0.0594
85	-0.1244	0.0000	-0.0028	-0.0014	-0.5416	-0.0018
86	-1.6640	-0.0000	-0.0027	-0.0014	-1.0516	-0.0475
87	-0.1248	0.0000	-0.0025	-0.0017	-0.5049	-0.0035
88	-1.6716	-0.0000	-0.0025	-0.0010	-1.0619	-0.0405
89	-1.5197	-0.0000	-0.0022	-0.0000	-0.9708	-0.1402
90	-0.1138	0.0001	-0.0021	0.0000	-0.4099	-0.0224
91	-0.0000	0.0001	-0.0020	-0.0000	-0.0585	-0.0017
92	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
93	-0.0839	0.0001	-0.0015	-0.0001	-0.3042	-0.0442
94	-1.1684	-0.0000	-0.0016	0.0017	-0.7795	-0.2322
95	-0.0000	0.0001	-0.0015	0.0001	-0.0428	-0.0034
96	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
97	-0.1105	0.0001	-0.0023	-0.0020	-0.4483	-0.0155
98	-0.1082	0.0001	-0.0026	-0.0017	-0.4727	-0.0108
99	-0.1066	0.0001	-0.0029	-0.0014	-0.4849	-0.0082
100	-0.1052	0.0001	-0.0031	-0.0008	-0.4866	-0.0076
101	-0.1038	0.0001	-0.0032	0.0001	-0.4788	-0.0090
102	-0.1020	0.0001	-0.0031	0.0011	-0.4621	-0.0123
103	-0.0994	0.0001	-0.0028	0.0018	-0.4367	-0.0176
104	-0.0957	0.0001	-0.0024	0.0025	-0.4025	-0.0246
105	-0.0907	0.0001	-0.0019	0.0033	-0.3587	-0.0335
106	-1.4947	-0.0000	-0.0023	-0.0012	-0.9515	-0.1475
107	-1.4679	-0.0000	-0.0026	-0.0017	-0.9322	-0.1596
108	-1.4388	-0.0000	-0.0029	-0.0014	-0.9129	-0.1750
109	-1.4068	-0.0000	-0.0031	-0.0008	-0.8937	-0.1919
110	-1.3718	-0.0000	-0.0031	0.0001	-0.8745	-0.2087
111	-1.3340	-0.0000	-0.0030	0.0011	-0.8554	-0.2238
112	-1.2939	-0.0000	-0.0028	0.0019	-0.8363	-0.2353
113	-1.2522	-0.0000	-0.0024	0.0024	-0.8173	-0.2417
114	-1.2099	-0.0000	-0.0020	0.0024	-0.7984	-0.2412

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RISULTATI : COMBINAZIONE 2 : SPOSTAMENTI E ROTAZIONI NODALI

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NODO n.ro	Tx (cm)	Ty (cm)	Tz (cm)	Rx (gradi)	Ry (gradi)	Rz (gradi)
1	-0.0000	-0.0001	-0.0010	-0.0000	-0.0286	0.0023
2	-0.0560	-0.0001	-0.0010	0.0001	-0.2028	0.0295
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	-0.7790	0.0000	-0.0011	-0.0013	-0.5197	0.1548
5	-0.0758	-0.0000	-0.0014	-0.0000	-0.2733	0.0149
6	-1.0132	0.0000	-0.0015	0.0000	-0.6472	0.0935
7	-0.0000	-0.0000	-0.0014	0.0000	-0.0390	0.0012
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
9	-0.0605	-0.0001	-0.0013	-0.0025	-0.2392	0.0224
10	-0.0638	-0.0001	-0.0017	-0.0019	-0.2683	0.0164
11	-0.0663	-0.0001	-0.0020	-0.0014	-0.2911	0.0117
12	-0.0680	-0.0001	-0.0022	-0.0008	-0.3080	0.0082
13	-0.0692	-0.0001	-0.0023	-0.0000	-0.3192	0.0060
14	-0.0702	-0.0001	-0.0022	0.0006	-0.3244	0.0051
15	-0.0711	-0.0001	-0.0020	0.0011	-0.3233	0.0055
16	-0.0721	-0.0000	-0.0018	0.0013	-0.3151	0.0072
17	-0.0737	-0.0000	-0.0016	0.0015	-0.2989	0.0104
18	-0.8066	0.0000	-0.0013	-0.0018	-0.5323	0.1608
19	-0.8348	0.0000	-0.0017	-0.0018	-0.5449	0.1612
20	-0.8626	0.0000	-0.0020	-0.0014	-0.5575	0.1569
21	-0.8894	0.0000	-0.0022	-0.0008	-0.5702	0.1492
22	-0.9146	0.0000	-0.0022	-0.0000	-0.5830	0.1392
23	-0.9379	0.0000	-0.0022	0.0006	-0.5958	0.1279
24	-0.9592	0.0000	-0.0020	0.0012	-0.6086	0.1166
25	-0.9787	0.0000	-0.0018	0.0013	-0.6215	0.1064
26	-0.9965	0.0000	-0.0016	0.0010	-0.6344	0.0983
27	-0.0832	-0.0000	-0.0017	0.0013	-0.3366	0.0023
28	-1.1144	0.0000	-0.0017	0.0008	-0.7079	0.0270
29	-0.0829	-0.0000	-0.0019	0.0011	-0.3611	0.0012
30	-1.1094	0.0000	-0.0019	0.0011	-0.7011	0.0317
31	-0.0827	-0.0000	-0.0021	0.0009	-0.3765	0.0008
32	-1.1032	0.0000	-0.0020	0.0009	-0.6942	0.0396
33	-0.0826	-0.0000	-0.0022	0.0005	-0.3841	0.0011
34	-1.0954	0.0000	-0.0022	0.0005	-0.6874	0.0498
35	-0.0823	-0.0000	-0.0022	-0.0001	-0.3843	0.0020
36	-1.0858	0.0000	-0.0022	-0.0001	-0.6806	0.0609
37	-0.0818	-0.0000	-0.0022	-0.0007	-0.3775	0.0036
38	-1.0742	0.0000	-0.0021	-0.0007	-0.6739	0.0721
39	-0.0810	-0.0000	-0.0020	-0.0011	-0.3635	0.0056
40	-1.0607	0.0000	-0.0020	-0.0011	-0.6672	0.0820
41	-0.0798	-0.0000	-0.0018	-0.0012	-0.3421	0.0083
42	-1.0457	0.0000	-0.0018	-0.0012	-0.6605	0.0896
43	-0.0781	-0.0000	-0.0016	-0.0014	-0.3124	0.0114
44	-1.0296	0.0000	-0.0016	-0.0009	-0.6539	0.0938
45	-1.1191	0.0000	-0.0016	-0.0000	-0.7148	0.0267
46	-0.0838	-0.0000	-0.0015	0.0000	-0.3018	0.0042
47	-0.0000	-0.0000	-0.0015	0.0000	-0.0431	0.0003
48	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
49	-0.0838	0.0000	-0.0015	-0.0000	-0.3018	-0.0042
50	-1.1191	-0.0000	-0.0016	0.0000	-0.7148	-0.0267
51	-0.0000	0.0000	-0.0015	-0.0000	-0.0431	-0.0003
52	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
53	-0.0844	-0.0000	-0.0017	-0.0015	-0.3403	0.0036
54	-0.0850	-0.0000	-0.0019	-0.0012	-0.3684	0.0028
55	-0.0854	-0.0000	-0.0021	-0.0010	-0.3876	0.0019
56	-0.0857	-0.0000	-0.0023	-0.0006	-0.3987	0.0010
57	-0.0857	0.0000	-0.0023	0.0000	-0.4024	-0.0000
58	-0.0857	0.0000	-0.0023	0.0006	-0.3987	-0.0010

59	-0.0854	0.0000	-0.0021	0.0010	-0.3876	-0.0019
60	-0.0850	0.0000	-0.0019	0.0012	-0.3684	-0.0028
61	-0.0844	0.0000	-0.0017	0.0015	-0.3403	-0.0036
62	-1.1239	0.0000	-0.0017	-0.0009	-0.7147	0.0281
63	-1.1286	0.0000	-0.0019	-0.0012	-0.7145	0.0250
64	-1.1324	0.0000	-0.0021	-0.0011	-0.7144	0.0185
65	-1.1349	0.0000	-0.0023	-0.0006	-0.7144	0.0098
66	-1.1358	-0.0000	-0.0023	0.0000	-0.7144	-0.0000
67	-1.1349	-0.0000	-0.0023	0.0006	-0.7144	-0.0098
68	-1.1324	-0.0000	-0.0021	0.0011	-0.7144	-0.0185
69	-1.1286	-0.0000	-0.0019	0.0012	-0.7145	-0.0250
70	-1.1239	-0.0000	-0.0017	0.0009	-0.7147	-0.0281
71	-0.0781	0.0000	-0.0016	0.0014	-0.3124	-0.0114
72	-1.0296	-0.0000	-0.0016	0.0009	-0.6539	-0.0938
73	-0.0798	0.0000	-0.0018	0.0012	-0.3421	-0.0083
74	-1.0457	-0.0000	-0.0018	0.0012	-0.6605	-0.0896
75	-0.0810	0.0000	-0.0020	0.0011	-0.3635	-0.0056
76	-1.0607	-0.0000	-0.0020	0.0011	-0.6672	-0.0820
77	-0.0818	0.0000	-0.0022	0.0007	-0.3775	-0.0036
78	-1.0742	-0.0000	-0.0021	0.0007	-0.6739	-0.0721
79	-0.0823	0.0000	-0.0022	0.0001	-0.3843	-0.0020
80	-1.0858	-0.0000	-0.0022	0.0001	-0.6806	-0.0609
81	-0.0826	0.0000	-0.0022	-0.0005	-0.3841	-0.0011
82	-1.0954	-0.0000	-0.0022	-0.0005	-0.6874	-0.0498
83	-0.0827	0.0000	-0.0021	-0.0009	-0.3765	-0.0008
84	-1.1032	-0.0000	-0.0020	-0.0009	-0.6942	-0.0396
85	-0.0829	0.0000	-0.0019	-0.0011	-0.3611	-0.0012
86	-1.1094	-0.0000	-0.0019	-0.0011	-0.7011	-0.0317
87	-0.0832	0.0000	-0.0017	-0.0013	-0.3366	-0.0023
88	-1.1144	-0.0000	-0.0017	-0.0008	-0.7079	-0.0270
89	-1.0132	-0.0000	-0.0015	-0.0000	-0.6472	-0.0935
90	-0.0758	0.0000	-0.0014	0.0000	-0.2733	-0.0149
91	-0.0000	0.0000	-0.0014	-0.0000	-0.0390	-0.0012
92	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
93	-0.0560	0.0001	-0.0010	-0.0001	-0.2028	-0.0295
94	-0.07790	-0.0000	-0.0011	0.0013	-0.5197	-0.1548
95	-0.0000	0.0001	-0.0010	0.0000	-0.0286	-0.0023
96	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
97	-0.0737	0.0000	-0.0016	-0.0015	-0.2989	-0.0104
98	-0.0721	0.0000	-0.0018	-0.0013	-0.3151	-0.0072
99	-0.0711	0.0001	-0.0020	-0.0011	-0.3233	-0.0055
100	-0.0702	0.0001	-0.0022	-0.0006	-0.3244	-0.0051
101	-0.0692	0.0001	-0.0023	0.0000	-0.3192	-0.0060
102	-0.0680	0.0001	-0.0022	0.0008	-0.3080	-0.0082
103	-0.0663	0.0001	-0.0020	0.0014	-0.2911	-0.0117
104	-0.0638	0.0001	-0.0017	0.0019	-0.2683	-0.0164
105	-0.0605	0.0001	-0.0013	0.0025	-0.2392	-0.0224
106	-0.9965	-0.0000	-0.0016	-0.0010	-0.6344	-0.0983
107	-0.9787	-0.0000	-0.0018	-0.0013	-0.6215	-0.1064
108	-0.9592	-0.0000	-0.0020	-0.0012	-0.6086	-0.1166
109	-0.9379	-0.0000	-0.0022	-0.0006	-0.5958	-0.1279
110	-0.9146	-0.0000	-0.0022	0.0000	-0.5830	-0.1392
111	-0.8894	-0.0000	-0.0022	0.0008	-0.5702	-0.1492
112	-0.8626	-0.0000	-0.0020	0.0014	-0.5575	-0.1569
113	-0.8348	-0.0000	-0.0017	0.0018	-0.5449	-0.1612
114	-0.8066	-0.0000	-0.0013	0.0018	-0.5323	-0.1608

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RISULTATI : COMBINAZIONE 3 : SPOSTAMENTI E ROTAZIONI NODALI

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NODO n.ro	Tx (cm)	Ty (cm)	Tz (cm)	Rx (gradi)	Ry (gradi)	Rz (gradi)
1	-0.0000	-0.0000	-0.0005	-0.0000	-0.0143	0.0011
2	-0.0280	-0.0001	-0.0005	0.0001	-0.1014	0.0147
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	-0.3896	0.0000	-0.0006	-0.0012	-0.2599	0.0774
5	-0.0379	-0.0000	-0.0007	0.0000	-0.1367	0.0075
6	-0.5067	0.0000	-0.0008	0.0001	-0.3237	0.0468
7	-0.0000	-0.0000	-0.0007	0.0000	-0.0196	0.0006
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
9	-0.0302	-0.0001	-0.0008	-0.0024	-0.1196	0.0112
10	-0.0319	-0.0000	-0.0012	-0.0018	-0.1342	0.0082
11	-0.0332	-0.0000	-0.0015	-0.0013	-0.1456	0.0059
12	-0.0340	-0.0000	-0.0016	-0.0007	-0.1541	0.0041
13	-0.0346	-0.0000	-0.0017	0.0001	-0.1596	0.0030
14	-0.0351	-0.0000	-0.0016	0.0008	-0.1623	0.0026
15	-0.0356	-0.0000	-0.0014	0.0012	-0.1617	0.0027
16	-0.0361	-0.0000	-0.0012	0.0014	-0.1576	0.0036
17	-0.0369	-0.0000	-0.0009	0.0016	-0.1495	0.0052
18	-0.4034	0.0000	-0.0008	-0.0017	-0.2662	0.0804
19	-0.4175	0.0000	-0.0011	-0.0017	-0.2725	0.0806
20	-0.4314	0.0000	-0.0014	-0.0013	-0.2788	0.0785
21	-0.4448	0.0000	-0.0016	-0.0007	-0.2852	0.0746
22	-0.4574	0.0000	-0.0016	0.0001	-0.2915	0.0696
23	-0.4690	0.0000	-0.0016	0.0008	-0.2979	0.0640
24	-0.4797	0.0000	-0.0014	0.0013	-0.3044	0.0583
25	-0.4894	0.0000	-0.0011	0.0014	-0.3108	0.0532
26	-0.4984	0.0000	-0.0009	0.0011	-0.3172	0.0492
27	-0.0416	-0.0000	-0.0010	0.0013	-0.1684	0.0012
28	-0.5573	0.0000	-0.0009	0.0008	-0.3540	0.0135
29	-0.0415	-0.0000	-0.0012	0.0011	-0.1806	0.0006
30	-0.5548	0.0000	-0.0011	0.0011	-0.3506	0.0158
31	-0.0414	-0.0000	-0.0013	0.0009	-0.1883	0.0004
32	-0.5517	0.0000	-0.0013	0.0010	-0.3472	0.0198
33	-0.0413	-0.0000	-0.0015	0.0005	-0.1921	0.0006
34	-0.5478	0.0000	-0.0014	0.0005	-0.3438	0.0249
35	-0.0412	-0.0000	-0.0015	-0.0001	-0.1922	0.0010
36	-0.5430	0.0000	-0.0015	-0.0001	-0.3404	0.0305
37	-0.0409	-0.0000	-0.0015	-0.0006	-0.1888	0.0018
38	-0.5372	0.0000	-0.0014	-0.0006	-0.3370	0.0360
39	-0.0405	-0.0000	-0.0013	-0.0010	-0.1818	0.0028
40	-0.5305	0.0000	-0.0013	-0.0011	-0.3336	0.0410
41	-0.0399	-0.0000	-0.0011	-0.0012	-0.1711	0.0041
42	-0.5229	0.0000	-0.0011	-0.0012	-0.3303	0.0448
43	-0.0391	-0.0000	-0.0009	-0.0014	-0.1563	0.0057
44	-0.5149	0.0000	-0.0009	-0.0008	-0.3270	0.0469
45	-0.5596	0.0000	-0.0009	-0.0000	-0.3575	0.0134
46	-0.0419	-0.0000	-0.0008	0.0000	-0.1510	0.0021
47	-0.0000	-0.0000	-0.0008	0.0000	-0.0216	0.0002
48	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
49	-0.0419	0.0000	-0.0008	-0.0000	-0.1510	-0.0021
50	-0.5596	-0.0000	-0.0009	0.0000	-0.3575	-0.0134
51	-0.0000	0.0000	-0.0008	-0.0000	-0.0216	-0.0002
52	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
53	-0.0422	-0.0000	-0.0010	-0.0015	-0.1702	0.0018
54	-0.0425	-0.0000	-0.0012	-0.0012	-0.1843	0.0014
55	-0.0427	-0.0000	-0.0014	-0.0010	-0.1938	0.0010

56	-0.0429	-0.0000	-0.0015	-0.0006	-0.1994	0.0005
57	-0.0429	0.0000	-0.0016	0.0000	-0.2012	-0.0000
58	-0.0429	0.0000	-0.0015	0.0006	-0.1994	-0.0005
59	-0.0427	0.0000	-0.0014	0.0010	-0.1938	-0.0010
60	-0.0425	0.0000	-0.0012	0.0012	-0.1843	-0.0014
61	-0.0422	0.0000	-0.0010	0.0015	-0.1702	-0.0018
62	-0.5621	0.0000	-0.0010	-0.0009	-0.3574	0.0141
63	-0.5644	0.0000	-0.0012	-0.0012	-0.3573	0.0125
64	-0.5663	0.0000	-0.0014	-0.0010	-0.3573	0.0093
65	-0.5676	0.0000	-0.0015	-0.0006	-0.3572	0.0049
66	-0.5680	-0.0000	-0.0016	0.0000	-0.3572	-0.0000
67	-0.5676	-0.0000	-0.0015	0.0006	-0.3572	-0.0049
68	-0.5663	-0.0000	-0.0014	0.0010	-0.3573	-0.0093
69	-0.5644	-0.0000	-0.0012	0.0012	-0.3573	-0.0125
70	-0.5621	-0.0000	-0.0010	0.0009	-0.3574	-0.0141
71	-0.0391	0.0000	-0.0009	0.0014	-0.1563	-0.0057
72	-0.5149	-0.0000	-0.0009	0.0008	-0.3270	-0.0469
73	-0.0399	0.0000	-0.0011	0.0012	-0.1711	-0.0041
74	-0.5229	-0.0000	-0.0011	0.0012	-0.3303	-0.0448
75	-0.0405	0.0000	-0.0013	0.0010	-0.1818	-0.0028
76	-0.5305	-0.0000	-0.0013	0.0011	-0.3336	-0.0410
77	-0.0409	0.0000	-0.0015	0.0006	-0.1888	-0.0018
78	-0.5372	-0.0000	-0.0014	0.0006	-0.3370	-0.0360
79	-0.0412	0.0000	-0.0015	0.0001	-0.1922	-0.0010
80	-0.5430	-0.0000	-0.0015	0.0001	-0.3404	-0.0305
81	-0.0413	0.0000	-0.0015	-0.0005	-0.1921	-0.0006
82	-0.5478	-0.0000	-0.0014	-0.0005	-0.3438	-0.0249
83	-0.0414	0.0000	-0.0013	-0.0009	-0.1883	-0.0004
84	-0.5517	-0.0000	-0.0013	-0.0010	-0.3472	-0.0198
85	-0.0415	0.0000	-0.0012	-0.0011	-0.1806	-0.0006
86	-0.5548	-0.0000	-0.0011	-0.0011	-0.3506	-0.0158
87	-0.0416	0.0000	-0.0010	-0.0013	-0.1684	-0.0012
88	-0.5573	-0.0000	-0.0009	-0.0008	-0.3540	-0.0135
89	-0.5067	-0.0000	-0.0008	-0.0001	-0.3237	-0.0468
90	-0.0379	0.0000	-0.0007	-0.0000	-0.1367	-0.0075
91	-0.0000	0.0000	-0.0007	-0.0000	-0.0196	-0.0006
92	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
93	-0.0280	0.0001	-0.0005	-0.0001	-0.1014	-0.0147
94	-0.3896	-0.0000	-0.0006	0.0012	-0.2599	-0.0774
95	-0.0000	0.0000	-0.0005	0.0000	-0.0143	-0.0011
96	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
97	-0.0369	0.0000	-0.0009	-0.0016	-0.1495	-0.0052
98	-0.0361	0.0000	-0.0012	-0.0014	-0.1576	-0.0036
99	-0.0356	0.0000	-0.0014	-0.0012	-0.1617	-0.0027
100	-0.0351	0.0000	-0.0016	-0.0008	-0.1623	-0.0026
101	-0.0346	0.0000	-0.0017	-0.0001	-0.1596	-0.0030
102	-0.0340	0.0000	-0.0016	0.0007	-0.1541	-0.0041
103	-0.0332	0.0000	-0.0015	0.0013	-0.1456	-0.0059
104	-0.0319	0.0000	-0.0012	0.0018	-0.1342	-0.0082
105	-0.0302	0.0001	-0.0008	0.0024	-0.1196	-0.0112
106	-0.4984	-0.0000	-0.0009	-0.0011	-0.3172	-0.0492
107	-0.4894	-0.0000	-0.0011	-0.0014	-0.3108	-0.0532
108	-0.4797	-0.0000	-0.0014	-0.0013	-0.3044	-0.0583
109	-0.4690	-0.0000	-0.0016	-0.0008	-0.2979	-0.0640
110	-0.4574	-0.0000	-0.0016	-0.0001	-0.2915	-0.0696
111	-0.4448	-0.0000	-0.0016	0.0007	-0.2852	-0.0746
112	-0.4314	-0.0000	-0.0014	0.0013	-0.2788	-0.0785
113	-0.4175	-0.0000	-0.0011	0.0017	-0.2725	-0.0806
114	-0.4034	-0.0000	-0.0008	0.0017	-0.2662	-0.0804
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RISULTATI : COMBINAZIONE 4 : SPOSTAMENTI E ROTAZIONI NODALI						
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NODO n.ro	Tx (cm)	Ty (cm)	Tz (cm)	Rx (gradi)	Ry (gradi)	Rz (gradi)
1	-0.0000	-0.0000	-0.0003	-0.0000	-0.0086	0.0007
2	-0.0168	-0.0000	-0.0003	0.0002	-0.0609	0.0088
3	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
4	-0.2338	0.0000	-0.0004	-0.0012	-0.1560	0.0465
5	-0.0228	-0.0000	-0.0004	0.0000	-0.0821	0.0045
6	-0.3041	0.0000	-0.0005	0.0001	-0.1942	0.0281
7	-0.0000	-0.0000	-0.0004	0.0000	-0.0118	0.0004
8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
9	-0.0182	-0.0000	-0.0006	-0.0024	-0.0718	0.0067
10	-0.0192	-0.0000	-0.0010	-0.0017	-0.0806	0.0049
11	-0.0199	-0.0000	-0.0012	-0.0012	-0.0874	0.0035
12	-0.0204	-0.0000	-0.0014	-0.0006	-0.0925	0.0025
13	-0.0208	-0.0000	-0.0014	0.0001	-0.0958	0.0018
14	-0.0211	-0.0000	-0.0014	0.0008	-0.0974	0.0015
15	-0.0214	-0.0000	-0.0012	0.0013	-0.0971	0.0017
16	-0.0217	-0.0000	-0.0009	0.0014	-0.0946	0.0022
17	-0.0221	-0.0000	-0.0007	0.0017	-0.0897	0.0031
18	-0.2421	0.0000	-0.0006	-0.0017	-0.1597	0.0483
19	-0.2506	0.0000	-0.0009	-0.0017	-0.1635	0.0484
20	-0.2589	0.0000	-0.0012	-0.0013	-0.1673	0.0471
21	-0.2670	0.0000	-0.0014	-0.0006	-0.1711	0.0448
22	-0.2745	0.0000	-0.0014	0.0001	-0.1750	0.0418
23	-0.2815	0.0000	-0.0013	0.0008	-0.1788	0.0384
24	-0.2879	0.0000	-0.0011	0.0013	-0.1827	0.0350
25	-0.2938	0.0000	-0.0009	0.0015	-0.1865	0.0319
26	-0.2991	0.0000	-0.0006	0.0011	-0.1904	0.0295
27	-0.0250	-0.0000	-0.0007	0.0014	-0.1011	0.0007
28	-0.3345	0.0000	-0.0006	0.0008	-0.2125	0.0081
29	-0.0249	-0.0000	-0.0009	0.0011	-0.1084	0.0004
30	-0.3330	0.0000	-0.0008	0.0011	-0.2104	0.0095
31	-0.0249	-0.0000	-0.0011	0.0009	-0.1130	0.0002
32	-0.3311	0.0000	-0.0010	0.0010	-0.2083	0.0119
33	-0.0248	-0.0000	-0.0012	0.0005	-0.1153	0.0003
34	-0.3288	0.0000	-0.0012	0.0005	-0.2063	0.0149
35	-0.0247	-0.0000	-0.0012	-0.0000	-0.1154	0.0006
36	-0.3259	0.0000	-0.0012	-0.0000	-0.2043	0.0183
37	-0.0246	-0.0000	-0.0012	-0.0006	-0.1133	0.0011
38	-0.3224	0.0000	-0.0011	-0.0006	-0.2022	0.0216
39	-0.0243	-0.0000	-0.0010	-0.0010	-0.1091	0.0017
40	-0.3184	0.0000	-0.0010	-0.0010	-0.2002	0.0246
41	-0.0240	-0.0000	-0.0008	-0.0011	-0.1027	0.0025
42	-0.3139	0.0000	-0.0008	-0.0012	-0.1982	0.0269
43	-0.0235	-0.0000	-0.0006	-0.0014	-0.0938	0.0034
44	-0.3090	0.0000	-0.0006	-0.0008	-0.1962	0.0282
45	-0.3359	0.0000	-0.0006	-0.0000	-0.2145	0.0080
46	-0.0252	-0.0000	-0.0005	0.0000	-0.0906	0.0012
47	-0.0000	-0.0000	-0.0005	0.0000	-0.0130	0.0001
48	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
49	-0.0252	0.0000	-0.0005	-0.0000	-0.0906	-0.0012
50	-0.3359	-0.0000	-0.0006	0.0000	-0.2145	-0.0080
51	-0.0000	0.0000	-0.0005	-0.0000	-0.0130	-0.0001
52	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

53	-0.0254	-0.0000	-0.0007	-0.0014	-0.1022	0.0011
54	-0.0255	-0.0000	-0.0009	-0.0012	-0.1106	0.0008
55	-0.0257	-0.0000	-0.0011	-0.0010	-0.1164	0.0006
56	-0.0257	-0.0000	-0.0012	-0.0006	-0.1197	0.0003
57	-0.0258	0.0000	-0.0013	0.0000	-0.1208	-0.0000
58	-0.0257	0.0000	-0.0012	0.0006	-0.1197	-0.0003
59	-0.0257	0.0000	-0.0011	0.0010	-0.1164	-0.0006
60	-0.0255	0.0000	-0.0009	0.0012	-0.1106	-0.0008
61	-0.0254	0.0000	-0.0007	0.0014	-0.1022	-0.0011
62	-0.3373	0.0000	-0.0007	-0.0009	-0.2145	0.0084
63	-0.3388	0.0000	-0.0009	-0.0012	-0.2144	0.0075
64	-0.3399	0.0000	-0.0011	-0.0010	-0.2144	0.0056
65	-0.3407	0.0000	-0.0012	-0.0006	-0.2144	0.0030
66	-0.3409	-0.0000	-0.0013	0.0000	-0.2144	-0.0000
67	-0.3407	-0.0000	-0.0012	0.0006	-0.2144	-0.0030
68	-0.3399	-0.0000	-0.0011	0.0010	-0.2144	-0.0056
69	-0.3388	-0.0000	-0.0009	0.0012	-0.2144	-0.0075
70	-0.3373	-0.0000	-0.0007	0.0009	-0.2145	-0.0084
71	-0.0235	0.0000	-0.0006	0.0014	-0.0938	-0.0034
72	-0.3090	-0.0000	-0.0006	0.0008	-0.1962	-0.0282
73	-0.0240	0.0000	-0.0008	0.0011	-0.1027	-0.0025
74	-0.3139	-0.0000	-0.0008	0.0012	-0.1982	-0.0269
75	-0.0243	0.0000	-0.0010	0.0010	-0.1091	-0.0017
76	-0.3184	-0.0000	-0.0010	0.0010	-0.2002	-0.0246
77	-0.0246	0.0000	-0.0012	0.0006	-0.1133	-0.0011
78	-0.3224	-0.0000	-0.0011	0.0006	-0.2022	-0.0216
79	-0.0247	0.0000	-0.0012	0.0000	-0.1154	-0.0006
80	-0.3259	-0.0000	-0.0012	0.0000	-0.2043	-0.0183
81	-0.0248	0.0000	-0.0012	-0.0005	-0.1153	-0.0003
82	-0.3288	-0.0000	-0.0012	-0.0005	-0.2063	-0.0149
83	-0.0249	0.0000	-0.0011	-0.0009	-0.1130	-0.0002
84	-0.3311	-0.0000	-0.0010	-0.0010	-0.2083	-0.0119
85	-0.0249	0.0000	-0.0009	-0.0011	-0.1084	-0.0004
86	-0.3330	-0.0000	-0.0008	-0.0011	-0.2104	-0.0095
87	-0.0250	0.0000	-0.0007	-0.0014	-0.1011	-0.0007
88	-0.3345	-0.0000	-0.0006	-0.0008	-0.2125	-0.0081
89	-0.3041	-0.0000	-0.0005	-0.0001	-0.1942	-0.0281
90	-0.0228	0.0000	-0.0004	-0.0000	-0.0821	-0.0045
91	-0.0000	0.0000	-0.0004	-0.0000	-0.0118	-0.0004
92	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
93	-0.0168	0.0000	-0.0003	-0.0002	-0.0609	-0.0088
94	-0.2338	-0.0000	-0.0004	0.0012	-0.1560	-0.0465
95	-0.0000	0.0000	-0.0003	0.0000	-0.0086	-0.0007
96	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
97	-0.0221	0.0000	-0.0007	-0.0017	-0.0897	-0.0031
98	-0.0217	0.0000	-0.0009	-0.0014	-0.0946	-0.0022
99	-0.0214	0.0000	-0.0012	-0.0013	-0.0971	-0.0017
100	-0.0211	0.0000	-0.0014	-0.0008	-0.0974	-0.0015
101	-0.0208	0.0000	-0.0014	-0.0001	-0.0958	-0.0018
102	-0.0204	0.0000	-0.0014	0.0006	-0.0925	-0.0025
103	-0.0199	0.0000	-0.0012	0.0012	-0.0874	-0.0035
104	-0.0192	0.0000	-0.0010	0.0017	-0.0806	-0.0049
105	-0.0182	0.0000	-0.0006	0.0024	-0.0718	-0.0067
106	-0.2991	-0.0000	-0.0006	-0.0011	-0.1904	-0.0295
107	-0.2938	-0.0000	-0.0009	-0.0015	-0.1865	-0.0319
108	-0.2879	-0.0000	-0.0011	-0.0013	-0.1827	-0.0350
109	-0.2815	-0.0000	-0.0013	-0.0008	-0.1788	-0.0384
110	-0.2745	-0.0000	-0.0014	-0.0001	-0.1750	-0.0418
111	-0.2670	-0.0000	-0.0014	0.0006	-0.1711	-0.0448
112	-0.2589	-0.0000	-0.0012	0.0013	-0.1673	-0.0471
113	-0.2506	-0.0000	-0.0009	0.0017	-0.1635	-0.0484
114	-0.2421	-0.0000	-0.0006	0.0017	-0.1597	-0.0483

DESCRIZIONE TABELLA SOLLECITAZIONI TRAVI E PILASTRI

Di seguito si riportano le spiegazioni delle sigle usate nella tabella SOLLECITAZIONI TRAVI E PILASTRI.

Per ogni gruppo di elementi ed internamente ad esso, per ogni elemento ad esso appartenente ed in ogni condizione di carico considerata vengono riportate, secondo modalita' diverse da tipo a tipo di elemento, azioni e/o tensioni in punti caratteristici riferiti alla terna locale.

ELEM. numero dell' elemento
n.ro
x ascissa locale misurata dal nodo I al nodo J
N sforzo normale nel p.to x
V2 forza di taglio ' ' ' in direz. 2 locale
V3 forza di taglio ' ' ' ' ' 3 '
T momento torcente ' ' '
M2 momento flettente ' ' ' intorno asse 2 locale
M3 momento flettente ' ' ' ' ' 3 '

Per la descrizione delle convenzioni usate per il segno delle azioni interne, si rimanda alla documentazione fornita con il programma.

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RISULTATI : CASO DI CARICO 1 : SOLLECITAZIONI TRAVI

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ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
2	0.00	0.0	21.8	0.7	-0.0	-0.0	-0.0
2	0.04	0.0	22.2	0.7	-0.0	0.0	-0.9
5	0.00	-0.0	33.0	-0.6	-0.1	-0.0	0.0
5	0.04	-0.0	33.4	-0.6	-0.1	-0.0	-1.3
7	0.00	2.0	-1.3	-0.0	-0.0	0.0	-0.1
7	0.10	2.0	-0.9	-0.0	-0.0	0.0	0.0
8	0.00	2.0	-0.2	-0.0	-0.0	0.0	0.0
8	0.10	2.0	0.2	-0.0	-0.0	0.0	0.0
9	0.00	2.0	-0.2	-0.0	-0.0	0.0	0.0
9	0.10	2.0	0.2	-0.0	-0.0	0.0	0.0
10	0.00	2.1	-0.2	-0.0	-0.0	0.0	0.0
10	0.10	2.1	0.2	-0.0	-0.0	0.0	0.0
11	0.00	2.1	-0.2	-0.0	-0.0	0.0	0.0
11	0.10	2.1	0.2	-0.0	-0.0	0.0	0.0
12	0.00	2.1	-0.2	-0.0	-0.0	0.0	0.0
12	0.10	2.1	0.2	-0.0	-0.0	-0.0	0.0
13	0.00	2.0	-0.1	-0.0	-0.0	-0.0	0.0
13	0.10	2.0	0.3	-0.0	-0.0	-0.0	0.0

14	0.00	2.0	-0.1	-0.0	-0.0	-0.0	0.0
14	0.10	2.0	0.3	-0.0	-0.0	-0.0	-0.0
15	0.00	2.0	-0.2	-0.0	-0.0	-0.0	-0.0
15	0.10	2.0	0.2	-0.0	-0.0	-0.0	0.0
16	0.00	2.0	0.5	-0.0	-0.0	-0.0	0.0
16	0.10	2.0	0.9	-0.0	-0.0	-0.0	-0.1
17	0.00	-1.3	-7.4	-0.0	-0.0	0.0	-1.0
17	0.10	-1.3	-6.7	-0.0	-0.0	0.0	-0.3
18	0.00	-1.3	-6.5	-0.0	-0.0	0.0	-0.3
18	0.10	-1.3	-5.8	-0.0	-0.0	0.0	0.3
19	0.00	-1.3	-4.5	-0.0	-0.0	0.0	0.3
19	0.10	-1.3	-3.7	-0.0	-0.0	0.0	0.8
20	0.00	-1.3	-2.5	-0.0	-0.0	0.0	0.8
20	0.10	-1.3	-1.7	-0.0	-0.0	-0.0	1.0
21	0.00	-1.3	-0.6	-0.0	-0.0	-0.0	1.0
21	0.10	-1.3	0.2	-0.0	-0.0	-0.0	1.0
22	0.00	-1.3	1.4	-0.0	-0.0	-0.0	1.0
22	0.10	-1.3	2.1	-0.0	-0.0	-0.0	0.8
23	0.00	-1.3	3.3	-0.0	-0.0	-0.0	0.8
23	0.10	-1.3	4.1	-0.0	-0.0	-0.0	0.4
24	0.00	-1.3	5.3	-0.0	-0.0	-0.0	0.4
24	0.10	-1.3	6.1	-0.0	-0.0	-0.0	-0.1
25	0.00	-1.3	7.3	-0.0	-0.0	-0.0	-0.1
25	0.10	-1.3	8.1	-0.0	-0.0	-0.0	-0.9
26	0.00	-1.3	8.6	-0.0	-0.0	-0.0	-0.9
26	0.10	-1.3	9.4	-0.0	-0.0	-0.0	-1.8
45	0.00	-1.0	7.9	0.0	-0.0	-0.0	-0.7
45	0.10	-1.0	8.6	0.0	-0.0	-0.0	-1.6
46	0.00	-1.1	6.5	0.0	-0.0	-0.0	-0.1
46	0.10	-1.1	7.3	0.0	-0.0	-0.0	-0.7
47	0.00	-1.1	4.4	0.0	-0.0	-0.0	0.4
47	0.10	-1.1	5.2	0.0	-0.0	-0.0	-0.1
48	0.00	-1.1	2.4	0.0	-0.0	-0.0	0.7
48	0.10	-1.1	3.2	0.0	-0.0	-0.0	0.4
49	0.00	-1.1	0.5	0.0	-0.0	-0.0	0.8
49	0.10	-1.1	1.3	0.0	-0.0	-0.0	0.7
50	0.00	-1.1	-1.4	0.0	-0.0	-0.0	0.7
50	0.10	-1.1	-0.7	0.0	-0.0	-0.0	0.8
51	0.00	-1.1	-3.4	0.0	-0.0	-0.0	0.4
51	0.10	-1.1	-2.6	0.0	-0.0	-0.0	0.7
52	0.00	-1.1	-5.4	0.0	-0.0	-0.0	-0.1
52	0.10	-1.1	-4.6	0.0	-0.0	-0.0	0.4
53	0.00	-1.1	-7.4	0.0	-0.0	-0.0	-0.8
53	0.10	-1.1	-6.6	0.0	-0.0	-0.0	-0.1
54	0.00	-1.0	-8.8	0.0	-0.0	-0.0	-1.6
54	0.10	-1.0	-8.0	0.0	-0.0	-0.0	-0.8
55	0.00	1.2	0.4	0.0	-0.0	0.0	0.0
55	0.10	1.2	0.8	0.0	-0.0	0.0	-0.1
56	0.00	1.2	-0.2	0.0	-0.0	0.0	-0.0
56	0.10	1.2	0.2	0.0	-0.0	0.0	0.0
57	0.00	1.2	-0.1	0.0	-0.0	0.0	0.0
57	0.10	1.2	0.3	0.0	-0.0	0.0	-0.0
58	0.00	1.2	-0.1	0.0	-0.0	-0.0	0.0
58	0.10	1.2	0.2	0.0	-0.0	0.0	0.0
59	0.00	1.2	-0.2	0.0	-0.0	-0.0	0.0
59	0.10	1.2	0.2	0.0	-0.0	-0.0	0.0
60	0.00	1.2	-0.2	0.0	-0.0	-0.0	0.0
60	0.10	1.2	0.2	0.0	-0.0	-0.0	0.0
61	0.00	1.2	-0.3	0.0	-0.0	-0.0	-0.0
61	0.10	1.2	0.1	0.0	-0.0	-0.0	0.0
62	0.00	1.2	-0.3	0.0	-0.0	-0.0	-0.0
62	0.10	1.2	0.1	0.0	-0.0	-0.0	0.0
63	0.00	1.2	-0.2	0.0	-0.0	-0.0	0.0
63	0.10	1.2	0.2	0.0	-0.0	-0.0	-0.0
64	0.00	1.2	-0.7	0.0	0.0	-0.0	-0.1
64	0.10	1.2	-0.4	0.0	0.0	-0.0	0.0
66	0.00	0.0	32.0	-0.1	-0.0	-0.0	0.0
66	0.04	0.0	32.4	-0.1	-0.0	-0.0	-1.3
69	0.00	0.0	32.0	0.1	0.0	0.0	0.0
69	0.04	0.0	32.4	0.1	0.0	0.0	-1.3
71	0.00	1.1	-0.8	-0.0	-0.0	-0.0	-0.1
71	0.10	1.1	-0.4	-0.0	-0.0	-0.0	0.0
72	0.00	1.1	-0.2	-0.0	-0.0	-0.0	0.0
72	0.10	1.1	0.2	-0.0	-0.0	-0.0	-0.0
73	0.00	1.1	-0.3	-0.0	-0.0	-0.0	-0.0
73	0.10	1.1	0.1	-0.0	-0.0	-0.0	0.0
74	0.00	1.1	-0.3	-0.0	-0.0	-0.0	0.0
74	0.10	1.1	0.1	-0.0	-0.0	-0.0	0.0

75	0.00	1.1	-0.2	-0.0	-0.0	-0.0	0.0
75	0.10	1.1	0.2	-0.0	-0.0	-0.0	0.0
76	0.00	1.1	-0.2	0.0	0.0	-0.0	0.0
76	0.10	1.1	0.2	0.0	0.0	-0.0	0.0
77	0.00	1.1	-0.1	0.0	0.0	-0.0	0.0
77	0.10	1.1	0.3	0.0	0.0	-0.0	0.0
78	0.00	1.1	-0.1	0.0	0.0	-0.0	0.0
78	0.10	1.1	0.3	0.0	0.0	-0.0	-0.0
79	0.00	1.1	-0.2	0.0	0.0	-0.0	-0.0
79	0.10	1.1	0.2	0.0	0.0	-0.0	0.0
80	0.00	1.1	0.4	0.0	0.0	-0.0	0.0
80	0.10	1.1	0.8	0.0	0.0	-0.0	-0.1
81	0.00	-1.1	-8.7	0.0	-0.0	-0.0	-1.6
81	0.10	-1.1	-7.9	0.0	-0.0	-0.0	-0.7
82	0.00	-1.1	-7.4	0.0	-0.0	-0.0	-0.7
82	0.10	-1.1	-6.6	0.0	-0.0	-0.0	-0.0
83	0.00	-1.1	-5.3	0.0	-0.0	-0.0	-0.1
83	0.10	-1.1	-4.5	0.0	-0.0	-0.0	0.4
84	0.00	-1.1	-3.3	0.0	-0.0	-0.0	0.4
84	0.10	-1.1	-2.5	0.0	-0.0	-0.0	0.7
85	0.00	-1.1	-1.4	0.0	-0.0	-0.0	0.7
85	0.10	-1.1	-0.6	0.0	-0.0	-0.0	0.8
86	0.00	-1.1	0.6	-0.0	0.0	-0.0	0.8
86	0.10	-1.1	1.4	-0.0	0.0	-0.0	0.7
87	0.00	-1.1	2.5	-0.0	0.0	-0.0	0.7
87	0.10	-1.1	3.3	-0.0	0.0	-0.0	0.4
88	0.00	-1.1	4.5	-0.0	0.0	-0.0	0.4
88	0.10	-1.1	5.3	-0.0	0.0	-0.0	-0.1
89	0.00	-1.1	6.6	-0.0	0.0	-0.0	-0.0
89	0.10	-1.1	7.4	-0.0	0.0	-0.0	-0.7
90	0.00	-1.1	7.9	-0.0	0.0	-0.0	-0.7
90	0.10	-1.1	8.7	-0.0	0.0	-0.0	-1.6
109	0.00	-1.0	8.0	-0.0	0.0	-0.0	-0.8
109	0.10	-1.0	8.8	-0.0	0.0	-0.0	-1.6
110	0.00	-1.1	6.6	-0.0	0.0	-0.0	-0.1
110	0.10	-1.1	7.4	-0.0	0.0	-0.0	-0.8
111	0.00	-1.1	4.6	-0.0	0.0	-0.0	0.4
111	0.10	-1.1	5.4	-0.0	0.0	-0.0	-0.1
112	0.00	-1.1	2.6	-0.0	0.0	-0.0	0.7
112	0.10	-1.1	3.4	-0.0	0.0	-0.0	0.4
113	0.00	-1.1	0.7	-0.0	0.0	-0.0	0.8
113	0.10	-1.1	1.4	-0.0	0.0	-0.0	0.7
114	0.00	-1.1	-1.3	-0.0	0.0	-0.0	0.7
114	0.10	-1.1	-0.5	-0.0	0.0	-0.0	0.8
115	0.00	-1.1	-3.2	-0.0	0.0	-0.0	0.4
115	0.10	-1.1	-2.4	-0.0	0.0	-0.0	0.7
116	0.00	-1.1	-5.2	-0.0	0.0	-0.0	-0.1
116	0.10	-1.1	-4.4	-0.0	0.0	-0.0	0.4
117	0.00	-1.1	-7.3	-0.0	0.0	-0.0	-0.7
117	0.10	-1.1	-6.5	-0.0	0.0	-0.0	-0.1
118	0.00	-1.0	-8.6	-0.0	0.0	-0.0	-1.6
118	0.10	-1.0	-7.9	-0.0	0.0	-0.0	-0.7
119	0.00	1.2	0.4	-0.0	-0.0	-0.0	0.0
119	0.10	1.2	0.7	-0.0	-0.0	-0.0	-0.1
120	0.00	1.2	-0.2	-0.0	0.0	-0.0	-0.0
120	0.10	1.2	0.2	-0.0	0.0	-0.0	0.0
121	0.00	1.2	-0.1	-0.0	0.0	-0.0	0.0
121	0.10	1.2	0.3	-0.0	0.0	-0.0	-0.0
122	0.00	1.2	-0.1	-0.0	0.0	-0.0	0.0
122	0.10	1.2	0.3	-0.0	0.0	-0.0	-0.0
123	0.00	1.2	-0.2	-0.0	0.0	-0.0	0.0
123	0.10	1.2	0.2	-0.0	0.0	-0.0	0.0
124	0.00	1.2	-0.2	-0.0	0.0	-0.0	0.0
124	0.10	1.2	0.2	-0.0	0.0	-0.0	0.0
125	0.00	1.2	-0.2	-0.0	0.0	0.0	0.0
125	0.10	1.2	0.1	-0.0	0.0	-0.0	0.0
126	0.00	1.2	-0.3	-0.0	0.0	0.0	-0.0
126	0.10	1.2	0.1	-0.0	0.0	0.0	0.0
127	0.00	1.2	-0.2	-0.0	0.0	0.0	0.0
127	0.10	1.2	0.2	-0.0	0.0	0.0	-0.0
128	0.00	1.2	-0.8	-0.0	0.0	0.0	-0.1
128	0.10	1.2	-0.4	-0.0	0.0	0.0	0.0
130	0.00	-0.0	33.0	0.6	0.1	0.0	0.0
130	0.04	-0.0	33.4	0.6	0.1	0.0	-1.3
133	0.00	0.0	21.8	-0.7	0.0	0.0	-0.0
133	0.04	0.0	22.2	-0.7	0.0	-0.0	-0.9
135	0.00	2.0	-0.9	0.0	0.0	-0.0	-0.1
135	0.10	2.0	-0.5	0.0	0.0	-0.0	0.0
136	0.00	2.0	-0.2	0.0	0.0	-0.0	0.0

136	0.10	2.0	0.2	0.0	0.0	-0.0	-0.0
137	0.00	2.0	-0.3	0.0	0.0	-0.0	-0.0
137	0.10	2.0	0.1	0.0	0.0	-0.0	0.0
138	0.00	2.0	-0.3	0.0	0.0	-0.0	0.0
138	0.10	2.0	0.1	0.0	0.0	-0.0	0.0
139	0.00	2.1	-0.2	0.0	0.0	-0.0	0.0
139	0.10	2.1	0.2	0.0	0.0	0.0	0.0
140	0.00	2.1	-0.2	0.0	0.0	0.0	0.0
140	0.10	2.1	0.2	0.0	0.0	0.0	0.0
141	0.00	2.1	-0.2	0.0	0.0	0.0	0.0
141	0.10	2.1	0.2	0.0	0.0	0.0	0.0
142	0.00	2.0	-0.2	0.0	0.0	0.0	0.0
142	0.10	2.0	0.2	0.0	0.0	0.0	0.0
143	0.00	2.0	-0.2	0.0	0.0	0.0	0.0
143	0.10	2.0	0.2	0.0	0.0	0.0	0.0
144	0.00	2.0	0.9	0.0	0.0	0.0	0.0
144	0.10	2.0	1.3	0.0	0.0	0.0	-0.1
145	0.00	-1.3	-9.4	0.0	0.0	-0.0	-1.8
145	0.10	-1.3	-8.6	0.0	0.0	-0.0	-0.9
146	0.00	-1.3	-8.1	0.0	0.0	-0.0	-0.9
146	0.10	-1.3	-7.3	0.0	0.0	-0.0	-0.1
147	0.00	-1.3	-6.1	0.0	0.0	-0.0	-0.1
147	0.10	-1.3	-5.3	0.0	0.0	-0.0	0.4
148	0.00	-1.3	-4.1	0.0	0.0	-0.0	0.4
148	0.10	-1.3	-3.3	0.0	0.0	-0.0	0.8
149	0.00	-1.3	-2.1	0.0	0.0	-0.0	0.8
149	0.10	-1.3	-1.4	0.0	0.0	-0.0	1.0
150	0.00	-1.3	-0.2	0.0	0.0	-0.0	1.0
150	0.10	-1.3	0.6	0.0	0.0	-0.0	1.0
151	0.00	-1.3	1.7	0.0	0.0	-0.0	1.0
151	0.10	-1.3	2.5	0.0	0.0	0.0	0.8
152	0.00	-1.3	3.7	0.0	0.0	0.0	0.8
152	0.10	-1.3	4.5	0.0	0.0	0.0	0.3
153	0.00	-1.3	5.8	0.0	0.0	0.0	0.3
153	0.10	-1.3	6.5	0.0	0.0	0.0	-0.3
154	0.00	-1.3	6.7	0.0	0.0	0.0	-0.3
154	0.10	-1.3	7.4	0.0	0.0	0.0	-1.0

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RISULTATI : CASO DI CARICO 1 : SOLLECITAZIONI PILASTRI

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ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
1	0.00	-21.8	0.7	0.0	0.0	-0.0	-0.0
1	0.27	-19.1	0.7	0.0	0.0	-0.0	-0.2
3	0.00	-17.8	-1.3	0.0	0.0	-0.0	-0.3
3	1.02	-7.4	-1.3	0.0	0.0	-0.0	1.0
4	0.00	-28.6	0.2	-0.0	0.0	0.0	0.1
4	1.02	-18.2	0.2	-0.0	0.0	-0.0	-0.1
6	0.00	-33.0	-0.6	-0.0	0.0	0.0	-0.1
6	0.27	-30.2	-0.6	-0.0	0.0	0.0	0.1
27	0.00	-0.7	-0.0	0.0	0.0	-0.0	-0.0
27	1.02	0.1	-0.0	0.0	0.0	-0.0	0.0
28	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
28	1.02	1.2	-0.0	0.0	0.0	0.0	0.0
29	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
29	1.02	1.2	-0.0	0.0	0.0	0.0	0.0
30	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
30	1.02	1.2	-0.0	0.0	0.0	0.0	0.0
31	0.00	0.4	0.0	0.0	0.0	-0.0	0.0
31	1.02	1.2	0.0	0.0	0.0	0.0	-0.0
32	0.00	0.4	0.0	-0.0	0.0	0.0	0.0
32	1.02	1.2	0.0	-0.0	0.0	0.0	-0.0
33	0.00	0.4	0.0	-0.0	0.0	0.0	0.0
33	1.02	1.2	0.0	-0.0	0.0	0.0	-0.0
34	0.00	0.5	0.0	-0.0	0.0	0.0	0.0
34	1.02	1.3	0.0	-0.0	0.0	-0.0	-0.0
35	0.00	-0.3	0.0	-0.0	0.0	0.0	0.0
35	1.02	0.5	0.0	-0.0	0.0	-0.0	-0.0
36	0.00	-0.2	0.0	0.0	0.0	0.0	0.0
36	1.02	0.6	0.0	0.0	0.0	0.0	-0.0
37	0.00	0.5	0.0	0.0	0.0	0.0	0.0
37	1.02	1.3	0.0	0.0	0.0	0.0	-0.0
38	0.00	0.4	0.0	0.0	0.0	0.0	0.0
38	1.02	1.2	0.0	0.0	0.0	0.0	-0.0
39	0.00	0.4	0.0	0.0	0.0	0.0	0.0
39	1.02	1.2	0.0	0.0	0.0	0.0	-0.0
40	0.00	0.4	-0.0	0.0	0.0	0.0	-0.0
40	1.02	1.2	-0.0	0.0	0.0	0.0	0.0
41	0.00	0.4	-0.0	-0.0	0.0	0.0	-0.0
41	1.02	1.2	-0.0	-0.0	0.0	0.0	0.0

42	0.00	0.4	-0.0	-0.0	0.0	0.0	-0.0
42	1.02	1.2	-0.0	-0.0	0.0	0.0	0.0
43	0.00	0.5	-0.0	-0.0	0.0	0.0	-0.0
43	1.02	1.3	-0.0	-0.0	0.0	0.0	0.0
44	0.00	-0.2	-0.0	-0.0	0.0	0.0	-0.0
44	1.02	0.6	-0.0	-0.0	0.0	-0.0	0.0
65	0.00	-32.0	-0.1	0.0	0.0	0.0	-0.0
65	0.27	-29.3	-0.1	0.0	0.0	0.0	0.0
67	0.00	-27.7	-0.0	0.0	0.0	0.0	0.0
67	1.02	-17.3	-0.0	0.0	0.0	0.0	0.0
68	0.00	-27.7	0.0	0.0	-0.0	0.0	-0.0
68	1.02	-17.3	0.0	0.0	-0.0	0.0	-0.0
70	0.00	-32.0	0.1	0.0	-0.0	0.0	0.0
70	0.27	-29.3	0.1	0.0	-0.0	0.0	-0.0
91	0.00	-0.2	-0.0	0.0	0.0	0.0	-0.0
91	1.02	0.6	-0.0	0.0	0.0	0.0	0.0
92	0.00	0.5	-0.0	0.0	0.0	0.0	-0.0
92	1.02	1.3	-0.0	0.0	0.0	0.0	0.0
93	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
93	1.02	1.2	-0.0	0.0	0.0	0.0	0.0
94	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
94	1.02	1.2	-0.0	0.0	0.0	0.0	0.0
95	0.00	0.4	-0.0	0.0	0.0	-0.0	0.0
95	1.02	1.2	-0.0	0.0	0.0	0.0	0.0
96	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
96	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0
97	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
97	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0
98	0.00	0.5	0.0	0.0	-0.0	0.0	0.0
98	1.02	1.3	0.0	0.0	-0.0	0.0	-0.0
99	0.00	-0.2	0.0	0.0	-0.0	0.0	0.0
99	1.02	0.6	0.0	0.0	-0.0	0.0	-0.0
100	0.00	-0.2	0.0	-0.0	-0.0	0.0	0.0
100	1.02	0.6	0.0	-0.0	-0.0	-0.0	-0.0
101	0.00	0.5	0.0	-0.0	-0.0	0.0	0.0
101	1.02	1.3	0.0	-0.0	-0.0	0.0	-0.0
102	0.00	0.4	0.0	-0.0	-0.0	0.0	0.0
102	1.02	1.2	0.0	-0.0	-0.0	0.0	-0.0
103	0.00	0.4	0.0	-0.0	-0.0	0.0	0.0
103	1.02	1.2	0.0	-0.0	-0.0	0.0	-0.0
104	0.00	0.4	0.0	0.0	-0.0	0.0	0.0
104	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0
105	0.00	0.4	-0.0	0.0	-0.0	0.0	-0.0
105	1.02	1.2	-0.0	0.0	-0.0	0.0	0.0
106	0.00	0.4	-0.0	0.0	-0.0	0.0	-0.0
106	1.02	1.2	-0.0	0.0	-0.0	0.0	0.0
107	0.00	0.5	-0.0	0.0	-0.0	0.0	-0.0
107	1.02	1.3	-0.0	0.0	-0.0	0.0	0.0
108	0.00	-0.2	-0.0	0.0	-0.0	0.0	-0.0
108	1.02	0.6	-0.0	0.0	-0.0	0.0	0.0
129	0.00	-33.0	0.6	-0.0	-0.0	0.0	0.1
129	0.27	-30.2	0.6	-0.0	-0.0	0.0	-0.1
131	0.00	-28.6	-0.2	-0.0	-0.0	0.0	-0.1
131	1.02	-18.2	-0.2	-0.0	-0.0	-0.0	0.1
132	0.00	-17.8	1.3	0.0	-0.0	-0.0	0.3
132	1.02	-7.4	1.3	0.0	-0.0	-0.0	-1.0
134	0.00	-21.8	-0.7	0.0	-0.0	-0.0	0.0
134	0.27	-19.1	-0.7	0.0	-0.0	-0.0	0.2
155	0.00	-0.3	-0.0	-0.0	-0.0	0.0	-0.0
155	1.02	0.5	-0.0	-0.0	-0.0	-0.0	0.0
156	0.00	0.5	-0.0	-0.0	-0.0	0.0	-0.0
156	1.02	1.3	-0.0	-0.0	-0.0	-0.0	0.0
157	0.00	0.4	-0.0	-0.0	-0.0	0.0	-0.0
157	1.02	1.2	-0.0	-0.0	-0.0	0.0	0.0
158	0.00	0.4	-0.0	-0.0	-0.0	0.0	-0.0
158	1.02	1.2	-0.0	-0.0	-0.0	0.0	0.0
159	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0
159	1.02	1.2	-0.0	0.0	-0.0	0.0	0.0
160	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
160	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0
161	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
161	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0
162	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
162	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0
163	0.00	-0.7	0.0	0.0	-0.0	-0.0	0.0
163	1.02	0.1	0.0	0.0	-0.0	-0.0	-0.0

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RISULTATI : CASO DI CARICO 2 : SOLLECITAZIONI TRAVI

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[illegible]

123	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
123	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
124	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
124	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
125	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
125	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
126	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
126	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
127	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
127	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
128	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
128	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
130	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
130	0.04	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
133	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
133	0.04	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
135	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
135	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
136	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
136	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
137	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
137	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
138	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
138	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
139	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
139	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
140	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
140	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
141	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
141	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
142	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
142	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
143	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
143	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
144	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
144	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
145	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
145	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
146	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
146	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
147	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
147	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
148	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
148	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
149	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
149	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
150	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
150	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
151	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
151	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
152	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
152	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
153	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
153	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
154	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
154	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0

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RISULTATI : CASO DI CARICO 2 : SOLLECITAZIONI PILASTRI

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ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
1	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
1	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
3	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
3	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
4	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
4	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
6	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
6	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
27	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
27	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
28	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
28	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
29	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
29	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
30	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
30	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
31	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
31	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0

[illegible]

155	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
156	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
156	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
157	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
157	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
158	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
158	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
159	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
159	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
160	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
160	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
161	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
161	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
162	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
162	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
163	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
163	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0

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RISULTATI : CASO DI CARICO 3 : SOLLECITAZIONI TRAVI

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ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
2	0.00	116.3	0.2	1.0	0.2	-13.4	-166.5
2	0.04	116.3	0.2	1.0	0.2	-13.4	-166.5
5	0.00	182.6	-0.2	0.4	0.1	-6.8	-227.4
5	0.04	182.6	-0.2	0.4	0.1	-6.8	-227.4
7	0.00	1.1	-0.0	4.7	-0.7	-3.0	-0.0
7	0.10	1.1	-0.0	4.7	-0.7	-2.5	-0.0
8	0.00	1.1	-0.0	4.8	-0.6	-2.5	-0.0
8	0.10	1.1	-0.0	4.8	-0.6	-2.0	-0.0
9	0.00	1.1	-0.0	4.9	-0.5	-2.0	-0.0
9	0.10	1.1	-0.0	4.9	-0.5	-1.6	-0.0
10	0.00	1.1	-0.0	5.0	-0.3	-1.6	-0.0
10	0.10	1.1	-0.0	5.0	-0.3	-1.1	-0.0
11	0.00	1.1	-0.0	5.1	-0.2	-1.1	-0.0
11	0.10	1.1	-0.0	5.1	-0.2	-0.6	0.0
12	0.00	1.1	-0.0	5.2	-0.1	-0.6	-0.0
12	0.10	1.1	-0.0	5.2	-0.1	-0.1	0.0
13	0.00	1.1	-0.0	5.3	0.0	-0.1	-0.0
13	0.10	1.1	-0.0	5.3	0.0	0.4	0.0
14	0.00	1.1	-0.0	5.4	0.2	0.4	0.0
14	0.10	1.1	-0.0	5.4	0.2	0.9	0.0
15	0.00	1.1	-0.0	5.5	0.3	0.9	0.0
15	0.10	1.1	-0.0	5.5	0.3	1.5	0.0
16	0.00	1.1	-0.0	5.7	0.5	1.5	0.0
16	0.10	1.1	-0.0	5.7	0.5	2.0	0.0
17	0.00	-0.2	-0.2	-121.1	-10.9	16.4	-0.1
17	0.10	-0.2	-0.2	-101.1	-10.9	5.3	-0.1
18	0.00	-0.2	-0.2	-101.2	-10.9	5.3	-0.1
18	0.10	-0.2	-0.2	-81.2	-10.9	-3.8	-0.1
19	0.00	-0.2	-0.2	-81.3	-10.9	-3.8	-0.1
19	0.10	-0.2	-0.2	-61.3	-10.9	-10.9	-0.0
20	0.00	-0.2	-0.2	-61.3	-11.0	-10.9	-0.0
20	0.10	-0.2	-0.2	-41.3	-11.0	-16.0	-0.0
21	0.00	-0.2	-0.2	-41.4	-11.0	-16.0	-0.0
21	0.10	-0.2	-0.2	-21.4	-11.0	-19.2	-0.0
22	0.00	-0.2	-0.2	-21.5	-11.0	-19.1	-0.0
22	0.10	-0.2	-0.2	-1.5	-11.0	-20.3	0.0
23	0.00	-0.2	-0.2	-1.6	-11.1	-20.3	0.0
23	0.10	-0.2	-0.2	18.4	-11.1	-19.4	0.0
24	0.00	-0.2	-0.2	18.3	-11.1	-19.4	0.0
24	0.10	-0.2	-0.2	38.3	-11.1	-16.6	0.1
25	0.00	-0.2	-0.2	38.1	-11.1	-16.6	0.1
25	0.10	-0.2	-0.2	58.1	-11.1	-11.8	0.1
26	0.00	-0.2	-0.1	58.0	-11.1	-11.7	0.1
26	0.10	-0.2	-0.1	78.0	-11.1	-4.9	0.1
45	0.00	-0.3	-0.0	78.1	-5.9	-4.7	0.0
45	0.10	-0.3	-0.0	98.1	-5.9	4.1	0.0
46	0.00	-0.3	-0.0	58.3	-5.9	-11.5	0.0
46	0.10	-0.3	-0.0	78.3	-5.9	-4.7	0.0
47	0.00	-0.3	-0.0	38.4	-5.9	-16.4	0.0
47	0.10	-0.3	-0.0	58.4	-5.9	-11.5	0.0
48	0.00	-0.3	-0.0	18.6	-5.9	-19.2	0.0
48	0.10	-0.3	-0.0	38.6	-5.9	-16.4	0.0
49	0.00	-0.3	-0.0	-1.3	-5.9	-20.1	0.0
49	0.10	-0.3	-0.0	18.7	-5.9	-19.2	0.0
50	0.00	-0.3	-0.0	-21.2	-5.8	-19.0	0.0
50	0.10	-0.3	-0.0	-1.2	-5.8	-20.1	0.0
51	0.00	-0.3	-0.0	-41.1	-5.8	-15.9	0.0
51	0.10	-0.3	-0.0	-21.1	-5.8	-19.0	0.0

52	0.00	-0.3	-0.0	-61.0	-5.8	-10.8	0.0
52	0.10	-0.3	-0.0	-41.0	-5.8	-15.9	0.0
53	0.00	-0.3	-0.0	-80.8	-5.7	-3.7	-0.0
53	0.10	-0.3	-0.0	-60.8	-5.7	-10.8	0.0
54	0.00	-0.3	0.0	-100.7	-5.7	5.3	-0.0
54	0.10	-0.3	0.0	-80.7	-5.7	-3.7	-0.0
55	0.00	1.7	-0.0	3.0	0.7	0.6	0.0
55	0.10	1.7	-0.0	3.0	0.7	0.9	0.0
56	0.00	1.7	-0.0	2.8	0.5	0.3	0.0
56	0.10	1.7	-0.0	2.8	0.5	0.6	0.0
57	0.00	1.7	-0.0	2.7	0.3	0.0	0.0
57	0.10	1.7	-0.0	2.7	0.3	0.3	0.0
58	0.00	1.7	-0.0	2.6	0.2	-0.2	0.0
58	0.10	1.7	-0.0	2.6	0.2	0.0	0.0
59	0.00	1.7	-0.0	2.4	0.0	-0.5	0.0
59	0.10	1.7	-0.0	2.4	0.0	-0.2	0.0
60	0.00	1.7	-0.0	2.3	-0.1	-0.7	0.0
60	0.10	1.7	-0.0	2.3	-0.1	-0.5	0.0
61	0.00	1.7	-0.0	2.2	-0.3	-0.9	-0.0
61	0.10	1.7	-0.0	2.2	-0.3	-0.7	0.0
62	0.00	1.7	-0.0	2.1	-0.4	-1.1	0.0
62	0.10	1.7	-0.0	2.1	-0.4	-0.9	0.0
63	0.00	1.7	-0.0	1.9	-0.6	-1.3	0.0
63	0.10	1.7	-0.0	1.9	-0.6	-1.1	0.0
64	0.00	1.7	-0.0	1.8	-0.8	-1.4	-0.0
64	0.10	1.7	-0.0	1.8	-0.8	-1.3	0.0
66	0.00	201.1	-0.0	0.1	0.0	-1.9	-251.1
66	0.04	201.1	-0.0	0.1	0.0	-1.9	-251.1
69	0.00	201.1	-0.0	-0.1	-0.0	1.9	-251.1
69	0.04	201.1	-0.0	-0.1	-0.0	1.9	-251.1
71	0.00	1.8	-0.0	-0.7	-0.8	-0.2	-0.0
71	0.10	1.8	-0.0	-0.7	-0.8	-0.3	0.0
72	0.00	1.8	-0.0	-0.5	-0.6	-0.3	0.0
72	0.10	1.8	-0.0	-0.5	-0.6	-0.3	0.0
73	0.00	1.8	0.0	-0.3	-0.4	-0.3	0.0
73	0.10	1.8	0.0	-0.3	-0.4	-0.3	0.0
74	0.00	1.8	-0.0	-0.2	-0.2	-0.4	0.0
74	0.10	1.8	-0.0	-0.2	-0.2	-0.4	0.0
75	0.00	1.8	-0.0	-0.1	-0.1	-0.4	0.0
75	0.10	1.8	-0.0	-0.1	-0.1	-0.4	0.0
76	0.00	1.8	0.0	0.1	0.1	-0.4	0.0
76	0.10	1.8	0.0	0.1	0.1	-0.4	0.0
77	0.00	1.8	0.0	0.2	0.2	-0.4	0.0
77	0.10	1.8	0.0	0.2	0.2	-0.4	0.0
78	0.00	1.8	-0.0	0.3	0.4	-0.3	0.0
78	0.10	1.8	-0.0	0.3	0.4	-0.3	0.0
79	0.00	1.8	0.0	0.5	0.6	-0.3	0.0
79	0.10	1.8	0.0	0.5	0.6	-0.3	0.0
80	0.00	1.8	0.0	0.7	0.8	-0.3	0.0
80	0.10	1.8	0.0	0.7	0.8	-0.2	-0.0
81	0.00	-0.4	0.0	-99.3	0.1	7.1	0.0
81	0.10	-0.4	0.0	-79.3	0.1	-1.9	0.0
82	0.00	-0.4	0.0	-79.5	0.1	-1.9	0.0
82	0.10	-0.4	0.0	-59.5	0.1	-8.8	0.0
83	0.00	-0.4	-0.0	-59.7	0.1	-8.8	0.0
83	0.10	-0.4	-0.0	-39.7	0.1	-13.8	0.0
84	0.00	-0.4	0.0	-39.8	0.1	-13.8	0.0
84	0.10	-0.4	0.0	-19.8	0.1	-16.8	0.0
85	0.00	-0.4	0.0	-19.9	0.0	-16.8	0.0
85	0.10	-0.4	0.0	0.1	0.0	-17.7	0.0
86	0.00	-0.4	-0.0	-0.1	-0.0	-17.7	0.0
86	0.10	-0.4	-0.0	19.9	-0.0	-16.8	0.0
87	0.00	-0.4	-0.0	19.8	-0.1	-16.8	0.0
87	0.10	-0.4	-0.0	39.8	-0.1	-13.8	0.0
88	0.00	-0.4	0.0	39.7	-0.1	-13.8	0.0
88	0.10	-0.4	0.0	59.7	-0.1	-8.8	0.0
89	0.00	-0.4	-0.0	59.5	-0.1	-8.8	0.0
89	0.10	-0.4	-0.0	79.5	-0.1	-1.9	0.0
90	0.00	-0.4	-0.0	79.3	-0.1	-1.9	0.0
90	0.10	-0.4	-0.0	99.3	-0.1	7.1	0.0
109	0.00	-0.3	-0.0	80.7	5.7	-3.7	-0.0
109	0.10	-0.3	-0.0	100.7	5.7	5.3	-0.0
110	0.00	-0.3	0.0	60.8	5.7	-10.8	0.0
110	0.10	-0.3	0.0	80.8	5.7	-3.7	-0.0
111	0.00	-0.3	0.0	41.0	5.8	-15.9	0.0
111	0.10	-0.3	0.0	61.0	5.8	-10.8	0.0
112	0.00	-0.3	0.0	21.1	5.8	-19.0	0.0
112	0.10	-0.3	0.0	41.1	5.8	-15.9	0.0

113	0.00	-0.3	0.0	1.2	5.8	-20.1	0.0
113	0.10	-0.3	0.0	21.2	5.8	-19.0	0.0
114	0.00	-0.3	0.0	-18.7	5.9	-19.2	0.0
114	0.10	-0.3	0.0	1.3	5.9	-20.1	0.0
115	0.00	-0.3	0.0	-38.6	5.9	-16.4	0.0
115	0.10	-0.3	0.0	-18.6	5.9	-19.2	0.0
116	0.00	-0.3	0.0	-58.4	5.9	-11.5	0.0
116	0.10	-0.3	0.0	-38.4	5.9	-16.4	0.0
117	0.00	-0.3	0.0	-78.3	5.9	-4.7	0.0
117	0.10	-0.3	0.0	-58.3	5.9	-11.5	0.0
118	0.00	-0.3	0.0	-98.1	5.9	4.1	0.0
118	0.10	-0.3	0.0	-78.1	5.9	-4.7	0.0
119	0.00	1.7	0.0	-1.8	0.8	-1.3	0.0
119	0.10	1.7	0.0	-1.8	0.8	-1.4	-0.0
120	0.00	1.7	0.0	-1.9	0.6	-1.1	0.0
120	0.10	1.7	0.0	-1.9	0.6	-1.3	0.0
121	0.00	1.7	0.0	-2.1	0.4	-0.9	0.0
121	0.10	1.7	0.0	-2.1	0.4	-1.1	0.0
122	0.00	1.7	0.0	-2.2	0.3	-0.7	0.0
122	0.10	1.7	0.0	-2.2	0.3	-0.9	-0.0
123	0.00	1.7	0.0	-2.3	0.1	-0.5	0.0
123	0.10	1.7	0.0	-2.3	0.1	-0.7	0.0
124	0.00	1.7	0.0	-2.4	-0.0	-0.2	0.0
124	0.10	1.7	0.0	-2.4	-0.0	-0.5	0.0
125	0.00	1.7	0.0	-2.6	-0.2	0.0	0.0
125	0.10	1.7	0.0	-2.6	-0.2	-0.2	0.0
126	0.00	1.7	0.0	-2.7	-0.3	0.3	0.0
126	0.10	1.7	0.0	-2.7	-0.3	0.0	0.0
127	0.00	1.7	0.0	-2.8	-0.5	0.6	0.0
127	0.10	1.7	0.0	-2.8	-0.5	0.3	0.0
128	0.00	1.7	0.0	-3.0	-0.7	0.9	0.0
128	0.10	1.7	0.0	-3.0	-0.7	0.6	0.0
130	0.00	182.6	-0.2	-0.4	-0.1	6.8	-227.4
130	0.04	182.6	-0.2	-0.4	-0.1	6.8	-227.4
133	0.00	116.3	0.2	-1.0	-0.2	13.4	-166.5
133	0.04	116.3	0.2	-1.0	-0.2	13.4	-166.5
135	0.00	1.1	0.0	-5.7	-0.5	2.0	0.0
135	0.10	1.1	0.0	-5.7	-0.5	1.5	0.0
136	0.00	1.1	0.0	-5.5	-0.3	1.5	0.0
136	0.10	1.1	0.0	-5.5	-0.3	0.9	0.0
137	0.00	1.1	0.0	-5.4	-0.2	0.9	0.0
137	0.10	1.1	0.0	-5.4	-0.2	0.4	0.0
138	0.00	1.1	0.0	-5.3	-0.0	0.4	0.0
138	0.10	1.1	0.0	-5.3	-0.0	-0.1	-0.0
139	0.00	1.1	0.0	-5.2	0.1	-0.1	0.0
139	0.10	1.1	0.0	-5.2	0.1	-0.6	-0.0
140	0.00	1.1	0.0	-5.1	0.2	-0.6	0.0
140	0.10	1.1	0.0	-5.1	0.2	-1.1	-0.0
141	0.00	1.1	0.0	-5.0	0.3	-1.1	-0.0
141	0.10	1.1	0.0	-5.0	0.3	-1.6	-0.0
142	0.00	1.1	0.0	-4.9	0.5	-1.6	-0.0
142	0.10	1.1	0.0	-4.9	0.5	-2.0	-0.0
143	0.00	1.1	0.0	-4.8	0.6	-2.0	-0.0
143	0.10	1.1	0.0	-4.8	0.6	-2.5	-0.0
144	0.00	1.1	0.0	-4.7	0.7	-2.5	-0.0
144	0.10	1.1	0.0	-4.7	0.7	-3.0	-0.0
145	0.00	-0.2	0.1	-78.0	11.1	-4.9	0.1
145	0.10	-0.2	0.1	-58.0	11.1	-11.7	0.1
146	0.00	-0.2	0.2	-58.1	11.1	-11.8	0.1
146	0.10	-0.2	0.2	-38.1	11.1	-16.6	0.1
147	0.00	-0.2	0.2	-38.3	11.1	-16.6	0.1
147	0.10	-0.2	0.2	-18.3	11.1	-19.4	0.0
148	0.00	-0.2	0.2	-18.4	11.1	-19.4	0.0
148	0.10	-0.2	0.2	1.6	11.1	-20.3	0.0
149	0.00	-0.2	0.2	1.5	11.0	-20.3	0.0
149	0.10	-0.2	0.2	21.5	11.0	-19.1	-0.0
150	0.00	-0.2	0.2	21.4	11.0	-19.2	-0.0
150	0.10	-0.2	0.2	41.4	11.0	-16.0	-0.0
151	0.00	-0.2	0.2	41.3	11.0	-16.0	-0.0
151	0.10	-0.2	0.2	61.3	11.0	-10.9	-0.0
152	0.00	-0.2	0.2	61.3	10.9	-10.9	-0.0
152	0.10	-0.2	0.2	81.3	10.9	-3.8	-0.1
153	0.00	-0.2	0.2	81.2	10.9	-3.8	-0.1
153	0.10	-0.2	0.2	101.2	10.9	5.3	-0.1
154	0.00	-0.2	0.2	101.1	10.9	5.3	-0.1
154	0.10	-0.2	0.2	121.1	10.9	16.4	-0.1

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RISULTATI : CASO DI CARICO 3 : SOLLECITAZIONI PILASTRI							
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ELEM.	ascissa	N	V2	V3	T	M2	M3

n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)
1	0.00	-0.2	1.0	116.3	13.4	-166.5	0.2
1	0.27	-0.2	1.0	116.3	13.4	-135.1	-0.1
3	0.00	-0.2	-0.2	121.1	16.4	-134.3	-0.1
3	1.02	-0.2	-0.2	121.1	16.4	-10.9	0.1
4	0.00	0.1	-0.1	178.6	10.3	-176.8	-0.1
4	1.02	0.1	-0.1	178.6	10.3	5.4	0.1
6	0.00	0.2	0.4	182.6	6.8	-227.4	0.1
6	0.27	0.2	0.4	182.6	6.8	-178.1	-0.0
27	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0
27	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0
28	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0
28	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0
29	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0
29	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0
30	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0
30	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0
31	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0
31	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0
32	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0
32	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0
33	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0
33	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0
34	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0
34	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0
35	0.00	0.0	-0.0	0.2	0.0	-0.2	-0.0
35	1.02	0.0	-0.0	0.2	0.0	-0.0	0.0
36	0.00	0.0	-0.0	0.2	0.0	-0.2	-0.0
36	1.02	0.0	-0.0	0.2	0.0	-0.0	0.0
37	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0
37	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0
38	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0
38	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0
39	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0
39	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0
40	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0
40	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0
41	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0
41	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0
42	0.00	0.0	-0.0	0.1	0.0	-0.2	-0.0
42	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0
43	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0
43	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0
44	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0
44	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0
65	0.00	0.0	0.1	201.1	1.9	-251.1	0.0
65	0.27	0.0	0.1	201.1	1.9	-196.8	-0.0
67	0.00	0.0	-0.0	197.4	2.9	-195.3	-0.0
67	1.02	0.0	-0.0	197.4	2.9	6.1	0.0
68	0.00	0.0	0.0	197.4	-2.9	-195.3	0.0
68	1.02	0.0	0.0	197.4	-2.9	6.1	-0.0
70	0.00	0.0	-0.1	201.1	-1.9	-251.1	-0.0
70	0.27	0.0	-0.1	201.1	-1.9	-196.8	0.0
91	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0
91	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0
92	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0
92	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0
93	0.00	0.0	-0.0	0.1	0.0	-0.2	-0.0
93	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0
94	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0
94	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0
95	0.00	-0.0	-0.0	0.1	-0.0	-0.1	-0.0
95	1.02	-0.0	-0.0	0.1	-0.0	-0.0	-0.0
96	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0
96	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0
97	0.00	0.0	0.0	0.1	-0.0	-0.2	0.0
97	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0
98	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0
98	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0
99	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0
99	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0
100	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0
100	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0
101	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0
101	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0
102	0.00	0.0	0.0	0.1	-0.0	-0.2	0.0
102	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0
103	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0
103	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0

104	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0
104	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0
105	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0
105	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0
106	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0
106	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0
107	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0
107	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0
108	0.00	0.0	0.0	0.2	-0.0	-0.2	0.0
108	1.02	0.0	0.0	0.2	-0.0	-0.0	-0.0
129	0.00	0.2	-0.4	182.6	-6.8	-227.4	-0.1
129	0.27	0.2	-0.4	182.6	-6.8	-178.1	0.0
131	0.00	0.1	0.1	178.6	-10.3	-176.8	0.1
131	1.02	0.1	0.1	178.6	-10.3	5.4	-0.1
132	0.00	-0.2	0.2	121.1	-16.4	-134.3	0.1
132	1.02	-0.2	0.2	121.1	-16.4	-10.9	-0.1
134	0.00	-0.2	-1.0	116.3	-13.4	-166.5	-0.2
134	0.27	-0.2	-1.0	116.3	-13.4	-135.1	0.1
155	0.00	0.0	0.0	0.2	-0.0	-0.2	0.0
155	1.02	0.0	0.0	0.2	-0.0	-0.0	-0.0
156	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0
156	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0
157	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0
157	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0
158	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0
158	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0
159	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0
159	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0
160	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0
160	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0
161	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0
161	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0
162	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0
162	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0
163	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0
163	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0

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RISULTATI : COMBINAZIONE 1 : SOLLECITAZIONI TRAVI

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ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
2	0.00	174.5	28.7	2.4	0.2	-20.1	-249.7
2	0.04	174.5	29.2	2.4	0.2	-20.0	-250.9
5	0.00	273.8	42.6	-0.2	-0.0	-10.2	-341.1
5	0.04	273.8	43.2	-0.2	-0.0	-10.2	-342.8
7	0.00	4.3	-1.6	7.1	-1.1	-4.4	-0.1
7	0.10	4.3	-1.1	7.1	-1.1	-3.7	0.0
8	0.00	4.4	-0.2	7.3	-0.9	-3.8	0.0
8	0.10	4.4	0.3	7.3	-0.9	-3.0	0.0
9	0.00	4.4	-0.3	7.4	-0.7	-3.1	0.0
9	0.10	4.4	0.2	7.4	-0.7	-2.3	0.0
10	0.00	4.4	-0.3	7.5	-0.5	-2.4	0.0
10	0.10	4.4	0.2	7.5	-0.5	-1.6	0.0
11	0.00	4.4	-0.3	7.7	-0.3	-1.6	0.0
11	0.10	4.4	0.2	7.7	-0.3	-0.9	0.0
12	0.00	4.4	-0.2	7.8	-0.2	-0.9	0.0
12	0.10	4.4	0.3	7.8	-0.2	-0.1	0.0
13	0.00	4.4	-0.2	7.9	0.0	-0.2	0.0
13	0.10	4.4	0.3	7.9	0.0	0.6	0.0
14	0.00	4.4	-0.2	8.1	0.3	0.6	0.0
14	0.10	4.4	0.3	8.1	0.3	1.4	-0.0
15	0.00	4.4	-0.3	8.3	0.5	1.4	-0.0
15	0.10	4.4	0.2	8.3	0.5	2.2	0.0
16	0.00	4.4	0.5	8.6	0.8	2.2	0.0
16	0.10	4.4	1.1	8.6	0.8	3.0	-0.1
17	0.00	-1.9	-9.9	-181.6	-16.3	24.6	-1.4
17	0.10	-1.9	-8.9	-151.6	-16.3	7.9	-0.5
18	0.00	-2.0	-8.8	-151.8	-16.3	7.9	-0.5
18	0.10	-2.0	-7.8	-121.8	-16.3	-5.7	0.4
19	0.00	-2.0	-6.1	-121.9	-16.4	-5.7	0.4
19	0.10	-2.0	-5.1	-91.9	-16.4	-16.4	0.9
20	0.00	-2.0	-3.6	-92.0	-16.5	-16.4	0.9
20	0.10	-2.0	-2.5	-62.0	-16.5	-24.1	1.2
21	0.00	-2.0	-1.0	-62.1	-16.5	-24.0	1.2
21	0.10	-2.0	-0.0	-32.1	-16.5	-28.7	1.3
22	0.00	-2.0	1.5	-32.3	-16.6	-28.7	1.3
22	0.10	-2.0	2.5	-2.3	-16.6	-30.4	1.1
23	0.00	-2.0	4.0	-2.4	-16.6	-30.4	1.1
23	0.10	-2.0	5.0	27.6	-16.6	-29.1	0.6

24	0.00	-2.0	6.6	27.4	-16.7	-29.1	0.6
24	0.10	-2.0	7.6	57.4	-16.7	-24.9	-0.1
25	0.00	-2.0	9.3	57.2	-16.7	-24.9	-0.1
25	0.10	-2.0	10.3	87.2	-16.7	-17.6	-1.1
26	0.00	-2.0	11.0	86.9	-16.7	-17.6	-1.0
26	0.10	-2.0	12.0	116.9	-16.7	-7.4	-2.2
45	0.00	-1.9	10.2	117.1	-8.9	-7.0	-0.9
45	0.10	-1.9	11.2	147.1	-8.9	6.2	-2.0
46	0.00	-1.9	8.4	87.4	-8.9	-17.3	-0.0
46	0.10	-1.9	9.4	117.4	-8.9	-7.0	-0.9
47	0.00	-1.9	5.7	57.6	-8.9	-24.5	0.6
47	0.10	-1.9	6.7	87.6	-8.9	-17.3	-0.0
48	0.00	-1.9	3.1	27.8	-8.8	-28.8	0.9
48	0.10	-1.9	4.1	57.8	-8.8	-24.5	0.6
49	0.00	-1.9	0.6	-2.0	-8.8	-30.1	1.1
49	0.10	-1.9	1.6	28.0	-8.8	-28.8	0.9
50	0.00	-1.9	-1.9	-31.8	-8.7	-28.5	0.9
50	0.10	-1.9	-0.9	-1.8	-8.7	-30.2	1.1
51	0.00	-1.9	-4.4	-61.6	-8.7	-23.8	0.5
51	0.10	-1.9	-3.4	-31.6	-8.7	-28.5	0.9
52	0.00	-1.9	-7.0	-91.5	-8.6	-16.2	-0.1
52	0.10	-1.9	-6.0	-61.5	-8.6	-23.9	0.5
53	0.00	-1.9	-9.7	-121.2	-8.6	-5.6	-1.0
53	0.10	-1.9	-8.7	-91.2	-8.6	-16.2	-0.1
54	0.00	-1.8	-11.5	-151.0	-8.6	8.0	-2.1
54	0.10	-1.8	-10.5	-121.0	-8.6	-5.6	-1.0
55	0.00	4.1	0.5	4.6	1.1	0.8	0.0
55	0.10	4.1	1.0	4.6	1.1	1.3	-0.1
56	0.00	4.1	-0.3	4.3	0.8	0.4	-0.0
56	0.10	4.1	0.2	4.3	0.8	0.8	0.0
57	0.00	4.1	-0.2	4.0	0.5	0.0	0.0
57	0.10	4.1	0.3	4.0	0.5	0.4	-0.0
58	0.00	4.1	-0.2	3.8	0.2	-0.4	0.0
58	0.10	4.1	0.3	3.8	0.2	0.0	0.0
59	0.00	4.1	-0.2	3.7	0.0	-0.7	0.0
59	0.10	4.1	0.3	3.7	0.0	-0.3	0.0
60	0.00	4.1	-0.3	3.5	-0.2	-1.0	0.0
60	0.10	4.1	0.2	3.5	-0.2	-0.7	0.0
61	0.00	4.1	-0.3	3.3	-0.4	-1.4	-0.0
61	0.10	4.1	0.2	3.3	-0.4	-1.0	0.0
62	0.00	4.1	-0.3	3.1	-0.7	-1.7	-0.0
62	0.10	4.1	0.2	3.1	-0.7	-1.3	0.0
63	0.00	4.1	-0.2	2.9	-0.9	-1.9	0.0
63	0.10	4.1	0.3	2.9	-0.9	-1.6	-0.0
64	0.00	4.1	-1.0	2.7	-1.2	-2.2	-0.1
64	0.10	4.1	-0.5	2.7	-1.2	-1.9	0.0
66	0.00	301.7	41.6	-0.0	-0.0	-2.8	-376.7
66	0.04	301.7	42.1	-0.0	-0.0	-2.8	-378.3
69	0.00	301.7	41.6	0.0	0.0	2.8	-376.7
69	0.04	301.7	42.1	0.0	0.0	2.8	-378.3
71	0.00	4.1	-1.0	-1.0	-1.2	-0.3	-0.1
71	0.10	4.1	-0.5	-1.0	-1.2	-0.4	0.0
72	0.00	4.1	-0.2	-0.7	-0.9	-0.4	0.0
72	0.10	4.1	0.3	-0.7	-0.9	-0.5	-0.0
73	0.00	4.1	-0.3	-0.5	-0.6	-0.5	-0.0
73	0.10	4.1	0.2	-0.5	-0.6	-0.5	0.0
74	0.00	4.1	-0.3	-0.3	-0.3	-0.5	0.0
74	0.10	4.1	0.2	-0.3	-0.3	-0.6	0.0
75	0.00	4.1	-0.3	-0.1	-0.1	-0.6	0.0
75	0.10	4.1	0.2	-0.1	-0.1	-0.6	0.0
76	0.00	4.1	-0.2	0.1	0.1	-0.6	0.0
76	0.10	4.1	0.3	0.1	0.1	-0.6	0.0
77	0.00	4.1	-0.2	0.3	0.3	-0.6	0.0
77	0.10	4.1	0.3	0.3	0.3	-0.5	0.0
78	0.00	4.1	-0.2	0.5	0.6	-0.5	0.0
78	0.10	4.1	0.3	0.5	0.6	-0.5	-0.0
79	0.00	4.1	-0.3	0.7	0.9	-0.5	-0.0
79	0.10	4.1	0.2	0.7	0.9	-0.4	0.0
80	0.00	4.1	0.5	1.0	1.2	-0.4	0.0
80	0.10	4.1	1.0	1.0	1.2	-0.3	-0.1
81	0.00	-1.9	-11.3	-149.0	0.2	10.6	-2.0
81	0.10	-1.9	-10.3	-119.0	0.2	-2.8	-1.0
82	0.00	-1.9	-9.6	-119.3	0.2	-2.8	-1.0
82	0.10	-1.9	-8.5	-89.3	0.2	-13.2	-0.1
83	0.00	-1.9	-6.9	-89.5	0.1	-13.2	-0.1
83	0.10	-1.9	-5.8	-59.5	0.1	-20.7	0.6
84	0.00	-1.9	-4.3	-59.7	0.1	-20.7	0.6
84	0.10	-1.9	-3.3	-29.7	0.1	-25.1	1.0
85	0.00	-1.9	-1.8	-29.9	0.0	-25.1	1.0

85	0.10	-1.9	-0.8	0.1	0.0	-26.6	1.1
86	0.00	-1.9	0.8	-0.1	-0.0	-26.6	1.1
86	0.10	-1.9	1.8	29.9	-0.0	-25.1	1.0
87	0.00	-1.9	3.3	29.7	-0.1	-25.1	1.0
87	0.10	-1.9	4.3	59.7	-0.1	-20.7	0.6
88	0.00	-1.9	5.8	59.5	-0.1	-20.7	0.6
88	0.10	-1.9	6.9	89.5	-0.1	-13.2	-0.1
89	0.00	-1.9	8.5	89.3	-0.2	-13.2	-0.1
89	0.10	-1.9	9.6	119.3	-0.2	-2.8	-1.0
90	0.00	-1.9	10.3	119.0	-0.2	-2.8	-1.0
90	0.10	-1.9	11.3	149.0	-0.2	10.6	-2.0
109	0.00	-1.8	10.5	121.0	8.6	-5.6	-1.0
109	0.10	-1.8	11.5	151.0	8.6	8.0	-2.1
110	0.00	-1.9	8.7	91.2	8.6	-16.2	-0.1
110	0.10	-1.9	9.7	121.2	8.6	-5.6	-1.0
111	0.00	-1.9	6.0	61.5	8.6	-23.9	0.5
111	0.10	-1.9	7.0	91.5	8.6	-16.2	-0.1
112	0.00	-1.9	3.4	31.6	8.7	-28.5	0.9
112	0.10	-1.9	4.4	61.6	8.7	-23.8	0.5
113	0.00	-1.9	0.9	1.8	8.7	-30.2	1.1
113	0.10	-1.9	1.9	31.8	8.7	-28.5	0.9
114	0.00	-1.9	-1.6	-28.0	8.8	-28.8	0.9
114	0.10	-1.9	-0.6	2.0	8.8	-30.1	1.1
115	0.00	-1.9	-4.1	-57.8	8.8	-24.5	0.6
115	0.10	-1.9	-3.1	-27.8	8.8	-28.8	0.9
116	0.00	-1.9	-6.7	-87.6	8.9	-17.3	-0.0
116	0.10	-1.9	-5.7	-57.6	8.9	-24.5	0.6
117	0.00	-1.9	-9.4	-117.4	8.9	-7.0	-0.9
117	0.10	-1.9	-8.4	-87.4	8.9	-17.3	-0.0
118	0.00	-1.9	-11.2	-147.1	8.9	6.2	-2.0
118	0.10	-1.9	-10.2	-117.1	8.9	-7.0	-0.9
119	0.00	4.1	0.5	-2.7	1.2	-1.9	0.0
119	0.10	4.1	1.0	-2.7	1.2	-2.2	-0.1
120	0.00	4.1	-0.3	-2.9	0.9	-1.6	-0.0
120	0.10	4.1	0.2	-2.9	0.9	-1.9	0.0
121	0.00	4.1	-0.2	-3.1	0.7	-1.3	0.0
121	0.10	4.1	0.3	-3.1	0.7	-1.7	-0.0
122	0.00	4.1	-0.2	-3.3	0.4	-1.0	0.0
122	0.10	4.1	0.3	-3.3	0.4	-1.4	-0.0
123	0.00	4.1	-0.2	-3.5	0.2	-0.7	0.0
123	0.10	4.1	0.3	-3.5	0.2	-1.0	0.0
124	0.00	4.1	-0.3	-3.7	-0.0	-0.3	0.0
124	0.10	4.1	0.2	-3.7	-0.0	-0.7	0.0
125	0.00	4.1	-0.3	-3.8	-0.2	0.0	0.0
125	0.10	4.1	0.2	-3.8	-0.2	-0.4	0.0
126	0.00	4.1	-0.3	-4.0	-0.5	0.4	-0.0
126	0.10	4.1	0.2	-4.0	-0.5	0.0	0.0
127	0.00	4.1	-0.2	-4.3	-0.8	0.8	0.0
127	0.10	4.1	0.3	-4.3	-0.8	0.4	-0.0
128	0.00	4.1	-1.0	-4.6	-1.1	1.3	-0.1
128	0.10	4.1	-0.5	-4.6	-1.1	0.8	0.0
130	0.00	273.8	42.6	0.2	0.0	10.2	-341.1
130	0.04	273.8	43.2	0.2	0.0	10.2	-342.8
133	0.00	174.5	28.7	-2.4	-0.2	20.1	-249.7
133	0.04	174.5	29.2	-2.4	-0.2	20.0	-250.9
135	0.00	4.4	-1.1	-8.6	-0.8	3.0	-0.1
135	0.10	4.4	-0.5	-8.6	-0.8	2.2	0.0
136	0.00	4.4	-0.2	-8.3	-0.5	2.2	0.0
136	0.10	4.4	0.3	-8.3	-0.5	1.4	-0.0
137	0.00	4.4	-0.3	-8.1	-0.3	1.4	-0.0
137	0.10	4.4	0.2	-8.1	-0.3	0.6	0.0
138	0.00	4.4	-0.3	-7.9	-0.0	0.6	0.0
138	0.10	4.4	0.2	-7.9	-0.0	-0.2	0.0
139	0.00	4.4	-0.3	-7.8	0.2	-0.1	0.0
139	0.10	4.4	0.2	-7.8	0.2	-0.9	0.0
140	0.00	4.4	-0.2	-7.7	0.3	-0.9	0.0
140	0.10	4.4	0.3	-7.7	0.3	-1.6	0.0
141	0.00	4.4	-0.2	-7.5	0.5	-1.6	0.0
141	0.10	4.4	0.3	-7.5	0.5	-2.4	0.0
142	0.00	4.4	-0.2	-7.4	0.7	-2.3	0.0
142	0.10	4.4	0.3	-7.4	0.7	-3.1	0.0
143	0.00	4.4	-0.3	-7.3	0.9	-3.0	0.0
143	0.10	4.4	0.2	-7.3	0.9	-3.8	0.0
144	0.00	4.3	1.1	-7.1	1.1	-3.7	0.0
144	0.10	4.3	1.6	-7.1	1.1	-4.4	-0.1
145	0.00	-2.0	-12.0	-116.9	16.7	-7.4	-2.2
145	0.10	-2.0	-11.0	-86.9	16.7	-17.6	-1.0
146	0.00	-2.0	-10.3	-87.2	16.7	-17.6	-1.1
146	0.10	-2.0	-9.3	-57.2	16.7	-24.9	-0.1

147	0.00	-2.0	-7.6	-57.4	16.7	-24.9	-0.1
147	0.10	-2.0	-6.6	-27.4	16.7	-29.1	0.6
148	0.00	-2.0	-5.0	-27.6	16.6	-29.1	0.6
148	0.10	-2.0	-4.0	2.4	16.6	-30.4	1.1
149	0.00	-2.0	-2.5	2.3	16.6	-30.4	1.1
149	0.10	-2.0	-1.5	32.3	16.6	-28.7	1.3
150	0.00	-2.0	0.0	32.1	16.5	-28.7	1.3
150	0.10	-2.0	1.0	62.1	16.5	-24.0	1.2
151	0.00	-2.0	2.5	62.0	16.5	-24.1	1.2
151	0.10	-2.0	3.6	92.0	16.5	-16.4	0.9
152	0.00	-2.0	5.1	91.9	16.4	-16.4	0.9
152	0.10	-2.0	6.1	121.9	16.4	-5.7	0.4
153	0.00	-2.0	7.8	121.8	16.3	-5.7	0.4
153	0.10	-2.0	8.8	151.8	16.3	7.9	-0.5
154	0.00	-1.9	8.9	151.6	16.3	7.9	-0.5
154	0.10	-1.9	9.9	181.6	16.3	24.6	-1.4

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RISULTATI : COMBINAZIONE 1 : SOLLECITAZIONI PILASTRI

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ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
1	0.00	-28.7	2.4	174.5	20.1	-249.7	0.2
1	0.27	-25.1	2.4	174.5	20.1	-202.6	-0.5
3	0.00	-23.4	-1.9	181.6	24.6	-201.5	-0.6
3	1.02	-9.9	-1.9	181.6	24.6	-16.3	1.4
4	0.00	-37.0	0.1	267.9	15.4	-265.2	0.0
4	1.02	-23.5	0.1	267.9	15.4	8.1	-0.1
6	0.00	-42.6	-0.2	273.8	10.2	-341.1	-0.0
6	0.27	-39.1	-0.2	273.8	10.2	-267.2	0.0
27	0.00	-0.9	-0.0	0.2	0.0	-0.2	-0.0
27	1.02	0.1	-0.0	0.2	0.0	-0.0	0.0
28	0.00	0.6	-0.0	0.1	0.0	-0.2	-0.0
28	1.02	1.6	-0.0	0.1	0.0	-0.1	0.0
29	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0
29	1.02	1.6	-0.0	0.1	0.0	-0.1	0.0
30	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0
30	1.02	1.5	-0.0	0.1	0.0	-0.1	0.0
31	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0
31	1.02	1.5	-0.0	0.1	0.0	-0.1	0.0
32	0.00	0.5	0.0	0.1	0.0	-0.2	0.0
32	1.02	1.5	0.0	0.1	0.0	-0.0	-0.0
33	0.00	0.5	0.0	0.2	0.0	-0.2	0.0
33	1.02	1.6	0.0	0.2	0.0	-0.0	-0.0
34	0.00	0.6	0.0	0.2	0.0	-0.2	0.0
34	1.02	1.7	0.0	0.2	0.0	-0.0	-0.0
35	0.00	-0.3	0.0	0.3	0.0	-0.3	0.0
35	1.02	0.7	0.0	0.3	0.0	-0.0	-0.0
36	0.00	-0.3	0.0	0.3	0.0	-0.3	0.0
36	1.02	0.8	0.0	0.3	0.0	-0.0	-0.0
37	0.00	0.6	0.0	0.2	0.0	-0.3	0.0
37	1.02	1.7	0.0	0.2	0.0	-0.0	-0.0
38	0.00	0.5	0.0	0.2	0.0	-0.2	0.0
38	1.02	1.5	0.0	0.2	0.0	-0.0	-0.0
39	0.00	0.5	0.0	0.2	0.0	-0.2	0.0
39	1.02	1.5	0.0	0.2	0.0	-0.0	-0.0
40	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0
40	1.02	1.5	-0.0	0.2	0.0	-0.0	0.0
41	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0
41	1.02	1.5	-0.0	0.2	0.0	-0.0	0.0
42	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0
42	1.02	1.6	-0.0	0.2	0.0	-0.0	0.0
43	0.00	0.6	-0.0	0.2	0.0	-0.3	-0.0
43	1.02	1.7	-0.0	0.2	0.0	-0.0	0.0
44	0.00	-0.3	-0.0	0.3	0.0	-0.3	-0.0
44	1.02	0.7	-0.0	0.3	0.0	-0.0	0.0
65	0.00	-41.6	-0.0	301.7	2.8	-376.7	-0.0
65	0.27	-38.0	-0.0	301.7	2.8	-295.2	0.0
67	0.00	-36.0	-0.0	296.1	4.4	-292.9	-0.0
67	1.02	-22.5	-0.0	296.1	4.4	9.1	0.0
68	0.00	-36.0	0.0	296.1	-4.4	-292.9	0.0
68	1.02	-22.5	0.0	296.1	-4.4	9.1	-0.0
70	0.00	-41.6	0.0	301.7	-2.8	-376.7	0.0
70	0.27	-38.0	0.0	301.7	-2.8	-295.2	-0.0
91	0.00	-0.3	-0.0	0.3	0.0	-0.3	-0.0
91	1.02	0.7	-0.0	0.3	0.0	-0.0	0.0
92	0.00	0.6	-0.0	0.2	0.0	-0.3	-0.0
92	1.02	1.7	-0.0	0.2	0.0	-0.0	0.0
93	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0
93	1.02	1.6	-0.0	0.2	0.0	-0.0	0.0

94	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0
94	1.02	1.5	-0.0	0.2	0.0	-0.1	0.0
95	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0
95	1.02	1.5	0.0	0.2	-0.0	-0.1	0.0
96	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0
96	1.02	1.5	0.0	0.2	-0.0	-0.1	-0.0
97	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0
97	1.02	1.6	0.0	0.2	-0.0	-0.0	-0.0
98	0.00	0.6	0.0	0.2	-0.0	-0.3	0.0
98	1.02	1.7	0.0	0.2	-0.0	-0.0	-0.0
99	0.00	-0.3	0.0	0.3	-0.0	-0.3	0.0
99	1.02	0.7	0.0	0.3	-0.0	-0.0	-0.0
100	0.00	-0.3	0.0	0.3	-0.0	-0.3	0.0
100	1.02	0.7	0.0	0.3	-0.0	-0.0	-0.0
101	0.00	0.6	0.0	0.2	-0.0	-0.3	0.0
101	1.02	1.7	0.0	0.2	-0.0	-0.0	-0.0
102	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0
102	1.02	1.6	0.0	0.2	-0.0	-0.0	-0.0
103	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0
103	1.02	1.5	0.0	0.2	-0.0	-0.0	-0.0
104	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0
104	1.02	1.5	0.0	0.2	-0.0	-0.0	-0.0
105	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0
105	1.02	1.5	-0.0	0.2	-0.0	-0.0	0.0
106	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0
106	1.02	1.5	-0.0	0.2	-0.0	-0.0	0.0
107	0.00	0.6	-0.0	0.2	-0.0	-0.3	-0.0
107	1.02	1.7	-0.0	0.2	-0.0	-0.0	0.0
108	0.00	-0.3	-0.0	0.3	-0.0	-0.3	-0.0
108	1.02	0.8	-0.0	0.3	-0.0	-0.0	0.0
129	0.00	-42.6	0.2	273.8	-10.2	-341.1	0.0
129	0.27	-39.1	0.2	273.8	-10.2	-267.2	-0.0
131	0.00	-37.0	-0.1	267.9	-15.4	-265.2	-0.0
131	1.02	-23.5	-0.1	267.9	-15.4	8.1	0.1
132	0.00	-23.4	1.9	181.6	-24.6	-201.5	0.6
132	1.02	-9.9	1.9	181.6	-24.6	-16.3	-1.4
134	0.00	-28.7	-2.4	174.5	-20.1	-249.7	-0.2
134	0.27	-25.1	-2.4	174.5	-20.1	-202.6	0.5
155	0.00	-0.3	-0.0	0.3	-0.0	-0.3	-0.0
155	1.02	0.7	-0.0	0.3	-0.0	-0.0	0.0
156	0.00	0.6	-0.0	0.2	-0.0	-0.2	-0.0
156	1.02	1.7	-0.0	0.2	-0.0	-0.0	0.0
157	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0
157	1.02	1.6	-0.0	0.2	-0.0	-0.0	0.0
158	0.00	0.5	-0.0	0.1	-0.0	-0.2	-0.0
158	1.02	1.5	-0.0	0.1	-0.0	-0.0	0.0
159	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0
159	1.02	1.5	0.0	0.1	-0.0	-0.1	-0.0
160	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0
160	1.02	1.5	0.0	0.1	-0.0	-0.1	-0.0
161	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0
161	1.02	1.6	0.0	0.1	-0.0	-0.1	-0.0
162	0.00	0.6	0.0	0.1	-0.0	-0.2	0.0
162	1.02	1.6	0.0	0.1	-0.0	-0.1	-0.0
163	0.00	-0.9	0.0	0.2	-0.0	-0.2	0.0
163	1.02	0.1	0.0	0.2	-0.0	-0.0	-0.0

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RISULTATI : COMBINAZIONE 2 : SOLLECITAZIONI TRAVI

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ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
2	0.00	116.3	22.0	1.7	0.1	-13.4	-166.5
2	0.04	116.3	22.4	1.7	0.1	-13.3	-167.4
5	0.00	182.6	32.8	-0.2	-0.0	-6.8	-227.4
5	0.04	182.6	33.2	-0.2	-0.0	-6.8	-228.7
7	0.00	3.2	-1.3	4.7	-0.7	-3.0	-0.1
7	0.10	3.2	-0.9	4.7	-0.7	-2.5	0.0
8	0.00	3.2	-0.2	4.8	-0.6	-2.5	0.0
8	0.10	3.2	0.2	4.8	-0.6	-2.0	0.0
9	0.00	3.2	-0.2	4.9	-0.5	-2.0	0.0
9	0.10	3.2	0.2	4.9	-0.5	-1.6	0.0
10	0.00	3.2	-0.2	5.0	-0.3	-1.6	0.0
10	0.10	3.2	0.1	5.0	-0.3	-1.1	0.0
11	0.00	3.2	-0.2	5.1	-0.2	-1.1	0.0
11	0.10	3.2	0.2	5.1	-0.2	-0.6	0.0
12	0.00	3.2	-0.2	5.2	-0.1	-0.6	0.0
12	0.10	3.2	0.2	5.2	-0.1	-0.1	0.0
13	0.00	3.2	-0.1	5.3	0.0	-0.1	0.0
13	0.10	3.2	0.3	5.3	0.0	0.4	0.0
14	0.00	3.2	-0.1	5.4	0.2	0.4	0.0

14	0.10	3.2	0.3	5.4	0.2	0.9	-0.0
15	0.00	3.2	-0.2	5.5	0.3	0.9	-0.0
15	0.10	3.2	0.2	5.5	0.3	1.5	0.0
16	0.00	3.2	0.4	5.7	0.5	1.5	0.0
16	0.10	3.2	0.8	5.7	0.5	2.0	-0.1
17	0.00	-1.5	-7.6	-121.1	-10.9	16.4	-1.1
17	0.10	-1.5	-6.8	-101.1	-10.9	5.3	-0.3
18	0.00	-1.5	-6.7	-101.2	-10.9	5.3	-0.3
18	0.10	-1.5	-5.9	-81.2	-10.9	-3.8	0.3
19	0.00	-1.5	-4.7	-81.3	-10.9	-3.8	0.3
19	0.10	-1.5	-3.9	-61.3	-10.9	-10.9	0.7
20	0.00	-1.5	-2.7	-61.3	-11.0	-10.9	0.7
20	0.10	-1.5	-1.9	-41.3	-11.0	-16.0	0.9
21	0.00	-1.5	-0.8	-41.4	-11.0	-16.0	0.9
21	0.10	-1.5	0.0	-21.4	-11.0	-19.2	1.0
22	0.00	-1.5	1.2	-21.5	-11.0	-19.1	1.0
22	0.10	-1.5	2.0	-1.5	-11.0	-20.3	0.8
23	0.00	-1.5	3.1	-1.6	-11.1	-20.3	0.8
23	0.10	-1.5	3.9	18.4	-11.1	-19.4	0.5
24	0.00	-1.5	5.1	18.3	-11.1	-19.4	0.5
24	0.10	-1.5	5.9	38.3	-11.1	-16.6	-0.1
25	0.00	-1.5	7.2	38.1	-11.1	-16.6	-0.1
25	0.10	-1.5	7.9	58.1	-11.1	-11.8	-0.8
26	0.00	-1.5	8.5	58.0	-11.1	-11.7	-0.8
26	0.10	-1.5	9.3	78.0	-11.1	-4.9	-1.7
45	0.00	-1.4	7.8	78.1	-5.9	-4.7	-0.7
45	0.10	-1.4	8.6	98.1	-5.9	4.1	-1.5
46	0.00	-1.4	6.5	58.3	-5.9	-11.5	-0.0
46	0.10	-1.4	7.2	78.3	-5.9	-4.7	-0.7
47	0.00	-1.4	4.4	38.4	-5.9	-16.4	0.4
47	0.10	-1.4	5.2	58.4	-5.9	-11.5	-0.0
48	0.00	-1.4	2.4	18.6	-5.9	-19.2	0.7
48	0.10	-1.4	3.2	38.6	-5.9	-16.4	0.4
49	0.00	-1.4	0.5	-1.3	-5.9	-20.1	0.8
49	0.10	-1.4	1.3	18.7	-5.9	-19.2	0.7
50	0.00	-1.4	-1.5	-21.2	-5.8	-19.0	0.7
50	0.10	-1.4	-0.7	-1.2	-5.8	-20.1	0.8
51	0.00	-1.4	-3.4	-41.1	-5.8	-15.9	0.4
51	0.10	-1.4	-2.6	-21.1	-5.8	-19.0	0.7
52	0.00	-1.4	-5.4	-61.0	-5.8	-10.8	-0.1
52	0.10	-1.4	-4.6	-41.0	-5.8	-15.9	0.4
53	0.00	-1.4	-7.5	-80.8	-5.7	-3.7	-0.8
53	0.10	-1.4	-6.7	-60.8	-5.7	-10.8	-0.1
54	0.00	-1.4	-8.8	-100.7	-5.7	5.3	-1.6
54	0.10	-1.4	-8.0	-80.7	-5.7	-3.7	-0.8
55	0.00	2.9	0.4	3.0	0.7	0.6	0.0
55	0.10	2.9	0.8	3.0	0.7	0.9	-0.1
56	0.00	2.9	-0.2	2.8	0.5	0.3	-0.0
56	0.10	2.9	0.2	2.8	0.5	0.6	0.0
57	0.00	2.9	-0.1	2.7	0.3	0.0	0.0
57	0.10	2.9	0.2	2.7	0.3	0.3	-0.0
58	0.00	2.9	-0.1	2.6	0.2	-0.2	0.0
58	0.10	2.9	0.2	2.6	0.2	0.0	0.0
59	0.00	2.9	-0.2	2.4	0.0	-0.5	0.0
59	0.10	2.9	0.2	2.4	0.0	-0.2	0.0
60	0.00	2.9	-0.2	2.3	-0.1	-0.7	0.0
60	0.10	2.9	0.2	2.3	-0.1	-0.5	0.0
61	0.00	2.9	-0.3	2.2	-0.3	-0.9	-0.0
61	0.10	2.9	0.1	2.2	-0.3	-0.7	0.0
62	0.00	2.9	-0.3	2.1	-0.4	-1.1	-0.0
62	0.10	2.9	0.1	2.1	-0.4	-0.9	0.0
63	0.00	2.9	-0.2	1.9	-0.6	-1.3	0.0
63	0.10	2.9	0.2	1.9	-0.6	-1.1	-0.0
64	0.00	2.9	-0.8	1.8	-0.8	-1.4	-0.1
64	0.10	2.9	-0.4	1.8	-0.8	-1.3	0.0
66	0.00	201.1	32.0	-0.0	-0.0	-1.9	-251.1
66	0.04	201.1	32.4	-0.0	-0.0	-1.9	-252.4
69	0.00	201.1	32.0	0.0	0.0	1.9	-251.1
69	0.04	201.1	32.4	0.0	0.0	1.9	-252.4
71	0.00	2.9	-0.8	-0.7	-0.8	-0.2	-0.1
71	0.10	2.9	-0.4	-0.7	-0.8	-0.3	0.0
72	0.00	2.9	-0.2	-0.5	-0.6	-0.3	0.0
72	0.10	2.9	0.2	-0.5	-0.6	-0.3	-0.0
73	0.00	2.9	-0.3	-0.3	-0.4	-0.3	-0.0
73	0.10	2.9	0.1	-0.3	-0.4	-0.3	0.0
74	0.00	2.9	-0.3	-0.2	-0.2	-0.4	0.0
74	0.10	2.9	0.1	-0.2	-0.2	-0.4	0.0
75	0.00	2.9	-0.2	-0.1	-0.1	-0.4	0.0
75	0.10	2.9	0.2	-0.1	-0.1	-0.4	0.0

76	0.00	2.9	-0.2	0.1	0.1	-0.4	0.0
76	0.10	2.9	0.2	0.1	0.1	-0.4	0.0
77	0.00	2.9	-0.1	0.2	0.2	-0.4	0.0
77	0.10	2.9	0.3	0.2	0.2	-0.4	0.0
78	0.00	2.9	-0.1	0.3	0.4	-0.3	0.0
78	0.10	2.9	0.3	0.3	0.4	-0.3	-0.0
79	0.00	2.9	-0.2	0.5	0.6	-0.3	-0.0
79	0.10	2.9	0.2	0.5	0.6	-0.3	0.0
80	0.00	2.9	0.4	0.7	0.8	-0.3	0.0
80	0.10	2.9	0.8	0.7	0.8	-0.2	-0.1
81	0.00	-1.4	-8.7	-99.3	0.1	7.1	-1.6
81	0.10	-1.4	-7.9	-79.3	0.1	-1.9	-0.7
82	0.00	-1.4	-7.4	-79.5	0.1	-1.9	-0.7
82	0.10	-1.4	-6.6	-59.5	0.1	-8.8	-0.0
83	0.00	-1.4	-5.3	-59.7	0.1	-8.8	-0.0
83	0.10	-1.4	-4.5	-39.7	0.1	-13.8	0.4
84	0.00	-1.4	-3.3	-39.8	0.1	-13.8	0.4
84	0.10	-1.4	-2.5	-19.8	0.1	-16.8	0.7
85	0.00	-1.4	-1.4	-19.9	0.0	-16.8	0.7
85	0.10	-1.4	-0.6	0.1	0.0	-17.7	0.8
86	0.00	-1.4	0.6	-0.1	-0.0	-17.7	0.8
86	0.10	-1.4	1.4	19.9	-0.0	-16.8	0.7
87	0.00	-1.4	2.5	19.8	-0.1	-16.8	0.7
87	0.10	-1.4	3.3	39.8	-0.1	-13.8	0.4
88	0.00	-1.4	4.5	39.7	-0.1	-13.8	0.4
88	0.10	-1.4	5.3	59.7	-0.1	-8.8	-0.0
89	0.00	-1.4	6.6	59.5	-0.1	-8.8	-0.0
89	0.10	-1.4	7.4	79.5	-0.1	-1.9	-0.7
90	0.00	-1.4	7.9	79.3	-0.1	-1.9	-0.7
90	0.10	-1.4	8.7	99.3	-0.1	7.1	-1.6
109	0.00	-1.4	8.0	80.7	5.7	-3.7	-0.8
109	0.10	-1.4	8.8	100.7	5.7	5.3	-1.6
110	0.00	-1.4	6.7	60.8	5.7	-10.8	-0.1
110	0.10	-1.4	7.5	80.8	5.7	-3.7	-0.8
111	0.00	-1.4	4.6	41.0	5.8	-15.9	0.4
111	0.10	-1.4	5.4	61.0	5.8	-10.8	-0.1
112	0.00	-1.4	2.6	21.1	5.8	-19.0	0.7
112	0.10	-1.4	3.4	41.1	5.8	-15.9	0.4
113	0.00	-1.4	0.7	1.2	5.8	-20.1	0.8
113	0.10	-1.4	1.5	21.2	5.8	-19.0	0.7
114	0.00	-1.4	-1.3	-18.7	5.9	-19.2	0.7
114	0.10	-1.4	-0.5	1.3	5.9	-20.1	0.8
115	0.00	-1.4	-3.2	-38.6	5.9	-16.4	0.4
115	0.10	-1.4	-2.4	-18.6	5.9	-19.2	0.7
116	0.00	-1.4	-5.2	-58.4	5.9	-11.5	-0.0
116	0.10	-1.4	-4.4	-38.4	5.9	-16.4	0.4
117	0.00	-1.4	-7.2	-78.3	5.9	-4.7	-0.7
117	0.10	-1.4	-6.5	-58.3	5.9	-11.5	-0.0
118	0.00	-1.4	-8.6	-98.1	5.9	4.1	-1.5
118	0.10	-1.4	-7.8	-78.1	5.9	-4.7	-0.7
119	0.00	2.9	0.4	-1.8	0.8	-1.3	0.0
119	0.10	2.9	0.8	-1.8	0.8	-1.4	-0.1
120	0.00	2.9	-0.2	-1.9	0.6	-1.1	-0.0
120	0.10	2.9	0.2	-1.9	0.6	-1.3	0.0
121	0.00	2.9	-0.1	-2.1	0.4	-0.9	0.0
121	0.10	2.9	0.3	-2.1	0.4	-1.1	-0.0
122	0.00	2.9	-0.1	-2.2	0.3	-0.7	0.0
122	0.10	2.9	0.3	-2.2	0.3	-0.9	-0.0
123	0.00	2.9	-0.2	-2.3	0.1	-0.5	0.0
123	0.10	2.9	0.2	-2.3	0.1	-0.7	0.0
124	0.00	2.9	-0.2	-2.4	-0.0	-0.2	0.0
124	0.10	2.9	0.2	-2.4	-0.0	-0.5	0.0
125	0.00	2.9	-0.2	-2.6	-0.2	0.0	0.0
125	0.10	2.9	0.1	-2.6	-0.2	-0.2	0.0
126	0.00	2.9	-0.2	-2.7	-0.3	0.3	-0.0
126	0.10	2.9	0.1	-2.7	-0.3	0.0	0.0
127	0.00	2.9	-0.2	-2.8	-0.5	0.6	0.0
127	0.10	2.9	0.2	-2.8	-0.5	0.3	-0.0
128	0.00	2.9	-0.8	-3.0	-0.7	0.9	-0.1
128	0.10	2.9	-0.4	-3.0	-0.7	0.6	0.0
130	0.00	182.6	32.8	0.2	0.0	6.8	-227.4
130	0.04	182.6	33.2	0.2	0.0	6.8	-228.7
133	0.00	116.3	22.0	-1.7	-0.1	13.4	-166.5
133	0.04	116.3	22.4	-1.7	-0.1	13.3	-167.4
135	0.00	3.2	-0.8	-5.7	-0.5	2.0	-0.1
135	0.10	3.2	-0.4	-5.7	-0.5	1.5	0.0
136	0.00	3.2	-0.2	-5.5	-0.3	1.5	0.0
136	0.10	3.2	0.2	-5.5	-0.3	0.9	-0.0

137	0.00	3.2	-0.3	-5.4	-0.2	0.9	-0.0
137	0.10	3.2	0.1	-5.4	-0.2	0.4	0.0
138	0.00	3.2	-0.3	-5.3	-0.0	0.4	0.0
138	0.10	3.2	0.1	-5.3	-0.0	-0.1	0.0
139	0.00	3.2	-0.2	-5.2	0.1	-0.1	0.0
139	0.10	3.2	0.2	-5.2	0.1	-0.6	0.0
140	0.00	3.2	-0.2	-5.1	0.2	-0.6	0.0
140	0.10	3.2	0.2	-5.1	0.2	-1.1	0.0
141	0.00	3.2	-0.1	-5.0	0.3	-1.1	0.0
141	0.10	3.2	0.2	-5.0	0.3	-1.6	0.0
142	0.00	3.2	-0.2	-4.9	0.5	-1.6	0.0
142	0.10	3.2	0.2	-4.9	0.5	-2.0	0.0
143	0.00	3.2	-0.2	-4.8	0.6	-2.0	0.0
143	0.10	3.2	0.2	-4.8	0.6	-2.5	0.0
144	0.00	3.2	0.9	-4.7	0.7	-2.5	0.0
144	0.10	3.2	1.3	-4.7	0.7	-3.0	-0.1
145	0.00	-1.5	-9.3	-78.0	11.1	-4.9	-1.7
145	0.10	-1.5	-8.5	-58.0	11.1	-11.7	-0.8
146	0.00	-1.5	-7.9	-58.1	11.1	-11.8	-0.8
146	0.10	-1.5	-7.2	-38.1	11.1	-16.6	-0.1
147	0.00	-1.5	-5.9	-38.3	11.1	-16.6	-0.1
147	0.10	-1.5	-5.1	-18.3	11.1	-19.4	0.5
148	0.00	-1.5	-3.9	-18.4	11.1	-19.4	0.5
148	0.10	-1.5	-3.1	1.6	11.1	-20.3	0.8
149	0.00	-1.5	-2.0	1.5	11.0	-20.3	0.8
149	0.10	-1.5	-1.2	21.5	11.0	-19.1	1.0
150	0.00	-1.5	-0.0	21.4	11.0	-19.2	1.0
150	0.10	-1.5	0.8	41.4	11.0	-16.0	0.9
151	0.00	-1.5	1.9	41.3	11.0	-16.0	0.9
151	0.10	-1.5	2.7	61.3	11.0	-10.9	0.7
152	0.00	-1.5	3.9	61.3	10.9	-10.9	0.7
152	0.10	-1.5	4.7	81.3	10.9	-3.8	0.3
153	0.00	-1.5	5.9	81.2	10.9	-3.8	0.3
153	0.10	-1.5	6.7	101.2	10.9	5.3	-0.3
154	0.00	-1.5	6.8	101.1	10.9	5.3	-0.3
154	0.10	-1.5	7.6	121.1	10.9	16.4	-1.1

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RISULTATI : COMBINAZIONE 2 : SOLLECITAZIONI PILASTRI

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ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
1	0.00	-22.0	1.7	116.3	13.4	-166.5	0.1
1	0.27	-19.3	1.7	116.3	13.4	-135.1	-0.3
3	0.00	-18.0	-1.5	121.1	16.4	-134.3	-0.4
3	1.02	-7.6	-1.5	121.1	16.4	-10.9	1.1
4	0.00	-28.5	0.1	178.6	10.3	-176.8	0.0
4	1.02	-18.1	0.1	178.6	10.3	5.4	-0.1
6	0.00	-32.8	-0.2	182.6	6.8	-227.4	-0.0
6	0.27	-30.1	-0.2	182.6	6.8	-178.1	0.0
27	0.00	-0.7	-0.0	0.1	0.0	-0.1	-0.0
27	1.02	0.1	-0.0	0.1	0.0	-0.0	0.0
28	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
28	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
29	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
29	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
30	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
30	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
31	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
31	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
32	0.00	0.4	0.0	0.1	0.0	-0.1	0.0
32	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0
33	0.00	0.4	0.0	0.1	0.0	-0.1	0.0
33	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0
34	0.00	0.5	0.0	0.1	0.0	-0.2	0.0
34	1.02	1.3	0.0	0.1	0.0	-0.0	-0.0
35	0.00	-0.3	0.0	0.2	0.0	-0.2	0.0
35	1.02	0.5	0.0	0.2	0.0	-0.0	-0.0
36	0.00	-0.2	0.0	0.2	0.0	-0.2	0.0
36	1.02	0.6	0.0	0.2	0.0	-0.0	-0.0
37	0.00	0.5	0.0	0.2	0.0	-0.2	0.0
37	1.02	1.3	0.0	0.2	0.0	-0.0	-0.0
38	0.00	0.4	0.0	0.1	0.0	-0.2	0.0
38	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0
39	0.00	0.4	0.0	0.1	0.0	-0.2	0.0
39	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0
40	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
40	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
41	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
41	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
42	0.00	0.4	-0.0	0.1	0.0	-0.2	-0.0

42	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
43	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0
43	1.02	1.3	-0.0	0.1	0.0	-0.0	0.0
44	0.00	-0.2	-0.0	0.2	0.0	-0.2	-0.0
44	1.02	0.6	-0.0	0.2	0.0	-0.0	0.0
65	0.00	-32.0	-0.0	201.1	1.9	-251.1	-0.0
65	0.27	-29.2	-0.0	201.1	1.9	-196.8	0.0
67	0.00	-27.7	-0.0	197.4	2.9	-195.3	-0.0
67	1.02	-17.3	-0.0	197.4	2.9	6.1	0.0
68	0.00	-27.7	0.0	197.4	-2.9	-195.3	0.0
68	1.02	-17.3	0.0	197.4	-2.9	6.1	-0.0
70	0.00	-32.0	0.0	201.1	-1.9	-251.1	0.0
70	0.27	-29.2	0.0	201.1	-1.9	-196.8	-0.0
91	0.00	-0.3	-0.0	0.2	0.0	-0.2	-0.0
91	1.02	0.5	-0.0	0.2	0.0	-0.0	0.0
92	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0
92	1.02	1.3	-0.0	0.2	0.0	-0.0	0.0
93	0.00	0.4	-0.0	0.1	0.0	-0.2	-0.0
93	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
94	0.00	0.4	-0.0	0.1	0.0	-0.2	-0.0
94	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
95	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
95	1.02	1.2	0.0	0.1	-0.0	-0.0	0.0
96	0.00	0.4	0.0	0.1	-0.0	-0.2	0.0
96	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
97	0.00	0.4	0.0	0.1	-0.0	-0.2	0.0
97	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
98	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0
98	1.02	1.3	0.0	0.2	-0.0	-0.0	-0.0
99	0.00	-0.3	0.0	0.2	-0.0	-0.2	0.0
99	1.02	0.5	0.0	0.2	-0.0	-0.0	-0.0
100	0.00	-0.2	0.0	0.2	-0.0	-0.2	0.0
100	1.02	0.6	0.0	0.2	-0.0	-0.0	-0.0
101	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0
101	1.02	1.3	0.0	0.1	-0.0	-0.0	-0.0
102	0.00	0.4	0.0	0.1	-0.0	-0.2	0.0
102	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
103	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
103	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
104	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
104	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
105	0.00	0.4	-0.0	0.1	-0.0	-0.2	-0.0
105	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0
106	0.00	0.4	-0.0	0.1	-0.0	-0.2	-0.0
106	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0
107	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0
107	1.02	1.3	-0.0	0.2	-0.0	-0.0	0.0
108	0.00	-0.2	-0.0	0.2	-0.0	-0.2	-0.0
108	1.02	0.6	-0.0	0.2	-0.0	-0.0	0.0
129	0.00	-32.8	0.2	182.6	-6.8	-227.4	0.0
129	0.27	-30.1	0.2	182.6	-6.8	-178.1	-0.0
131	0.00	-28.5	-0.1	178.6	-10.3	-176.8	-0.0
131	1.02	-18.1	-0.1	178.6	-10.3	5.4	0.1
132	0.00	-18.0	1.5	121.1	-16.4	-134.3	0.4
132	1.02	-7.6	1.5	121.1	-16.4	-10.9	-1.1
134	0.00	-22.0	-1.7	116.3	-13.4	-166.5	-0.1
134	0.27	-19.3	-1.7	116.3	-13.4	-135.1	0.3
155	0.00	-0.3	-0.0	0.2	-0.0	-0.2	-0.0
155	1.02	0.5	-0.0	0.2	-0.0	-0.0	0.0
156	0.00	0.5	-0.0	0.1	-0.0	-0.2	-0.0
156	1.02	1.3	-0.0	0.1	-0.0	-0.0	0.0
157	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0
157	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0
158	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0
158	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0
159	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
159	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
160	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
160	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
161	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
161	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
162	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
162	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
163	0.00	-0.7	0.0	0.1	-0.0	-0.1	0.0
163	1.02	0.1	0.0	0.1	-0.0	-0.0	-0.0

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RISULTATI : COMBINAZIONE 3 : SOLLECITAZIONI TRAVI

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ELEM.	ascissa	N	V2	V3	T	M2	M3
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)

2	0.00	58.2	21.9	1.2	0.0	-6.7	-83.3
2	0.04	58.2	22.3	1.2	0.0	-6.7	-84.1
5	0.00	91.3	32.9	-0.4	-0.0	-3.4	-113.7
5	0.04	91.3	33.3	-0.4	-0.0	-3.4	-115.0
7	0.00	2.6	-1.3	2.4	-0.4	-1.5	-0.1
7	0.10	2.6	-0.9	2.4	-0.4	-1.2	0.0
8	0.00	2.6	-0.2	2.4	-0.3	-1.3	0.0
8	0.10	2.6	0.2	2.4	-0.3	-1.0	0.0
9	0.00	2.6	-0.2	2.5	-0.2	-1.0	0.0
9	0.10	2.6	0.2	2.5	-0.2	-0.8	0.0
10	0.00	2.6	-0.2	2.5	-0.2	-0.8	0.0
10	0.10	2.6	0.1	2.5	-0.2	-0.5	0.0
11	0.00	2.6	-0.2	2.5	-0.1	-0.5	0.0
11	0.10	2.6	0.2	2.5	-0.1	-0.3	0.0
12	0.00	2.6	-0.2	2.6	-0.1	-0.3	0.0
12	0.10	2.6	0.2	2.6	-0.1	-0.0	0.0
13	0.00	2.6	-0.1	2.6	0.0	-0.1	0.0
13	0.10	2.6	0.3	2.6	0.0	0.2	0.0
14	0.00	2.6	-0.1	2.7	0.1	0.2	0.0
14	0.10	2.6	0.3	2.7	0.1	0.5	-0.0
15	0.00	2.6	-0.2	2.8	0.2	0.5	-0.0
15	0.10	2.6	0.2	2.8	0.2	0.7	0.0
16	0.00	2.6	0.4	2.9	0.3	0.7	0.0
16	0.10	2.6	0.8	2.9	0.3	1.0	-0.1
17	0.00	-1.4	-7.5	-60.5	-5.4	8.2	-1.0
17	0.10	-1.4	-6.7	-50.5	-5.4	2.6	-0.3
18	0.00	-1.4	-6.6	-50.6	-5.4	2.6	-0.3
18	0.10	-1.4	-5.9	-40.6	-5.4	-1.9	0.3
19	0.00	-1.4	-4.6	-40.6	-5.5	-1.9	0.3
19	0.10	-1.4	-3.8	-30.6	-5.5	-5.5	0.7
20	0.00	-1.4	-2.6	-30.7	-5.5	-5.5	0.7
20	0.10	-1.4	-1.8	-20.7	-5.5	-8.0	1.0
21	0.00	-1.4	-0.7	-20.7	-5.5	-8.0	1.0
21	0.10	-1.4	0.1	-10.7	-5.5	-9.6	1.0
22	0.00	-1.4	1.3	-10.8	-5.5	-9.6	1.0
22	0.10	-1.4	2.0	-0.8	-5.5	-10.1	0.8
23	0.00	-1.4	3.2	-0.8	-5.5	-10.1	0.8
23	0.10	-1.4	4.0	9.2	-5.5	-9.7	0.5
24	0.00	-1.4	5.2	9.1	-5.6	-9.7	0.5
24	0.10	-1.4	6.0	19.1	-5.6	-8.3	-0.1
25	0.00	-1.4	7.3	19.1	-5.6	-8.3	-0.1
25	0.10	-1.4	8.0	29.1	-5.6	-5.9	-0.9
26	0.00	-1.4	8.6	29.0	-5.6	-5.9	-0.9
26	0.10	-1.4	9.3	39.0	-5.6	-2.5	-1.7
45	0.00	-1.2	7.9	39.0	-3.0	-2.3	-0.7
45	0.10	-1.2	8.6	49.0	-3.0	2.1	-1.5
46	0.00	-1.2	6.5	29.1	-3.0	-5.8	-0.0
46	0.10	-1.2	7.3	39.1	-3.0	-2.3	-0.7
47	0.00	-1.2	4.4	19.2	-3.0	-8.2	0.4
47	0.10	-1.2	5.2	29.2	-3.0	-5.8	-0.0
48	0.00	-1.2	2.4	9.3	-2.9	-9.6	0.7
48	0.10	-1.2	3.2	19.3	-2.9	-8.2	0.4
49	0.00	-1.2	0.5	-0.7	-2.9	-10.0	0.8
49	0.10	-1.2	1.3	9.3	-2.9	-9.6	0.7
50	0.00	-1.2	-1.5	-10.6	-2.9	-9.5	0.7
50	0.10	-1.2	-0.7	-0.6	-2.9	-10.1	0.8
51	0.00	-1.2	-3.4	-20.5	-2.9	-7.9	0.4
51	0.10	-1.2	-2.6	-10.5	-2.9	-9.5	0.7
52	0.00	-1.2	-5.4	-30.5	-2.9	-5.4	-0.1
52	0.10	-1.2	-4.6	-20.5	-2.9	-8.0	0.4
53	0.00	-1.2	-7.4	-40.4	-2.9	-1.9	-0.8
53	0.10	-1.2	-6.7	-30.4	-2.9	-5.4	-0.1
54	0.00	-1.2	-8.8	-50.3	-2.9	2.7	-1.6
54	0.10	-1.2	-8.0	-40.3	-2.9	-1.9	-0.8
55	0.00	2.0	0.4	1.5	0.4	0.3	0.0
55	0.10	2.0	0.8	1.5	0.4	0.4	-0.1
56	0.00	2.1	-0.2	1.4	0.3	0.1	-0.0
56	0.10	2.1	0.2	1.4	0.3	0.3	0.0
57	0.00	2.1	-0.1	1.3	0.2	0.0	0.0
57	0.10	2.1	0.3	1.3	0.2	0.1	-0.0
58	0.00	2.1	-0.1	1.3	0.1	-0.1	0.0
58	0.10	2.1	0.2	1.3	0.1	0.0	0.0
59	0.00	2.1	-0.2	1.2	0.0	-0.2	0.0
59	0.10	2.1	0.2	1.2	0.0	-0.1	0.0
60	0.00	2.1	-0.2	1.2	-0.1	-0.3	0.0
60	0.10	2.1	0.2	1.2	-0.1	-0.2	0.0
61	0.00	2.1	-0.3	1.1	-0.1	-0.5	-0.0
61	0.10	2.1	0.1	1.1	-0.1	-0.3	0.0

62	0.00	2.1	-0.3	1.0	-0.2	-0.6	-0.0
62	0.10	2.1	0.1	1.0	-0.2	-0.4	0.0
63	0.00	2.0	-0.2	1.0	-0.3	-0.6	0.0
63	0.10	2.0	0.2	1.0	-0.3	-0.5	-0.0
64	0.00	2.0	-0.8	0.9	-0.4	-0.7	-0.1
64	0.10	2.0	-0.4	0.9	-0.4	-0.6	0.0
66	0.00	100.6	32.0	-0.1	-0.0	-0.9	-125.6
66	0.04	100.6	32.4	-0.1	-0.0	-0.9	-126.8
69	0.00	100.6	32.0	0.1	0.0	0.9	-125.6
69	0.04	100.6	32.4	0.1	0.0	0.9	-126.8
71	0.00	2.0	-0.8	-0.3	-0.4	-0.1	-0.1
71	0.10	2.0	-0.4	-0.3	-0.4	-0.1	0.0
72	0.00	2.0	-0.2	-0.2	-0.3	-0.1	0.0
72	0.10	2.0	0.2	-0.2	-0.3	-0.2	-0.0
73	0.00	2.0	-0.3	-0.2	-0.2	-0.2	-0.0
73	0.10	2.0	0.1	-0.2	-0.2	-0.2	0.0
74	0.00	2.0	-0.3	-0.1	-0.1	-0.2	0.0
74	0.10	2.0	0.1	-0.1	-0.1	-0.2	0.0
75	0.00	2.0	-0.2	-0.0	-0.0	-0.2	0.0
75	0.10	2.0	0.2	-0.0	-0.0	-0.2	0.0
76	0.00	2.0	-0.2	0.0	0.0	-0.2	0.0
76	0.10	2.0	0.2	0.0	0.0	-0.2	0.0
77	0.00	2.0	-0.1	0.1	0.1	-0.2	0.0
77	0.10	2.0	0.3	0.1	0.1	-0.2	0.0
78	0.00	2.0	-0.1	0.2	0.2	-0.2	0.0
78	0.10	2.0	0.3	0.2	0.2	-0.2	-0.0
79	0.00	2.0	-0.2	0.2	0.3	-0.2	-0.0
79	0.10	2.0	0.2	0.2	0.3	-0.1	0.0
80	0.00	2.0	0.4	0.3	0.4	-0.1	0.0
80	0.10	2.0	0.8	0.3	0.4	-0.1	-0.1
81	0.00	-1.2	-8.7	-49.7	0.1	3.5	-1.6
81	0.10	-1.2	-7.9	-39.7	0.1	-0.9	-0.7
82	0.00	-1.2	-7.4	-39.8	0.1	-0.9	-0.7
82	0.10	-1.2	-6.6	-29.8	0.1	-4.4	-0.0
83	0.00	-1.2	-5.3	-29.8	0.0	-4.4	-0.0
83	0.10	-1.2	-4.5	-19.8	0.0	-6.9	0.4
84	0.00	-1.2	-3.3	-19.9	0.0	-6.9	0.4
84	0.10	-1.2	-2.5	-9.9	0.0	-8.4	0.7
85	0.00	-1.2	-1.4	-10.0	0.0	-8.4	0.7
85	0.10	-1.2	-0.6	0.0	0.0	-8.9	0.8
86	0.00	-1.2	0.6	-0.0	-0.0	-8.9	0.8
86	0.10	-1.2	1.4	10.0	-0.0	-8.4	0.7
87	0.00	-1.2	2.5	9.9	-0.0	-8.4	0.7
87	0.10	-1.2	3.3	19.9	-0.0	-6.9	0.4
88	0.00	-1.2	4.5	19.8	-0.0	-6.9	0.4
88	0.10	-1.2	5.3	29.8	-0.0	-4.4	-0.0
89	0.00	-1.2	6.6	29.8	-0.1	-4.4	-0.0
89	0.10	-1.2	7.4	39.8	-0.1	-0.9	-0.7
90	0.00	-1.2	7.9	39.7	-0.1	-0.9	-0.7
90	0.10	-1.2	8.7	49.7	-0.1	3.5	-1.6
109	0.00	-1.2	8.0	40.3	2.9	-1.9	-0.8
109	0.10	-1.2	8.8	50.3	2.9	2.7	-1.6
110	0.00	-1.2	6.7	30.4	2.9	-5.4	-0.1
110	0.10	-1.2	7.4	40.4	2.9	-1.9	-0.8
111	0.00	-1.2	4.6	20.5	2.9	-8.0	0.4
111	0.10	-1.2	5.4	30.5	2.9	-5.4	-0.1
112	0.00	-1.2	2.6	10.5	2.9	-9.5	0.7
112	0.10	-1.2	3.4	20.5	2.9	-7.9	0.4
113	0.00	-1.2	0.7	0.6	2.9	-10.1	0.8
113	0.10	-1.2	1.5	10.6	2.9	-9.5	0.7
114	0.00	-1.2	-1.3	-9.3	2.9	-9.6	0.7
114	0.10	-1.2	-0.5	0.7	2.9	-10.0	0.8
115	0.00	-1.2	-3.2	-19.3	2.9	-8.2	0.4
115	0.10	-1.2	-2.4	-9.3	2.9	-9.6	0.7
116	0.00	-1.2	-5.2	-29.2	3.0	-5.8	-0.0
116	0.10	-1.2	-4.4	-19.2	3.0	-8.2	0.4
117	0.00	-1.2	-7.3	-39.1	3.0	-2.3	-0.7
117	0.10	-1.2	-6.5	-29.1	3.0	-5.8	-0.0
118	0.00	-1.2	-8.6	-49.0	3.0	2.1	-1.5
118	0.10	-1.2	-7.9	-39.0	3.0	-2.3	-0.7
119	0.00	2.0	0.4	-0.9	0.4	-0.6	0.0
119	0.10	2.0	0.8	-0.9	0.4	-0.7	-0.1
120	0.00	2.0	-0.2	-1.0	0.3	-0.5	-0.0
120	0.10	2.0	0.2	-1.0	0.3	-0.6	0.0
121	0.00	2.1	-0.1	-1.0	0.2	-0.4	0.0
121	0.10	2.1	0.3	-1.0	0.2	-0.6	-0.0
122	0.00	2.1	-0.1	-1.1	0.1	-0.3	0.0
122	0.10	2.1	0.3	-1.1	0.1	-0.5	-0.0
123	0.00	2.1	-0.2	-1.2	0.1	-0.2	0.0

123	0.10	2.1	0.2	-1.2	0.1	-0.3	0.0
124	0.00	2.1	-0.2	-1.2	-0.0	-0.1	0.0
124	0.10	2.1	0.2	-1.2	-0.0	-0.2	0.0
125	0.00	2.1	-0.2	-1.3	-0.1	0.0	0.0
125	0.10	2.1	0.1	-1.3	-0.1	-0.1	0.0
126	0.00	2.1	-0.3	-1.3	-0.2	0.1	-0.0
126	0.10	2.1	0.1	-1.3	-0.2	0.0	0.0
127	0.00	2.1	-0.2	-1.4	-0.3	0.3	0.0
127	0.10	2.1	0.2	-1.4	-0.3	0.1	-0.0
128	0.00	2.0	-0.8	-1.5	-0.4	0.4	-0.1
128	0.10	2.0	-0.4	-1.5	-0.4	0.3	0.0
130	0.00	91.3	32.9	0.4	0.0	3.4	-113.7
130	0.04	91.3	33.3	0.4	0.0	3.4	-115.0
133	0.00	58.2	21.9	-1.2	-0.0	6.7	-83.3
133	0.04	58.2	22.3	-1.2	-0.0	6.7	-84.1
135	0.00	2.6	-0.8	-2.9	-0.3	1.0	-0.1
135	0.10	2.6	-0.4	-2.9	-0.3	0.7	0.0
136	0.00	2.6	-0.2	-2.8	-0.2	0.7	0.0
136	0.10	2.6	0.2	-2.8	-0.2	0.5	-0.0
137	0.00	2.6	-0.3	-2.7	-0.1	0.5	-0.0
137	0.10	2.6	0.1	-2.7	-0.1	0.2	0.0
138	0.00	2.6	-0.3	-2.6	-0.0	0.2	0.0
138	0.10	2.6	0.1	-2.6	-0.0	-0.1	0.0
139	0.00	2.6	-0.2	-2.6	0.1	-0.0	0.0
139	0.10	2.6	0.2	-2.6	0.1	-0.3	0.0
140	0.00	2.6	-0.2	-2.5	0.1	-0.3	0.0
140	0.10	2.6	0.2	-2.5	0.1	-0.5	0.0
141	0.00	2.6	-0.1	-2.5	0.2	-0.5	0.0
141	0.10	2.6	0.2	-2.5	0.2	-0.8	0.0
142	0.00	2.6	-0.2	-2.5	0.2	-0.8	0.0
142	0.10	2.6	0.2	-2.5	0.2	-1.0	0.0
143	0.00	2.6	-0.2	-2.4	0.3	-1.0	0.0
143	0.10	2.6	0.2	-2.4	0.3	-1.3	0.0
144	0.00	2.6	0.9	-2.4	0.4	-1.2	0.0
144	0.10	2.6	1.3	-2.4	0.4	-1.5	-0.1
145	0.00	-1.4	-9.3	-39.0	5.6	-2.5	-1.7
145	0.10	-1.4	-8.6	-29.0	5.6	-5.9	-0.9
146	0.00	-1.4	-8.0	-29.1	5.6	-5.9	-0.9
146	0.10	-1.4	-7.3	-19.1	5.6	-8.3	-0.1
147	0.00	-1.4	-6.0	-19.1	5.6	-8.3	-0.1
147	0.10	-1.4	-5.2	-9.1	5.6	-9.7	0.5
148	0.00	-1.4	-4.0	-9.2	5.5	-9.7	0.5
148	0.10	-1.4	-3.2	0.8	5.5	-10.1	0.8
149	0.00	-1.4	-2.0	0.8	5.5	-10.1	0.8
149	0.10	-1.4	-1.3	10.8	5.5	-9.6	1.0
150	0.00	-1.4	-0.1	10.7	5.5	-9.6	1.0
150	0.10	-1.4	0.7	20.7	5.5	-8.0	1.0
151	0.00	-1.4	1.8	20.7	5.5	-8.0	1.0
151	0.10	-1.4	2.6	30.7	5.5	-5.5	0.7
152	0.00	-1.4	3.8	30.6	5.5	-5.5	0.7
152	0.10	-1.4	4.6	40.6	5.5	-1.9	0.3
153	0.00	-1.4	5.9	40.6	5.4	-1.9	0.3
153	0.10	-1.4	6.6	50.6	5.4	2.6	-0.3
154	0.00	-1.4	6.7	50.5	5.4	2.6	-0.3
154	0.10	-1.4	7.5	60.5	5.4	8.2	-1.0

RISULTATI : COMBINAZIONE 3 : SOLLECITAZIONI PILASTRI							
ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
1	0.00	-21.9	1.2	58.2	6.7	-83.3	0.0
1	0.27	-19.2	1.2	58.2	6.7	-67.5	-0.3
3	0.00	-17.9	-1.4	60.5	8.2	-67.2	-0.4
3	1.02	-7.5	-1.4	60.5	8.2	-5.4	1.0
4	0.00	-28.6	0.2	89.3	5.1	-88.4	0.1
4	1.02	-18.2	0.2	89.3	5.1	2.7	-0.1
6	0.00	-32.9	-0.4	91.3	3.4	-113.7	-0.0
6	0.27	-30.1	-0.4	91.3	3.4	-89.0	0.1
27	0.00	-0.7	-0.0	0.1	0.0	-0.1	-0.0
27	1.02	0.1	-0.0	0.1	0.0	-0.0	0.0
28	0.00	0.4	-0.0	0.0	0.0	-0.1	-0.0
28	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
29	0.00	0.4	-0.0	0.0	0.0	-0.1	-0.0
29	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
30	0.00	0.4	-0.0	0.0	0.0	-0.1	-0.0
30	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
31	0.00	0.4	0.0	0.0	0.0	-0.1	0.0
31	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0
32	0.00	0.4	0.0	0.0	0.0	-0.1	0.0
32	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0

33	0.00	0.4	0.0	0.1	0.0	-0.1	0.0
33	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0
34	0.00	0.5	0.0	0.1	0.0	-0.1	0.0
34	1.02	1.3	0.0	0.1	0.0	-0.0	-0.0
35	0.00	-0.3	0.0	0.1	0.0	-0.1	0.0
35	1.02	0.5	0.0	0.1	0.0	-0.0	-0.0
36	0.00	-0.2	0.0	0.1	0.0	-0.1	0.0
36	1.02	0.6	0.0	0.1	0.0	-0.0	-0.0
37	0.00	0.5	0.0	0.1	0.0	-0.1	0.0
37	1.02	1.3	0.0	0.1	0.0	-0.0	-0.0
38	0.00	0.4	0.0	0.1	0.0	-0.1	0.0
38	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0
39	0.00	0.4	0.0	0.1	0.0	-0.1	0.0
39	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0
40	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
40	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
41	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
41	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
42	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
42	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
43	0.00	0.5	-0.0	0.1	0.0	-0.1	-0.0
43	1.02	1.3	-0.0	0.1	0.0	-0.0	0.0
44	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0
44	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0
65	0.00	-32.0	-0.1	100.6	0.9	-125.6	-0.0
65	0.27	-29.3	-0.1	100.6	0.9	-98.4	0.0
67	0.00	-27.7	-0.0	98.7	1.5	-97.6	0.0
67	1.02	-17.3	-0.0	98.7	1.5	3.0	0.0
68	0.00	-27.7	0.0	98.7	-1.5	-97.6	-0.0
68	1.02	-17.3	0.0	98.7	-1.5	3.0	-0.0
70	0.00	-32.0	0.1	100.6	-0.9	-125.6	0.0
70	0.27	-29.3	0.1	100.6	-0.9	-98.4	-0.0
91	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0
91	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0
92	0.00	0.5	-0.0	0.1	0.0	-0.1	-0.0
92	1.02	1.3	-0.0	0.1	0.0	-0.0	0.0
93	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
93	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
94	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0
94	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0
95	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
95	1.02	1.2	0.0	0.1	-0.0	-0.0	0.0
96	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
96	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
97	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
97	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
98	0.00	0.5	0.0	0.1	-0.0	-0.1	0.0
98	1.02	1.3	0.0	0.1	-0.0	-0.0	-0.0
99	0.00	-0.2	0.0	0.1	-0.0	-0.1	0.0
99	1.02	0.6	0.0	0.1	-0.0	-0.0	-0.0
100	0.00	-0.2	0.0	0.1	-0.0	-0.1	0.0
100	1.02	0.6	0.0	0.1	-0.0	-0.0	-0.0
101	0.00	0.5	0.0	0.1	-0.0	-0.1	0.0
101	1.02	1.3	0.0	0.1	-0.0	-0.0	-0.0
102	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
102	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
103	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
103	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
104	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0
104	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0
105	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0
105	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0
106	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0
106	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0
107	0.00	0.5	-0.0	0.1	-0.0	-0.1	-0.0
107	1.02	1.3	-0.0	0.1	-0.0	-0.0	0.0
108	0.00	-0.2	-0.0	0.1	-0.0	-0.1	-0.0
108	1.02	0.6	-0.0	0.1	-0.0	-0.0	0.0
129	0.00	-32.9	0.4	91.3	-3.4	-113.7	0.0
129	0.27	-30.1	0.4	91.3	-3.4	-89.0	-0.1
131	0.00	-28.6	-0.2	89.3	-5.1	-88.4	-0.1
131	1.02	-18.2	-0.2	89.3	-5.1	2.7	0.1
132	0.00	-17.9	1.4	60.5	-8.2	-67.2	0.4
132	1.02	-7.5	1.4	60.5	-8.2	-5.4	-1.0
134	0.00	-21.9	-1.2	58.2	-6.7	-83.3	-0.0
134	0.27	-19.2	-1.2	58.2	-6.7	-67.5	0.3
155	0.00	-0.3	-0.0	0.1	-0.0	-0.1	-0.0
155	1.02	0.5	-0.0	0.1	-0.0	-0.0	0.0

156	0.00	0.5	-0.0	0.1	-0.0	-0.1	-0.0
156	1.02	1.3	-0.0	0.1	-0.0	-0.0	0.0
157	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0
157	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0
158	0.00	0.4	-0.0	0.0	-0.0	-0.1	-0.0
158	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0
159	0.00	0.4	-0.0	0.0	-0.0	-0.1	-0.0
159	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0
160	0.00	0.4	0.0	0.0	-0.0	-0.1	0.0
160	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
161	0.00	0.4	0.0	0.0	-0.0	-0.1	0.0
161	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
162	0.00	0.4	0.0	0.0	-0.0	-0.1	0.0
162	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
163	0.00	-0.7	0.0	0.1	-0.0	-0.1	0.0
163	1.02	0.1	0.0	0.1	-0.0	-0.0	-0.0

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RISULTATI : COMBINAZIONE 4 : SOLLECITAZIONI TRAVI

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ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
2	0.00	34.9	21.9	1.0	0.0	-4.0	-50.0
2	0.04	34.9	22.3	1.0	0.0	-4.0	-50.8
5	0.00	54.8	32.9	-0.5	-0.1	-2.0	-68.2
5	0.04	54.8	33.3	-0.5	-0.1	-2.1	-69.5
7	0.00	2.4	-1.3	1.4	-0.2	-0.9	-0.1
7	0.10	2.4	-0.9	1.4	-0.2	-0.7	0.0
8	0.00	2.4	-0.2	1.5	-0.2	-0.8	0.0
8	0.10	2.4	0.2	1.5	-0.2	-0.6	0.0
9	0.00	2.4	-0.2	1.5	-0.1	-0.6	0.0
9	0.10	2.4	0.2	1.5	-0.1	-0.5	0.0
10	0.00	2.4	-0.2	1.5	-0.1	-0.5	0.0
10	0.10	2.4	0.1	1.5	-0.1	-0.3	0.0
11	0.00	2.4	-0.2	1.5	-0.1	-0.3	0.0
11	0.10	2.4	0.2	1.5	-0.1	-0.2	0.0
12	0.00	2.4	-0.2	1.6	-0.0	-0.2	0.0
12	0.10	2.4	0.2	1.6	-0.0	-0.0	0.0
13	0.00	2.4	-0.1	1.6	0.0	-0.0	0.0
13	0.10	2.4	0.3	1.6	0.0	0.1	0.0
14	0.00	2.4	-0.1	1.6	0.1	0.1	0.0
14	0.10	2.4	0.3	1.6	0.1	0.3	-0.0
15	0.00	2.4	-0.2	1.7	0.1	0.3	-0.0
15	0.10	2.4	0.2	1.7	0.1	0.4	0.0
16	0.00	2.4	0.5	1.7	0.2	0.4	0.0
16	0.10	2.4	0.8	1.7	0.2	0.6	-0.1
17	0.00	-1.3	-7.5	-36.3	-3.3	4.9	-1.0
17	0.10	-1.3	-6.7	-30.3	-3.3	1.6	-0.3
18	0.00	-1.3	-6.6	-30.4	-3.3	1.6	-0.3
18	0.10	-1.3	-5.8	-24.4	-3.3	-1.1	0.3
19	0.00	-1.4	-4.6	-24.4	-3.3	-1.1	0.3
19	0.10	-1.4	-3.8	-18.4	-3.3	-3.3	0.7
20	0.00	-1.4	-2.6	-18.4	-3.3	-3.3	0.7
20	0.10	-1.4	-1.8	-12.4	-3.3	-4.8	1.0
21	0.00	-1.4	-0.6	-12.4	-3.3	-4.8	1.0
21	0.10	-1.4	0.1	-6.4	-3.3	-5.7	1.0
22	0.00	-1.4	1.3	-6.5	-3.3	-5.7	1.0
22	0.10	-1.4	2.1	-0.5	-3.3	-6.1	0.8
23	0.00	-1.4	3.2	-0.5	-3.3	-6.1	0.8
23	0.10	-1.4	4.0	5.5	-3.3	-5.8	0.5
24	0.00	-1.4	5.2	5.5	-3.3	-5.8	0.5
24	0.10	-1.4	6.0	11.5	-3.3	-5.0	-0.1
25	0.00	-1.3	7.3	11.4	-3.3	-5.0	-0.1
25	0.10	-1.3	8.1	17.4	-3.3	-3.5	-0.9
26	0.00	-1.3	8.6	17.4	-3.3	-3.5	-0.9
26	0.10	-1.3	9.4	23.4	-3.3	-1.5	-1.8
45	0.00	-1.1	7.9	23.4	-1.8	-1.4	-0.7
45	0.10	-1.1	8.6	29.4	-1.8	1.2	-1.6
46	0.00	-1.1	6.5	17.5	-1.8	-3.5	-0.0
46	0.10	-1.1	7.3	23.5	-1.8	-1.4	-0.7
47	0.00	-1.2	4.4	11.5	-1.8	-4.9	0.4
47	0.10	-1.2	5.2	17.5	-1.8	-3.5	-0.0
48	0.00	-1.2	2.4	5.6	-1.8	-5.8	0.7
48	0.10	-1.2	3.2	11.6	-1.8	-4.9	0.4
49	0.00	-1.2	0.5	-0.4	-1.8	-6.0	0.8
49	0.10	-1.2	1.3	5.6	-1.8	-5.8	0.7
50	0.00	-1.2	-1.5	-6.4	-1.7	-5.7	0.7
50	0.10	-1.2	-0.7	-0.4	-1.7	-6.0	0.8
51	0.00	-1.2	-3.4	-12.3	-1.7	-4.8	0.4
51	0.10	-1.2	-2.6	-6.3	-1.7	-5.7	0.7
52	0.00	-1.2	-5.4	-18.3	-1.7	-3.2	-0.1

52	0.10	-1.2	-4.6	-12.3	-1.7	-4.8	0.4
53	0.00	-1.1	-7.4	-24.2	-1.7	-1.1	-0.8
53	0.10	-1.1	-6.7	-18.2	-1.7	-3.2	-0.1
54	0.00	-1.1	-8.8	-30.2	-1.7	1.6	-1.6
54	0.10	-1.1	-8.0	-24.2	-1.7	-1.1	-0.8
55	0.00	1.7	0.4	0.9	0.2	0.2	0.0
55	0.10	1.7	0.8	0.9	0.2	0.3	-0.1
56	0.00	1.7	-0.2	0.9	0.2	0.1	-0.0
56	0.10	1.7	0.2	0.9	0.2	0.2	0.0
57	0.00	1.7	-0.1	0.8	0.1	0.0	0.0
57	0.10	1.7	0.3	0.8	0.1	0.1	-0.0
58	0.00	1.7	-0.1	0.8	0.0	-0.1	0.0
58	0.10	1.7	0.2	0.8	0.0	0.0	0.0
59	0.00	1.7	-0.2	0.7	0.0	-0.1	0.0
59	0.10	1.7	0.2	0.7	0.0	-0.1	0.0
60	0.00	1.7	-0.2	0.7	-0.0	-0.2	0.0
60	0.10	1.7	0.2	0.7	-0.0	-0.1	0.0
61	0.00	1.7	-0.3	0.7	-0.1	-0.3	-0.0
61	0.10	1.7	0.1	0.7	-0.1	-0.2	0.0
62	0.00	1.7	-0.3	0.6	-0.1	-0.3	-0.0
62	0.10	1.7	0.1	0.6	-0.1	-0.3	0.0
63	0.00	1.7	-0.2	0.6	-0.2	-0.4	0.0
63	0.10	1.7	0.2	0.6	-0.2	-0.3	-0.0
64	0.00	1.7	-0.8	0.5	-0.2	-0.4	-0.1
64	0.10	1.7	-0.4	0.5	-0.2	-0.4	0.0
66	0.00	60.3	32.0	-0.1	-0.0	-0.6	-75.3
66	0.04	60.3	32.4	-0.1	-0.0	-0.6	-76.6
69	0.00	60.3	32.0	0.1	0.0	0.6	-75.3
69	0.04	60.3	32.4	0.1	0.0	0.6	-76.6
71	0.00	1.6	-0.8	-0.2	-0.2	-0.1	-0.1
71	0.10	1.6	-0.4	-0.2	-0.2	-0.1	0.0
72	0.00	1.6	-0.2	-0.1	-0.2	-0.1	0.0
72	0.10	1.6	0.2	-0.1	-0.2	-0.1	-0.0
73	0.00	1.6	-0.3	-0.1	-0.1	-0.1	-0.0
73	0.10	1.6	0.1	-0.1	-0.1	-0.1	0.0
74	0.00	1.7	-0.3	-0.1	-0.1	-0.1	0.0
74	0.10	1.7	0.1	-0.1	-0.1	-0.1	0.0
75	0.00	1.7	-0.2	-0.0	-0.0	-0.1	0.0
75	0.10	1.7	0.2	-0.0	-0.0	-0.1	0.0
76	0.00	1.7	-0.2	0.0	0.0	-0.1	0.0
76	0.10	1.7	0.2	0.0	0.0	-0.1	0.0
77	0.00	1.7	-0.1	0.1	0.1	-0.1	0.0
77	0.10	1.7	0.3	0.1	0.1	-0.1	0.0
78	0.00	1.6	-0.1	0.1	0.1	-0.1	0.0
78	0.10	1.6	0.3	0.1	0.1	-0.1	-0.0
79	0.00	1.6	-0.2	0.1	0.2	-0.1	-0.0
79	0.10	1.6	0.2	0.1	0.2	-0.1	0.0
80	0.00	1.6	0.4	0.2	0.2	-0.1	0.0
80	0.10	1.6	0.8	0.2	0.2	-0.1	-0.1
81	0.00	-1.2	-8.7	-29.8	0.0	2.1	-1.6
81	0.10	-1.2	-7.9	-23.8	0.0	-0.6	-0.7
82	0.00	-1.2	-7.4	-23.9	0.0	-0.6	-0.7
82	0.10	-1.2	-6.6	-17.9	0.0	-2.6	-0.0
83	0.00	-1.2	-5.3	-17.9	0.0	-2.6	-0.0
83	0.10	-1.2	-4.5	-11.9	0.0	-4.1	0.4
84	0.00	-1.2	-3.3	-11.9	0.0	-4.1	0.4
84	0.10	-1.2	-2.5	-5.9	0.0	-5.0	0.7
85	0.00	-1.2	-1.4	-6.0	0.0	-5.0	0.7
85	0.10	-1.2	-0.6	0.0	0.0	-5.3	0.8
86	0.00	-1.2	0.6	-0.0	-0.0	-5.3	0.8
86	0.10	-1.2	1.4	6.0	-0.0	-5.0	0.7
87	0.00	-1.2	2.5	5.9	-0.0	-5.0	0.7
87	0.10	-1.2	3.3	11.9	-0.0	-4.1	0.4
88	0.00	-1.2	4.5	11.9	-0.0	-4.1	0.4
88	0.10	-1.2	5.3	17.9	-0.0	-2.6	-0.0
89	0.00	-1.2	6.6	17.9	-0.0	-2.6	-0.0
89	0.10	-1.2	7.4	23.9	-0.0	-0.6	-0.7
90	0.00	-1.2	7.9	23.8	-0.0	-0.6	-0.7
90	0.10	-1.2	8.7	29.8	-0.0	2.1	-1.6
109	0.00	-1.1	8.0	24.2	1.7	-1.1	-0.8
109	0.10	-1.1	8.8	30.2	1.7	1.6	-1.6
110	0.00	-1.1	6.7	18.2	1.7	-3.2	-0.1
110	0.10	-1.1	7.4	24.2	1.7	-1.1	-0.8
111	0.00	-1.2	4.6	12.3	1.7	-4.8	0.4
111	0.10	-1.2	5.4	18.3	1.7	-3.2	-0.1
112	0.00	-1.2	2.6	6.3	1.7	-5.7	0.7
112	0.10	-1.2	3.4	12.3	1.7	-4.8	0.4
113	0.00	-1.2	0.7	0.4	1.7	-6.0	0.8
113	0.10	-1.2	1.5	6.4	1.7	-5.7	0.7

114	0.00	-1.2	-1.3	-5.6	1.8	-5.8	0.7
114	0.10	-1.2	-0.5	0.4	1.8	-6.0	0.8
115	0.00	-1.2	-3.2	-11.6	1.8	-4.9	0.4
115	0.10	-1.2	-2.4	-5.6	1.8	-5.8	0.7
116	0.00	-1.2	-5.2	-17.5	1.8	-3.5	-0.0
116	0.10	-1.2	-4.4	-11.5	1.8	-4.9	0.4
117	0.00	-1.1	-7.3	-23.5	1.8	-1.4	-0.7
117	0.10	-1.1	-6.5	-17.5	1.8	-3.5	-0.0
118	0.00	-1.1	-8.6	-29.4	1.8	1.2	-1.6
118	0.10	-1.1	-7.9	-23.4	1.8	-1.4	-0.7
119	0.00	1.7	0.4	-0.5	0.2	-0.4	0.0
119	0.10	1.7	0.8	-0.5	0.2	-0.4	-0.1
120	0.00	1.7	-0.2	-0.6	0.2	-0.3	-0.0
120	0.10	1.7	0.2	-0.6	0.2	-0.4	0.0
121	0.00	1.7	-0.1	-0.6	0.1	-0.3	0.0
121	0.10	1.7	0.3	-0.6	0.1	-0.3	-0.0
122	0.00	1.7	-0.1	-0.7	0.1	-0.2	0.0
122	0.10	1.7	0.3	-0.7	0.1	-0.3	-0.0
123	0.00	1.7	-0.2	-0.7	0.0	-0.1	0.0
123	0.10	1.7	0.2	-0.7	0.0	-0.2	0.0
124	0.00	1.7	-0.2	-0.7	-0.0	-0.1	0.0
124	0.10	1.7	0.2	-0.7	-0.0	-0.1	0.0
125	0.00	1.7	-0.2	-0.8	-0.0	0.0	0.0
125	0.10	1.7	0.1	-0.8	-0.0	-0.1	0.0
126	0.00	1.7	-0.3	-0.8	-0.1	0.1	-0.0
126	0.10	1.7	0.1	-0.8	-0.1	0.0	0.0
127	0.00	1.7	-0.2	-0.9	-0.2	0.2	0.0
127	0.10	1.7	0.2	-0.9	-0.2	0.1	-0.0
128	0.00	1.7	-0.8	-0.9	-0.2	0.3	-0.1
128	0.10	1.7	-0.4	-0.9	-0.2	0.2	0.0
130	0.00	54.8	32.9	0.5	0.1	2.0	-68.2
130	0.04	54.8	33.3	0.5	0.1	2.1	-69.5
133	0.00	34.9	21.9	-1.0	-0.0	4.0	-50.0
133	0.04	34.9	22.3	-1.0	-0.0	4.0	-50.8
135	0.00	2.4	-0.8	-1.7	-0.2	0.6	-0.1
135	0.10	2.4	-0.5	-1.7	-0.2	0.4	0.0
136	0.00	2.4	-0.2	-1.7	-0.1	0.4	0.0
136	0.10	2.4	0.2	-1.7	-0.1	0.3	-0.0
137	0.00	2.4	-0.3	-1.6	-0.1	0.3	-0.0
137	0.10	2.4	0.1	-1.6	-0.1	0.1	0.0
138	0.00	2.4	-0.3	-1.6	-0.0	0.1	0.0
138	0.10	2.4	0.1	-1.6	-0.0	-0.0	0.0
139	0.00	2.4	-0.2	-1.6	0.0	-0.0	0.0
139	0.10	2.4	0.2	-1.6	0.0	-0.2	0.0
140	0.00	2.4	-0.2	-1.5	0.1	-0.2	0.0
140	0.10	2.4	0.2	-1.5	0.1	-0.3	0.0
141	0.00	2.4	-0.1	-1.5	0.1	-0.3	0.0
141	0.10	2.4	0.2	-1.5	0.1	-0.5	0.0
142	0.00	2.4	-0.2	-1.5	0.1	-0.5	0.0
142	0.10	2.4	0.2	-1.5	0.1	-0.6	0.0
143	0.00	2.4	-0.2	-1.5	0.2	-0.6	0.0
143	0.10	2.4	0.2	-1.5	0.2	-0.8	0.0
144	0.00	2.4	0.9	-1.4	0.2	-0.7	0.0
144	0.10	2.4	1.3	-1.4	0.2	-0.9	-0.1
145	0.00	-1.3	-9.4	-23.4	3.3	-1.5	-1.8
145	0.10	-1.3	-8.6	-17.4	3.3	-3.5	-0.9
146	0.00	-1.3	-8.1	-17.4	3.3	-3.5	-0.9
146	0.10	-1.3	-7.3	-11.4	3.3	-5.0	-0.1
147	0.00	-1.4	-6.0	-11.5	3.3	-5.0	-0.1
147	0.10	-1.4	-5.2	-5.5	3.3	-5.8	0.5
148	0.00	-1.4	-4.0	-5.5	3.3	-5.8	0.5
148	0.10	-1.4	-3.2	0.5	3.3	-6.1	0.8
149	0.00	-1.4	-2.1	0.5	3.3	-6.1	0.8
149	0.10	-1.4	-1.3	6.5	3.3	-5.7	1.0
150	0.00	-1.4	-0.1	6.4	3.3	-5.7	1.0
150	0.10	-1.4	0.6	12.4	3.3	-4.8	1.0
151	0.00	-1.4	1.8	12.4	3.3	-4.8	1.0
151	0.10	-1.4	2.6	18.4	3.3	-3.3	0.7
152	0.00	-1.4	3.8	18.4	3.3	-3.3	0.7
152	0.10	-1.4	4.6	24.4	3.3	-1.1	0.3
153	0.00	-1.3	5.8	24.4	3.3	-1.1	0.3
153	0.10	-1.3	6.6	30.4	3.3	1.6	-0.3
154	0.00	-1.3	6.7	30.3	3.3	1.6	-0.3
154	0.10	-1.3	7.5	36.3	3.3	4.9	-1.0

RISULTATI : COMBINAZIONE 4 : SOLLECITAZIONI PILASTRI

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)
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1	0.00	-21.9	1.0	34.9	4.0	-50.0	0.0
1	0.27	-19.1	1.0	34.9	4.0	-40.5	-0.3
3	0.00	-17.9	-1.3	36.3	4.9	-40.3	-0.4
3	1.02	-7.5	-1.3	36.3	4.9	-3.3	1.0
4	0.00	-28.6	0.2	53.6	3.1	-53.0	0.1
4	1.02	-18.2	0.2	53.6	3.1	1.6	-0.1
6	0.00	-32.9	-0.5	54.8	2.0	-68.2	-0.1
6	0.27	-30.2	-0.5	54.8	2.0	-53.4	0.1
27	0.00	-0.7	-0.0	0.0	0.0	-0.0	-0.0
27	1.02	0.1	-0.0	0.0	0.0	-0.0	0.0
28	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
28	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
29	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
29	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
30	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
30	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
31	0.00	0.4	0.0	0.0	0.0	-0.0	0.0
31	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0
32	0.00	0.4	0.0	0.0	0.0	-0.0	0.0
32	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0
33	0.00	0.4	0.0	0.0	0.0	-0.0	0.0
33	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0
34	0.00	0.5	0.0	0.0	0.0	-0.0	0.0
34	1.02	1.3	0.0	0.0	0.0	-0.0	-0.0
35	0.00	-0.3	0.0	0.1	0.0	-0.1	0.0
35	1.02	0.5	0.0	0.1	0.0	-0.0	-0.0
36	0.00	-0.2	0.0	0.1	0.0	-0.1	0.0
36	1.02	0.6	0.0	0.1	0.0	-0.0	-0.0
37	0.00	0.5	0.0	0.0	0.0	-0.1	0.0
37	1.02	1.3	0.0	0.0	0.0	-0.0	-0.0
38	0.00	0.4	0.0	0.0	0.0	-0.0	0.0
38	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0
39	0.00	0.4	0.0	0.0	0.0	-0.0	0.0
39	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0
40	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
40	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
41	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
41	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
42	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
42	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
43	0.00	0.5	-0.0	0.0	0.0	-0.1	-0.0
43	1.02	1.3	-0.0	0.0	0.0	-0.0	0.0
44	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0
44	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0
65	0.00	-32.0	-0.1	60.3	0.6	-75.3	-0.0
65	0.27	-29.3	-0.1	60.3	0.6	-59.0	0.0
67	0.00	-27.7	-0.0	59.2	0.9	-58.6	0.0
67	1.02	-17.3	-0.0	59.2	0.9	1.8	0.0
68	0.00	-27.7	0.0	59.2	-0.9	-58.6	-0.0
68	1.02	-17.3	0.0	59.2	-0.9	1.8	-0.0
70	0.00	-32.0	0.1	60.3	-0.6	-75.3	0.0
70	0.27	-29.3	0.1	60.3	-0.6	-59.0	-0.0
91	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0
91	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0
92	0.00	0.5	-0.0	0.0	0.0	-0.1	-0.0
92	1.02	1.3	-0.0	0.0	0.0	-0.0	0.0
93	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
93	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
94	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0
94	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0
95	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
95	1.02	1.2	0.0	0.0	-0.0	-0.0	0.0
96	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
96	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
97	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
97	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
98	0.00	0.5	0.0	0.0	-0.0	-0.1	0.0
98	1.02	1.3	0.0	0.0	-0.0	-0.0	-0.0
99	0.00	-0.2	0.0	0.1	-0.0	-0.1	0.0
99	1.02	0.6	0.0	0.1	-0.0	-0.0	-0.0
100	0.00	-0.2	0.0	0.1	-0.0	-0.1	0.0
100	1.02	0.6	0.0	0.1	-0.0	-0.0	-0.0
101	0.00	0.5	0.0	0.0	-0.0	-0.1	0.0
101	1.02	1.3	0.0	0.0	-0.0	-0.0	-0.0
102	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
102	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
103	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
103	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
104	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0

104	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
105	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0
105	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0
106	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0
106	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0
107	0.00	0.5	-0.0	0.0	-0.0	-0.1	-0.0
107	1.02	1.3	-0.0	0.0	-0.0	-0.0	0.0
108	0.00	-0.2	-0.0	0.1	-0.0	-0.1	-0.0
108	1.02	0.6	-0.0	0.1	-0.0	-0.0	0.0
129	0.00	-32.9	0.5	54.8	-2.0	-68.2	0.1
129	0.27	-30.2	0.5	54.8	-2.0	-53.4	-0.1
131	0.00	-28.6	-0.2	53.6	-3.1	-53.0	-0.1
131	1.02	-18.2	-0.2	53.6	-3.1	1.6	0.1
132	0.00	-17.9	1.3	36.3	-4.9	-40.3	0.4
132	1.02	-7.5	1.3	36.3	-4.9	-3.3	-1.0
134	0.00	-21.9	-1.0	34.9	-4.0	-50.0	-0.0
134	0.27	-19.1	-1.0	34.9	-4.0	-40.5	0.3
155	0.00	-0.3	-0.0	0.1	-0.0	-0.1	-0.0
155	1.02	0.5	-0.0	0.1	-0.0	-0.0	0.0
156	0.00	0.5	-0.0	0.0	-0.0	-0.0	-0.0
156	1.02	1.3	-0.0	0.0	-0.0	-0.0	0.0
157	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0
157	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0
158	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0
158	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0
159	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0
159	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0
160	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
160	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
161	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
161	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
162	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0
162	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0
163	0.00	-0.7	0.0	0.0	-0.0	-0.0	0.0
163	1.02	0.1	0.0	0.0	-0.0	-0.0	-0.0

DESCRIZIONE TABELLA SOLLECITAZIONI TRAVI E PILASTRI

Di seguito si riportano le spiegazioni delle sigle usate nella tabella SOLLECITAZIONI TRAVI E PILASTRI.
Per ogni gruppo di elementi ed internamente ad esso, per ogni elemento ad esso appartenente ed in ogni condizione di carico considerata vengono riportate, secondo modalita' diverse da tipo a tipo di elemento, azioni e/o tensioni in punti caratteristici riferiti alla terna locale.

ELEM. numero dell' elemento
n.ro
x ascissa locale misurata dal nodo I al nodo J
N sforzo normale nel p.to x
V2 forza di taglio ' ' ' in direz. 2 locale
V3 forza di taglio ' ' ' ' 3 '
T momento torcente ' ' '
M2 momento flettente ' ' ' intorno asse 2 locale
M3 momento flettente ' ' ' ' 3 '

Per la descrizione delle convenzioni usate per il segno delle azioni interne, si rimanda alla documentazione fornita con il programma.

RISULTATI : SOLLECITAZIONI TRAVI PER N.RO DI ELEMENTO

ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
2	0.00	0.0	21.8	0.7	-0.0	-0.0	-0.0	1	
2	0.04	0.0	22.2	0.7	-0.0	0.0	-0.9	1	
2	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
2	0.04	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
2	0.00	116.3	0.2	1.0	0.2	-13.4	-166.5	3	
2	0.04	116.3	0.2	1.0	0.2	-13.4	-166.5	3	
2	0.00	174.5	28.7	2.4	0.2	-20.1	-249.7		1
2	0.04	174.5	29.2	2.4	0.2	-20.0	-250.9		1
2	0.00	116.3	22.0	1.7	0.1	-13.4	-166.5		2
2	0.04	116.3	22.4	1.7	0.1	-13.3	-167.4		2
2	0.00	58.2	21.9	1.2	0.0	-6.7	-83.3		3
2	0.04	58.2	22.3	1.2	0.0	-6.7	-84.1		3
2	0.00	34.9	21.9	1.0	0.0	-4.0	-50.0		4
2	0.04	34.9	22.3	1.0	0.0	-4.0	-50.8		4
5	0.00	-0.0	33.0	-0.6	-0.1	-0.0	0.0	1	
5	0.04	-0.0	33.4	-0.6	-0.1	-0.0	-1.3	1	
5	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
5	0.04	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
5	0.00	182.6	-0.2	0.4	0.1	-6.8	-227.4	3	
5	0.04	182.6	-0.2	0.4	0.1	-6.8	-227.4	3	
5	0.00	273.8	42.6	-0.2	-0.0	-10.2	-341.1		1
5	0.04	273.8	43.2	-0.2	-0.0	-10.2	-342.8		1
5	0.00	182.6	32.8	-0.2	-0.0	-6.8	-227.4		2
5	0.04	182.6	33.2	-0.2	-0.0	-6.8	-228.7		2
5	0.00	91.3	32.9	-0.4	-0.0	-3.4	-113.7		3
5	0.04	91.3	33.3	-0.4	-0.0	-3.4	-115.0		3
5	0.00	54.8	32.9	-0.5	-0.1	-2.0	-68.2		4
5	0.04	54.8	33.3	-0.5	-0.1	-2.1	-69.5		4
7	0.00	2.0	-1.3	-0.0	-0.0	0.0	-0.1	1	
7	0.10	2.0	-0.9	-0.0	-0.0	0.0	0.0	1	
7	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
7	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
7	0.00	1.1	-0.0	4.7	-0.7	-3.0	-0.0	3	
7	0.10	1.1	-0.0	4.7	-0.7	-2.5	-0.0	3	
7	0.00	4.3	-1.6	7.1	-1.1	-4.4	-0.1		1
7	0.10	4.3	-1.1	7.1	-1.1	-3.7	0.0		1
7	0.00	3.2	-1.3	4.7	-0.7	-3.0	-0.1		2

135	0.10	2.4	-0.5	-1.7	-0.2	0.4	0.0		4
136	0.00	2.0	-0.2	0.0	0.0	-0.0	0.0	1	
136	0.10	2.0	0.2	0.0	0.0	-0.0	-0.0	1	
136	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
136	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
136	0.00	1.1	0.0	-5.5	-0.3	1.5	0.0	3	
136	0.10	1.1	0.0	-5.5	-0.3	0.9	0.0	3	
136	0.00	4.4	-0.2	-8.3	-0.5	2.2	0.0		1
136	0.10	4.4	0.3	-8.3	-0.5	1.4	-0.0		1
136	0.00	3.2	-0.2	-5.5	-0.3	1.5	0.0	2	
136	0.10	3.2	0.2	-5.5	-0.3	0.9	-0.0	2	
136	0.00	2.6	-0.2	-2.8	-0.2	0.7	0.0	3	
136	0.10	2.6	0.2	-2.8	-0.2	0.5	-0.0	3	
136	0.00	2.4	-0.2	-1.7	-0.1	0.4	0.0	4	
136	0.10	2.4	0.2	-1.7	-0.1	0.3	-0.0	4	
137	0.00	2.0	-0.3	0.0	0.0	-0.0	-0.0	1	
137	0.10	2.0	0.1	0.0	0.0	-0.0	0.0	1	
137	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
137	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
137	0.00	1.1	0.0	-5.4	-0.2	0.9	0.0	3	
137	0.10	1.1	0.0	-5.4	-0.2	0.4	0.0	3	
137	0.00	4.4	-0.3	-8.1	-0.3	1.4	-0.0		1
137	0.10	4.4	0.2	-8.1	-0.3	0.6	0.0		1
137	0.00	3.2	-0.3	-5.4	-0.2	0.9	-0.0	2	
137	0.10	3.2	0.1	-5.4	-0.2	0.4	0.0	2	
137	0.00	2.6	-0.3	-2.7	-0.1	0.5	-0.0	3	
137	0.10	2.6	0.1	-2.7	-0.1	0.2	0.0	3	
137	0.00	2.4	-0.3	-1.6	-0.1	0.3	-0.0	4	
137	0.10	2.4	0.1	-1.6	-0.1	0.1	0.0	4	
138	0.00	2.0	-0.3	0.0	0.0	-0.0	0.0	1	
138	0.10	2.0	0.1	0.0	0.0	-0.0	0.0	1	
138	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
138	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
138	0.00	1.1	0.0	-5.3	-0.0	0.4	0.0	3	
138	0.10	1.1	0.0	-5.3	-0.0	-0.1	-0.0	3	
138	0.00	4.4	-0.3	-7.9	-0.0	0.6	0.0		1
138	0.10	4.4	0.2	-7.9	-0.0	-0.2	0.0		1
138	0.00	3.2	-0.3	-5.3	-0.0	0.4	0.0	2	
138	0.10	3.2	0.1	-5.3	-0.0	-0.1	0.0	2	
138	0.00	2.6	-0.3	-2.6	-0.0	0.2	0.0	3	
138	0.10	2.6	0.1	-2.6	-0.0	-0.1	0.0	3	
138	0.00	2.4	-0.3	-1.6	-0.0	0.1	0.0	4	
138	0.10	2.4	0.1	-1.6	-0.0	-0.0	0.0	4	
139	0.00	2.1	-0.2	0.0	0.0	-0.0	0.0	1	
139	0.10	2.1	0.2	0.0	0.0	0.0	0.0	1	
139	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
139	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
139	0.00	1.1	0.0	-5.2	0.1	-0.1	0.0	3	
139	0.10	1.1	0.0	-5.2	0.1	-0.6	-0.0	3	
139	0.00	4.4	-0.3	-7.8	0.2	-0.1	0.0		1
139	0.10	4.4	0.2	-7.8	0.2	-0.9	0.0		1
139	0.00	3.2	-0.2	-5.2	0.1	-0.1	0.0	2	
139	0.10	3.2	0.2	-5.2	0.1	-0.6	0.0	2	
139	0.00	2.6	-0.2	-2.6	0.1	-0.0	0.0	3	
139	0.10	2.6	0.2	-2.6	0.1	-0.3	0.0	3	
139	0.00	2.4	-0.2	-1.6	0.0	-0.0	0.0	4	
139	0.10	2.4	0.2	-1.6	0.0	-0.2	0.0	4	
140	0.00	2.1	-0.2	0.0	0.0	0.0	0.0	1	
140	0.10	2.1	0.2	0.0	0.0	0.0	0.0	1	
140	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
140	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
140	0.00	1.1	0.0	-5.1	0.2	-0.6	0.0	3	
140	0.10	1.1	0.0	-5.1	0.2	-1.1	-0.0	3	
140	0.00	4.4	-0.2	-7.7	0.3	-0.9	0.0		1
140	0.10	4.4	0.3	-7.7	0.3	-1.6	0.0		1
140	0.00	3.2	-0.2	-5.1	0.2	-0.6	0.0	2	
140	0.10	3.2	0.2	-5.1	0.2	-1.1	0.0	2	
140	0.00	2.6	-0.2	-2.5	0.1	-0.3	0.0	3	
140	0.10	2.6	0.2	-2.5	0.1	-0.5	0.0	3	
140	0.00	2.4	-0.2	-1.5	0.1	-0.2	0.0	4	
140	0.10	2.4	0.2	-1.5	0.1	-0.3	0.0	4	
141	0.00	2.1	-0.2	0.0	0.0	0.0	0.0	1	
141	0.10	2.1	0.2	0.0	0.0	0.0	0.0	1	
141	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
141	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
141	0.00	1.1	0.0	-5.0	0.3	-1.1	-0.0	3	
141	0.10	1.1	0.0	-5.0	0.3	-1.6	-0.0	3	
141	0.00	4.4	-0.2	-7.5	0.5	-1.6	0.0		1
141	0.10	4.4	0.3	-7.5	0.5	-2.4	0.0		1
141	0.00	3.2	-0.1	-5.0	0.3	-1.1	0.0	2	
141	0.10	3.2	0.2	-5.0	0.3	-1.6	0.0	2	
141	0.00	2.6	-0.1	-2.5	0.2	-0.5	0.0	3	
141	0.10	2.6	0.2	-2.5	0.2	-0.8	0.0	3	
141	0.00	2.4	-0.1	-1.5	0.1	-0.3	0.0	4	
141	0.10	2.4	0.2	-1.5	0.1	-0.5	0.0	4	
142	0.00	2.0	-0.2	0.0	0.0	0.0	0.0	1	
142	0.10	2.0	0.2	0.0	0.0	0.0	0.0	1	
142	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
142	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
142	0.00	1.1	0.0	-4.9	0.5	-1.6	-0.0	3	
142	0.10	1.1	0.0	-4.9	0.5	-2.0	-0.0	3	
142	0.00	4.4	-0.2	-7.4	0.7	-2.3	0.0		1
142	0.10	4.4	0.3	-7.4	0.7	-3.1	0.0		1
142	0.00	3.2	-0.2	-4.9	0.5	-1.6	0.0	2	
142	0.10	3.2	0.2	-4.9	0.5	-2.0	0.0	2	
142	0.00	2.6	-0.2	-2.5	0.2	-0.8	0.0	3	
142	0.10	2.6	0.2	-2.5	0.2	-1.0	0.0	3	
142	0.00	2.4	-0.2	-1.5	0.1	-0.5	0.0	4	
142	0.10	2.4	0.2	-1.5	0.1	-0.6	0.0	4	
143	0.00	2.0	-0.2	0.0	0.0	0.0	0.0	1	
143	0.10	2.0	0.2	0.0	0.0	0.0	0.0	1	
143	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
143	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
143	0.00	1.1	0.0	-4.8	0.6	-2.0	-0.0	3	
143	0.10	1.1	0.0	-4.8	0.6	-2.5	-0.0	3	
143	0.00	4.4	-0.3	-7.3	0.9	-3.0	0.0		1
143	0.10	4.4	0.2	-7.3	0.9	-3.8	0.0		1
143	0.00	3.2	-0.2	-4.8	0.6	-2.0	0.0	2	
143	0.10	3.2	0.2	-4.8	0.6	-2.5	0.0	2	
143	0.00	2.6	-0.2	-2.4	0.3	-1.0	0.0	3	
143	0.10	2.6	0.2	-2.4	0.3	-1.3	0.0	3	
143	0.00	2.4	-0.2	-1.5	0.2	-0.6	0.0	4	
143	0.10	2.4	0.2	-1.5	0.2	-0.8	0.0	4	
144	0.00	2.0	0.9	0.0	0.0	0.0	0.0	1	
144	0.10	2.0	1.3	0.0	0.0	0.0	-0.1	1	
144	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
144	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
144	0.00	1.1	0.0	-4.7	0.7	-2.5	-0.0	3	

144	0.10	1.1	0.0	-4.7	0.7	-3.0	-0.0	3	
144	0.00	4.3	1.1	-7.1	1.1	-3.7	0.0		1
144	0.10	4.3	1.6	-7.1	1.1	-4.4	-0.1		1
144	0.00	3.2	0.9	-4.7	0.7	-2.5	0.0		2
144	0.10	3.2	1.3	-4.7	0.7	-3.0	-0.1		2
144	0.00	2.6	0.9	-2.4	0.4	-1.2	0.0		3
144	0.10	2.6	1.3	-2.4	0.4	-1.5	-0.1		3
144	0.00	2.4	0.9	-1.4	0.2	-0.7	0.0		4
144	0.10	2.4	1.3	-1.4	0.2	-0.9	-0.1		4
145	0.00	-1.3	-9.4	0.0	0.0	-0.0	-1.8	1	
145	0.10	-1.3	-8.6	0.0	0.0	-0.0	-0.9	1	
145	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
145	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
145	0.00	-0.2	0.1	-78.0	11.1	-4.9	0.1	3	
145	0.10	-0.2	0.1	-58.0	11.1	-11.7	0.1	3	
145	0.00	-2.0	-12.0	-116.9	16.7	-7.4	-2.2		1
145	0.10	-2.0	-11.0	-86.9	16.7	-17.6	-1.0		1
145	0.00	-1.5	-9.3	-78.0	11.1	-4.9	-1.7		2
145	0.10	-1.5	-8.5	-58.0	11.1	-11.7	-0.8		2
145	0.00	-1.4	-9.3	-39.0	5.6	-2.5	-1.7		3
145	0.10	-1.4	-8.6	-29.0	5.6	-5.9	-0.9		3
145	0.00	-1.3	-9.4	-23.4	3.3	-1.5	-1.8		4
145	0.10	-1.3	-8.6	-17.4	3.3	-3.5	-0.9		4
146	0.00	-1.3	-8.1	0.0	0.0	-0.0	-0.9	1	
146	0.10	-1.3	-7.3	0.0	0.0	-0.0	-0.1	1	
146	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
146	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
146	0.00	-0.2	0.2	-58.1	11.1	-11.8	0.1	3	
146	0.10	-0.2	0.2	-38.1	11.1	-16.6	0.1	3	
146	0.00	-2.0	-10.3	-87.2	16.7	-17.6	-1.1		1
146	0.10	-2.0	-9.3	-57.2	16.7	-24.9	-0.1		1
146	0.00	-1.5	-7.9	-58.1	11.1	-11.8	-0.8		2
146	0.10	-1.5	-7.2	-38.1	11.1	-16.6	-0.1		2
146	0.00	-1.4	-8.0	-29.1	5.6	-5.9	-0.9		3
146	0.10	-1.4	-7.3	-19.1	5.6	-8.3	-0.1		3
146	0.00	-1.3	-8.1	-17.4	3.3	-3.5	-0.9		4
146	0.10	-1.3	-7.3	-11.4	3.3	-5.0	-0.1		4
147	0.00	-1.3	-6.1	0.0	0.0	-0.0	-0.1	1	
147	0.10	-1.3	-5.3	0.0	0.0	-0.0	0.4	1	
147	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
147	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
147	0.00	-0.2	0.2	-38.3	11.1	-16.6	0.1	3	
147	0.10	-0.2	0.2	-18.3	11.1	-19.4	0.0	3	
147	0.00	-2.0	-7.6	-57.4	16.7	-24.9	-0.1		1
147	0.10	-2.0	-6.6	-27.4	16.7	-29.1	0.6		1
147	0.00	-1.5	-5.9	-38.3	11.1	-16.6	-0.1		2
147	0.10	-1.5	-5.1	-18.3	11.1	-19.4	0.5		2
147	0.00	-1.4	-6.0	-19.1	5.6	-8.3	-0.1		3
147	0.10	-1.4	-5.2	-9.1	5.6	-9.7	0.5		3
147	0.00	-1.4	-6.0	-11.5	3.3	-5.0	-0.1		4
147	0.10	-1.4	-5.2	-5.5	3.3	-5.8	0.5		4
148	0.00	-1.3	-4.1	0.0	0.0	-0.0	0.4	1	
148	0.10	-1.3	-3.3	0.0	0.0	-0.0	0.8	1	
148	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
148	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
148	0.00	-0.2	0.2	-18.4	11.1	-19.4	0.0	3	
148	0.10	-0.2	0.2	1.6	11.1	-20.3	0.0	3	
148	0.00	-2.0	-5.0	-27.6	16.6	-29.1	0.6		1
148	0.10	-2.0	-4.0	2.4	16.6	-30.4	1.1		1
148	0.00	-1.5	-3.9	-18.4	11.1	-19.4	0.5		2
148	0.10	-1.5	-3.1	1.6	11.1	-20.3	0.8		2
148	0.00	-1.4	-4.0	-9.2	5.5	-9.7	0.5		3
148	0.10	-1.4	-3.2	0.8	5.5	-10.1	0.8		3
148	0.00	-1.4	-4.0	-5.5	3.3	-5.8	0.5		4
148	0.10	-1.4	-3.2	0.5	3.3	-6.1	0.8		4
149	0.00	-1.3	-2.1	0.0	0.0	-0.0	0.8	1	
149	0.10	-1.3	-1.4	0.0	0.0	-0.0	1.0	1	
149	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
149	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
149	0.00	-0.2	0.2	1.5	11.0	-20.3	0.0	3	
149	0.10	-0.2	0.2	21.5	11.0	-19.1	-0.0	3	
149	0.00	-2.0	-2.5	2.3	16.6	-30.4	1.1		1
149	0.10	-2.0	-1.5	32.3	16.6	-28.7	1.3		1
149	0.00	-1.5	-2.0	1.5	11.0	-20.3	0.8		2
149	0.10	-1.5	-1.2	21.5	11.0	-19.1	1.0		2
149	0.00	-1.4	-2.0	0.8	5.5	-10.1	0.8		3
149	0.10	-1.4	-1.3	10.8	5.5	-9.6	1.0		3
149	0.00	-1.4	-2.1	0.5	3.3	-6.1	0.8		4
149	0.10	-1.4	-1.3	6.5	3.3	-5.7	1.0		4
150	0.00	-1.3	-0.2	0.0	0.0	-0.0	1.0	1	
150	0.10	-1.3	0.6	0.0	0.0	-0.0	1.0	1	
150	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
150	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
150	0.00	-0.2	0.2	21.4	11.0	-19.2	-0.0	3	
150	0.10	-0.2	0.2	41.4	11.0	-16.0	-0.0	3	
150	0.00	-2.0	0.0	32.1	16.5	-28.7	1.3		1
150	0.10	-2.0	1.0	62.1	16.5	-24.0	1.2		1
150	0.00	-1.5	-0.0	21.4	11.0	-19.2	1.0		2
150	0.10	-1.5	0.8	41.4	11.0	-16.0	0.9		2
150	0.00	-1.4	-0.1	10.7	5.5	-9.6	1.0		3
150	0.10	-1.4	0.7	20.7	5.5	-8.0	1.0		3
150	0.00	-1.4	-0.1	6.4	3.3	-5.7	1.0		4
150	0.10	-1.4	0.6	12.4	3.3	-4.8	1.0		4
151	0.00	-1.3	1.7	0.0	0.0	-0.0	1.0	1	
151	0.10	-1.3	2.5	0.0	0.0	0.0	0.8	1	
151	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
151	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
151	0.00	-0.2	0.2	41.3	11.0	-16.0	-0.0	3	
151	0.10	-0.2	0.2	61.3	11.0	-10.9	-0.0	3	
151	0.00	-2.0	2.5	62.0	16.5	-24.1	1.2		1
151	0.10	-2.0	3.6	92.0	16.5	-16.4	0.9		1
151	0.00	-1.5	1.9	41.3	11.0	-16.0	0.9		2
151	0.10	-1.5	2.7	61.3	11.0	-10.9	0.7		2
151	0.00	-1.4	1.8	20.7	5.5	-8.0	1.0		3
151	0.10	-1.4	2.6	30.7	5.5	-5.5	0.7		3
151	0.00	-1.4	1.8	12.4	3.3	-4.8	1.0		4
151	0.10	-1.4	2.6	18.4	3.3	-3.3	0.7		4
152	0.00	-1.3	3.7	0.0	0.0	0.0	0.8	1	
152	0.10	-1.3	4.5	0.0	0.0	0.0	0.3	1	
152	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
152	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
152	0.00	-0.2	0.2	61.3	10.9	-10.9	-0.0	3	
152	0.10	-0.2	0.2	81.3	10.9	-3.8	-0.1	3	
152	0.00	-2.0	5.1	91.9	16.4	-16.4	0.9		1
152	0.10	-2.0	6.1	121.9	16.4	-5.7	0.4		1
152	0.00	-1.5	3.9	61.3	10.9	-10.9	0.7		2
152	0.10	-1.5	4.7	81.3	10.9	-3.8	0.3		2
152	0.00	-1.4	3.8	30.6	5.5	-5.5	0.7		3

152	0.10	-1.4	4.6	40.6	5.5	-1.9	0.3	3
152	0.00	-1.4	3.8	18.4	3.3	-3.3	0.7	4
152	0.10	-1.4	4.6	24.4	3.3	-1.1	0.3	4
153	0.00	-1.3	5.8	0.0	0.0	0.0	0.3	1
153	0.10	-1.3	6.5	0.0	0.0	0.0	-0.3	1
153	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
153	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
153	0.00	-0.2	0.2	81.2	10.9	-3.8	-0.1	3
153	0.10	-0.2	0.2	101.2	10.9	5.3	-0.1	3
153	0.00	-2.0	7.8	121.8	16.3	-5.7	0.4	1
153	0.10	-2.0	8.8	151.8	16.3	7.9	-0.5	1
153	0.00	-1.5	5.9	81.2	10.9	-3.8	0.3	2
153	0.10	-1.5	6.7	101.2	10.9	5.3	-0.3	2
153	0.00	-1.4	5.9	40.6	5.4	-1.9	0.3	3
153	0.10	-1.4	6.6	50.6	5.4	2.6	-0.3	3
153	0.00	-1.3	5.8	24.4	3.3	-1.1	0.3	4
153	0.10	-1.3	6.6	30.4	3.3	1.6	-0.3	4
154	0.00	-1.3	6.7	0.0	0.0	0.0	-0.3	1
154	0.10	-1.3	7.4	0.0	0.0	0.0	-1.0	1
154	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
154	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
154	0.00	-0.2	0.2	101.1	10.9	5.3	-0.1	3
154	0.10	-0.2	0.2	121.1	10.9	16.4	-0.1	3
154	0.00	-1.9	8.9	151.6	16.3	7.9	-0.5	1
154	0.10	-1.9	9.9	181.6	16.3	24.6	-1.4	1
154	0.00	-1.5	6.8	101.1	10.9	5.3	-0.3	2
154	0.10	-1.5	7.6	121.1	10.9	16.4	-1.1	2
154	0.00	-1.4	6.7	50.5	5.4	2.6	-0.3	3
154	0.10	-1.4	7.5	60.5	5.4	8.2	-1.0	3
154	0.00	-1.3	6.7	30.3	3.3	1.6	-0.3	4
154	0.10	-1.3	7.5	36.3	3.3	4.9	-1.0	4

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RISULTATI : SOLLECITAZIONI PILASTRI PER N.RO DI ELEMENTO

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ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
1	0.00	-21.8	0.7	0.0	0.0	-0.0	-0.0	1	
1	0.27	-19.1	0.7	0.0	0.0	-0.0	-0.2	1	
1	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
1	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
1	0.00	-0.2	1.0	116.3	13.4	-166.5	0.2	3	
1	0.27	-0.2	1.0	116.3	13.4	-135.1	-0.1	3	
1	0.00	-28.7	2.4	174.5	20.1	-249.7	0.2		1
1	0.27	-25.1	2.4	174.5	20.1	-202.6	-0.5		1
1	0.00	-22.0	1.7	116.3	13.4	-166.5	0.1		2
1	0.27	-19.3	1.7	116.3	13.4	-135.1	-0.3		2
1	0.00	-21.9	1.2	58.2	6.7	-83.3	0.0		3
1	0.27	-19.2	1.2	58.2	6.7	-67.5	-0.3		3
1	0.00	-21.9	1.0	34.9	4.0	-50.0	0.0		4
1	0.27	-19.1	1.0	34.9	4.0	-40.5	-0.3		4
3	0.00	-17.8	-1.3	0.0	0.0	-0.0	-0.3	1	
3	1.02	-7.4	-1.3	0.0	0.0	-0.0	1.0	1	
3	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
3	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
3	0.00	-0.2	-0.2	121.1	16.4	-134.3	-0.1	3	
3	1.02	-0.2	-0.2	121.1	16.4	-10.9	0.1	3	
3	0.00	-23.4	-1.9	181.6	24.6	-201.5	-0.6		1
3	1.02	-9.9	-1.9	181.6	24.6	-16.3	1.4		1
3	0.00	-18.0	-1.5	121.1	16.4	-134.3	-0.4		2
3	1.02	-7.6	-1.5	121.1	16.4	-10.9	1.1		2
3	0.00	-17.9	-1.4	60.5	8.2	-67.2	-0.4		3
3	1.02	-7.5	-1.4	60.5	8.2	-5.4	1.0		3
3	0.00	-17.9	-1.3	36.3	4.9	-40.3	-0.4		4
3	1.02	-7.5	-1.3	36.3	4.9	-3.3	1.0		4
4	0.00	-28.6	0.2	-0.0	0.0	0.0	0.1	1	
4	1.02	-18.2	0.2	-0.0	0.0	-0.0	-0.1	1	
4	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
4	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
4	0.00	0.1	-0.1	178.6	10.3	-176.8	-0.1	3	
4	1.02	0.1	-0.1	178.6	10.3	5.4	0.1	3	
4	0.00	-37.0	0.1	267.9	15.4	-265.2	0.0		1
4	1.02	-23.5	0.1	267.9	15.4	8.1	-0.1		1
4	0.00	-28.5	0.1	178.6	10.3	-176.8	0.0		2
4	1.02	-18.1	0.1	178.6	10.3	5.4	-0.1		2
4	0.00	-28.6	0.2	89.3	5.1	-88.4	0.1		3
4	1.02	-18.2	0.2	89.3	5.1	2.7	-0.1		3
4	0.00	-28.6	0.2	53.6	3.1	-53.0	0.1		4
4	1.02	-18.2	0.2	53.6	3.1	1.6	-0.1		4
6	0.00	-33.0	-0.6	-0.0	0.0	0.0	-0.1	1	
6	0.27	-30.2	-0.6	-0.0	0.0	0.0	0.1	1	
6	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
6	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
6	0.00	0.2	0.4	182.6	6.8	-227.4	0.1	3	
6	0.27	0.2	0.4	182.6	6.8	-178.1	-0.0	3	
6	0.00	-42.6	-0.2	273.8	10.2	-341.1	-0.0		1
6	0.27	-39.1	-0.2	273.8	10.2	-267.2	0.0		1
6	0.00	-32.8	-0.2	182.6	6.8	-227.4	-0.0		2
6	0.27	-30.1	-0.2	182.6	6.8	-178.1	0.0		2
6	0.00	-32.9	-0.4	91.3	3.4	-113.7	-0.0		3
6	0.27	-30.1	-0.4	91.3	3.4	-89.0	0.1		3
6	0.00	-32.9	-0.5	54.8	2.0	-68.2	-0.1		4
6	0.27	-30.2	-0.5	54.8	2.0	-53.4	0.1		4
27	0.00	-0.7	-0.0	0.0	0.0	-0.0	-0.0	1	
27	1.02	0.1	-0.0	0.0	0.0	-0.0	0.0	1	
27	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
27	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
27	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
27	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
27	0.00	-0.9	-0.0	0.2	0.0	-0.2	-0.0		1
27	1.02	0.1	-0.0	0.2	0.0	-0.0	0.0		1
27	0.00	-0.7	-0.0	0.1	0.0	-0.1	-0.0		2
27	1.02	0.1	-0.0	0.1	0.0	-0.0	0.0		2
27	0.00	-0.7	-0.0	0.1	0.0	-0.1	-0.0		3
27	1.02	0.1	-0.0	0.1	0.0	-0.0	0.0		3
27	0.00	-0.7	-0.0	0.0	0.0	-0.0	-0.0		4
27	1.02	0.1	-0.0	0.0	0.0	-0.0	0.0		4
28	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	1	
28	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1	
28	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
28	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
28	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
28	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3	
28	0.00	0.6	-0.0	0.1	0.0	-0.2	-0.0		1
28	1.02	1.6	-0.0	0.1	0.0	-0.1	0.0		1
28	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		2
28	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		2
28	0.00	0.4	-0.0	0.0	0.0	-0.1	-0.0		3

28	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	3
28	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	4
28	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	4
29	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	1
29	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1
29	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
29	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
29	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0	3
29	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3
29	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0	1
29	1.02	1.6	-0.0	0.1	0.0	-0.1	0.0	1
29	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0	2
29	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	2
29	0.00	0.4	-0.0	0.0	0.0	-0.1	-0.0	3
29	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	3
29	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	4
29	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	4
30	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	1
30	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1
30	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
30	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
30	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0	3
30	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3
30	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0	1
30	1.02	1.5	-0.0	0.1	0.0	-0.1	0.0	1
30	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0	2
30	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	2
30	0.00	0.4	-0.0	0.0	0.0	-0.1	-0.0	3
30	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	3
30	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	4
30	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	4
31	0.00	0.4	0.0	0.0	0.0	-0.0	0.0	1
31	1.02	1.2	0.0	0.0	0.0	0.0	-0.0	1
31	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
31	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
31	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0	3
31	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3
31	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0	1
31	1.02	1.5	-0.0	0.1	0.0	-0.1	0.0	1
31	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0	2
31	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	2
31	0.00	0.4	0.0	0.0	0.0	-0.1	0.0	3
31	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0	3
31	0.00	0.4	0.0	0.0	0.0	-0.0	0.0	4
31	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0	4
32	0.00	0.4	0.0	-0.0	0.0	0.0	0.0	1
32	1.02	1.2	0.0	-0.0	0.0	0.0	-0.0	1
32	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
32	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
32	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0	3
32	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3
32	0.00	0.5	0.0	0.1	0.0	-0.2	0.0	1
32	1.02	1.5	0.0	0.1	0.0	-0.0	-0.0	1
32	0.00	0.4	0.0	0.1	0.0	-0.1	0.0	2
32	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0	2
32	0.00	0.4	0.0	0.0	0.0	-0.1	0.0	3
32	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0	3
32	0.00	0.4	0.0	0.0	0.0	-0.0	0.0	4
32	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0	4
33	0.00	0.4	0.0	-0.0	0.0	0.0	0.0	1
33	1.02	1.2	0.0	-0.0	0.0	0.0	-0.0	1
33	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
33	1.02	-0.0	-0.0	0.1	0.0	-0.1	-0.0	3
33	0.00	-0.0	-0.0	0.1	0.0	-0.0	0.0	3
33	0.00	0.5	0.0	0.2	0.0	-0.2	0.0	1
33	1.02	1.6	0.0	0.2	0.0	-0.0	-0.0	1
33	0.00	0.4	0.0	0.1	0.0	-0.1	0.0	2
33	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0	2
33	0.00	0.4	0.0	0.1	0.0	-0.1	0.0	3
33	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0	3
33	0.00	0.4	0.0	0.0	0.0	-0.0	0.0	4
33	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0	4
34	0.00	0.5	0.0	-0.0	0.0	0.0	0.0	1
34	1.02	1.3	0.0	-0.0	0.0	-0.0	-0.0	1
34	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
34	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
34	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0	3
34	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3
34	0.00	0.6	0.0	0.2	0.0	-0.2	0.0	1
34	1.02	1.7	0.0	0.2	0.0	-0.0	-0.0	1
34	0.00	0.5	0.0	0.1	0.0	-0.2	0.0	2
34	1.02	1.3	0.0	0.1	0.0	-0.0	-0.0	2
34	0.00	0.5	0.0	0.1	0.0	-0.1	0.0	3
34	1.02	1.3	0.0	0.1	0.0	-0.0	-0.0	3
34	0.00	0.5	0.0	0.0	0.0	-0.0	0.0	4
34	1.02	1.3	0.0	0.0	0.0	-0.0	-0.0	4
35	0.00	-0.3	0.0	-0.0	0.0	0.0	0.0	1
35	1.02	0.5	0.0	-0.0	0.0	-0.0	-0.0	1
35	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
35	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
35	0.00	0.0	-0.0	0.2	0.0	-0.2	-0.0	3
35	1.02	0.0	-0.0	0.2	0.0	-0.0	0.0	3
35	0.00	-0.3	0.0	0.3	0.0	-0.3	0.0	1
35	1.02	0.7	0.0	0.3	0.0	-0.0	-0.0	1
35	0.00	-0.3	0.0	0.2	0.0	-0.2	0.0	2
35	1.02	0.5	0.0	0.2	0.0	-0.0	-0.0	2
35	0.00	-0.3	0.0	0.1	0.0	-0.1	0.0	3
35	1.02	0.5	0.0	0.1	0.0	-0.0	-0.0	3
35	0.00	-0.3	0.0	0.1	0.0	-0.1	0.0	4
35	1.02	0.5	0.0	0.1	0.0	-0.0	-0.0	4
36	0.00	-0.2	0.0	0.0	0.0	0.0	0.0	1
36	1.02	0.6	0.0	0.0	0.0	0.0	-0.0	1
36	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
36	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
36	0.00	0.0	-0.0	0.2	0.0	-0.2	-0.0	3
36	1.02	0.0	-0.0	0.2	0.0	-0.0	0.0	3
36	0.00	-0.3	0.0	0.3	0.0	-0.3	0.0	1
36	1.02	0.8	0.0	0.3	0.0	-0.0	-0.0	1
36	0.00	-0.2	0.0	0.2	0.0	-0.2	0.0	2
36	1.02	0.6	0.0	0.2	0.0	-0.0	-0.0	2
36	0.00	-0.2	0.0	0.1	0.0	-0.1	0.0	3
36	1.02	0.6	0.0	0.1	0.0	-0.0	-0.0	3
36	0.00	-0.2	0.0	0.1	0.0	-0.1	0.0	4
36	1.02	0.6	0.0	0.1	0.0	-0.0	-0.0	4
37	0.00	0.5	0.0	0.0	0.0	0.0	0.0	1
37	1.02	1.3	0.0	0.0	0.0	0.0	-0.0	1
37	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2

37	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
37	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0	3
37	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0	3
37	0.00	0.6	0.0	0.2	0.0	-0.3	0.0	1
37	1.02	1.7	0.0	0.2	0.0	-0.0	-0.0	1
37	0.00	0.5	0.0	0.2	0.0	-0.2	0.0	2
37	1.02	1.3	0.0	0.2	0.0	-0.0	-0.0	2
37	0.00	0.5	0.0	0.1	0.0	-0.1	0.0	3
37	1.02	1.3	0.0	0.1	0.0	-0.0	-0.0	3
37	0.00	0.5	0.0	0.0	0.0	-0.1	0.0	4
37	1.02	1.3	0.0	0.0	0.0	-0.0	-0.0	4
38	0.00	0.4	0.0	0.0	0.0	0.0	0.0	1
38	1.02	1.2	0.0	0.0	0.0	0.0	-0.0	1
38	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
38	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
38	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0	3
38	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3
38	0.00	0.5	0.0	0.2	0.0	-0.2	0.0	1
38	1.02	1.5	0.0	0.2	0.0	-0.0	-0.0	1
38	0.00	0.4	0.0	0.1	0.0	-0.2	0.0	2
38	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0	2
38	0.00	0.4	0.0	0.1	0.0	-0.1	0.0	3
38	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0	3
38	0.00	0.4	0.0	0.0	0.0	-0.0	0.0	4
38	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0	4
39	0.00	0.4	0.0	0.0	0.0	0.0	0.0	1
39	1.02	1.2	0.0	0.0	0.0	0.0	-0.0	1
39	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
39	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
39	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0	3
39	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3
39	0.00	0.5	0.0	0.2	0.0	-0.2	0.0	1
39	1.02	1.5	0.0	0.2	0.0	-0.0	-0.0	1
39	0.00	0.4	0.0	0.1	0.0	-0.2	0.0	2
39	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0	2
39	0.00	0.4	0.0	0.1	0.0	-0.1	0.0	3
39	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0	3
39	0.00	0.4	0.0	0.0	0.0	-0.0	0.0	4
39	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0	4
40	0.00	0.4	-0.0	0.0	0.0	0.0	-0.0	1
40	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1
40	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
40	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
40	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0	3
40	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3
40	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0	1
40	1.02	1.5	-0.0	0.2	0.0	-0.0	0.0	1
40	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0	2
40	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	2
40	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0	3
40	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	3
40	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	4
40	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	4
41	0.00	0.4	-0.0	-0.0	0.0	0.0	-0.0	1
41	1.02	1.2	-0.0	-0.0	0.0	0.0	0.0	1
41	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
41	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
41	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0	3
41	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3
41	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0	1
41	1.02	1.5	-0.0	0.2	0.0	-0.0	0.0	1
41	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0	2
41	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	2
41	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	3
41	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	3
41	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	4
41	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	4
42	0.00	0.4	-0.0	-0.0	0.0	0.0	-0.0	1
42	1.02	1.2	-0.0	-0.0	0.0	0.0	0.0	1
42	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
42	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
42	0.00	0.0	-0.0	0.1	0.0	-0.2	-0.0	3
42	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3
42	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0	1
42	1.02	1.6	-0.0	0.2	0.0	-0.0	0.0	1
42	0.00	0.4	-0.0	0.1	0.0	-0.2	-0.0	2
42	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	2
42	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0	3
42	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	3
42	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	4
42	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	4
43	0.00	0.5	-0.0	-0.0	0.0	0.0	-0.0	1
43	1.02	1.3	-0.0	-0.0	0.0	0.0	0.0	1
43	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
43	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
43	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0	3
43	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3
43	0.00	0.6	-0.0	0.2	0.0	-0.3	-0.0	1
43	1.02	1.7	-0.0	0.2	0.0	-0.0	0.0	1
43	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0	2
43	1.02	1.3	-0.0	0.1	0.0	-0.0	0.0	2
43	0.00	0.5	-0.0	0.1	0.0	-0.1	-0.0	3
43	1.02	1.3	-0.0	0.1	0.0	-0.0	0.0	3
43	0.00	0.5	-0.0	0.0	0.0	-0.1	-0.0	4
43	1.02	1.3	-0.0	0.0	0.0	-0.0	0.0	4
44	0.00	-0.2	-0.0	-0.0	0.0	0.0	-0.0	1
44	1.02	0.6	-0.0	-0.0	0.0	-0.0	0.0	1
44	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
44	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
44	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0	3
44	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0	3
44	0.00	-0.3	-0.0	0.3	0.0	-0.3	-0.0	1
44	1.02	0.7	-0.0	0.3	0.0	-0.0	0.0	1
44	0.00	-0.2	-0.0	0.2	0.0	-0.2	-0.0	2
44	1.02	0.6	-0.0	0.2	0.0	-0.0	0.0	2
44	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0	3
44	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0	3
44	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0	4
44	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0	4
65	0.00	-32.0	-0.1	0.0	0.0	0.0	-0.0	1
65	0.27	-29.3	-0.1	0.0	0.0	0.0	0.0	1
65	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
65	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
65	0.00	0.0	0.1	201.1	1.9	-251.1	0.0	3
65	0.27	0.0	0.1	201.1	1.9	-196.8	-0.0	3
65	0.00	-41.6	-0.0	301.7	2.8	-376.7	-0.0	1
65	0.27	-38.0	-0.0	301.7	2.8	-295.2	0.0	1
65	0.00	-32.0	-0.0	201.1	1.9	-251.1	-0.0	2

65	0.27	-29.2	-0.0	201.1	1.9	-196.8	0.0	2
65	0.00	-32.0	-0.1	100.6	0.9	-125.6	-0.0	3
65	0.27	-29.3	-0.1	100.6	0.9	-98.4	0.0	3
65	0.00	-32.0	-0.1	60.3	0.6	-75.3	-0.0	4
65	0.27	-29.3	-0.1	60.3	0.6	-59.0	0.0	4
67	0.00	-27.7	-0.0	0.0	0.0	0.0	0.0	1
67	1.02	-17.3	-0.0	0.0	0.0	0.0	0.0	1
67	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
67	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
67	0.00	0.0	-0.0	197.4	2.9	-195.3	-0.0	3
67	1.02	0.0	-0.0	197.4	2.9	6.1	0.0	3
67	0.00	-36.0	-0.0	296.1	4.4	-292.9	-0.0	1
67	1.02	-22.5	-0.0	296.1	4.4	9.1	0.0	1
67	0.00	-27.7	-0.0	197.4	2.9	-195.3	-0.0	2
67	1.02	-17.3	-0.0	197.4	2.9	6.1	0.0	2
67	0.00	-27.7	-0.0	98.7	1.5	-97.6	0.0	3
67	1.02	-17.3	-0.0	98.7	1.5	3.0	0.0	3
67	0.00	-27.7	-0.0	59.2	0.9	-58.6	0.0	4
67	1.02	-17.3	-0.0	59.2	0.9	1.8	0.0	4
68	0.00	-27.7	0.0	0.0	-0.0	0.0	-0.0	1
68	1.02	-17.3	0.0	0.0	-0.0	0.0	-0.0	1
68	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
68	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
68	0.00	0.0	0.0	197.4	-2.9	-195.3	0.0	3
68	1.02	0.0	0.0	197.4	-2.9	6.1	-0.0	3
68	0.00	-36.0	0.0	296.1	-4.4	-292.9	0.0	1
68	1.02	-22.5	0.0	296.1	-4.4	9.1	-0.0	1
68	0.00	-27.7	0.0	197.4	-2.9	-195.3	0.0	2
68	1.02	-17.3	0.0	197.4	-2.9	6.1	-0.0	2
68	0.00	-27.7	0.0	98.7	-1.5	-97.6	-0.0	3
68	1.02	-17.3	0.0	98.7	-1.5	3.0	-0.0	3
68	0.00	-27.7	0.0	59.2	-0.9	-58.6	-0.0	4
68	1.02	-17.3	0.0	59.2	-0.9	1.8	-0.0	4
70	0.00	-32.0	0.1	0.0	-0.0	0.0	0.0	1
70	0.27	-29.3	0.1	0.0	-0.0	0.0	-0.0	1
70	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
70	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
70	0.00	0.0	-0.1	201.1	-1.9	-251.1	-0.0	3
70	0.27	0.0	-0.1	201.1	-1.9	-196.8	0.0	3
70	0.00	-41.6	0.0	301.7	-2.8	-376.7	0.0	1
70	0.27	-38.0	0.0	301.7	-2.8	-295.2	-0.0	1
70	0.00	-32.0	0.0	201.1	-1.9	-251.1	0.0	2
70	0.27	-29.2	0.0	201.1	-1.9	-196.8	-0.0	2
70	0.00	-32.0	0.1	100.6	-0.9	-125.6	0.0	3
70	0.27	-29.3	0.1	100.6	-0.9	-98.4	-0.0	3
70	0.00	-32.0	0.1	60.3	-0.6	-75.3	0.0	4
70	0.27	-29.3	0.1	60.3	-0.6	-59.0	-0.0	4
91	0.00	-0.2	-0.0	0.0	0.0	0.0	-0.0	1
91	1.02	0.6	-0.0	0.0	0.0	0.0	0.0	1
91	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
91	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
91	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0	3
91	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0	3
91	0.00	-0.3	-0.0	0.3	0.0	-0.3	-0.0	1
91	1.02	0.7	-0.0	0.3	0.0	-0.0	0.0	1
91	0.00	-0.3	-0.0	0.2	0.0	-0.2	-0.0	2
91	1.02	0.5	-0.0	0.2	0.0	-0.0	0.0	2
91	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0	3
91	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0	3
91	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0	4
91	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0	4
92	0.00	0.5	-0.0	0.0	0.0	0.0	-0.0	1
92	1.02	1.3	-0.0	0.0	0.0	0.0	0.0	1
92	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
92	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
92	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0	3
92	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0	3
92	0.00	0.6	-0.0	0.2	0.0	-0.3	-0.0	1
92	1.02	1.7	-0.0	0.2	0.0	-0.0	0.0	1
92	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0	2
92	1.02	1.3	-0.0	0.2	0.0	-0.0	0.0	2
92	0.00	0.5	-0.0	0.1	0.0	-0.1	-0.0	3
92	1.02	1.3	-0.0	0.1	0.0	-0.0	0.0	3
92	0.00	0.5	-0.0	0.0	0.0	-0.1	-0.0	4
92	1.02	1.3	-0.0	0.0	0.0	-0.0	0.0	4
93	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	1
93	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1
93	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
93	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
93	0.00	0.0	-0.0	0.1	0.0	-0.2	-0.0	3
93	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3
93	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0	1
93	1.02	1.6	-0.0	0.2	0.0	-0.0	0.0	1
93	0.00	0.4	-0.0	0.1	0.0	-0.2	-0.0	2
93	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	2
93	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0	3
93	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	3
93	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	4
93	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	4
94	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	1
94	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1
94	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
94	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
94	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0	3
94	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3
94	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0	1
94	1.02	1.5	-0.0	0.2	0.0	-0.1	0.0	1
94	0.00	0.4	-0.0	0.1	0.0	-0.2	-0.0	2
94	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	2
94	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0	3
94	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0	3
94	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	4
94	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0	4
95	0.00	0.4	-0.0	0.0	0.0	-0.0	0.0	1
95	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1
95	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
95	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
95	0.00	-0.0	-0.0	0.1	-0.0	-0.1	-0.0	3
95	1.02	-0.0	-0.0	0.1	-0.0	-0.0	-0.0	3
95	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0	1
95	1.02	1.5	0.0	0.2	-0.0	-0.1	0.0	1
95	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0	2
95	1.02	1.2	0.0	0.1	-0.0	-0.0	0.0	2
95	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0	3
95	1.02	1.2	0.0	0.1	-0.0	-0.0	0.0	3
95	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	4
95	1.02	1.2	0.0	0.0	-0.0	-0.0	0.0	4
96	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	1

96	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1
96	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
96	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
96	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0	3
96	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3
96	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0	1
96	1.02	1.5	0.0	0.2	-0.0	-0.1	-0.0	1
96	0.00	0.4	0.0	0.1	-0.0	-0.2	0.0	2
96	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0	2
96	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0	3
96	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0	3
96	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	4
96	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0	4
97	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	1
97	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1
97	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
97	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
97	0.00	0.0	0.0	0.1	-0.0	-0.2	0.0	3
97	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3
97	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0	1
97	1.02	1.6	0.0	0.2	-0.0	-0.0	-0.0	1
97	0.00	0.4	0.0	0.1	-0.0	-0.2	0.0	2
97	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0	2
97	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0	3
97	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0	3
97	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	4
97	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0	4
98	0.00	0.5	0.0	0.0	-0.0	0.0	0.0	1
98	1.02	1.3	0.0	0.0	-0.0	0.0	-0.0	1
98	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
98	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
98	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0	3
98	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0	3
98	0.00	0.6	0.0	0.2	-0.0	-0.3	0.0	1
98	1.02	1.7	0.0	0.2	-0.0	-0.0	-0.0	1
98	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0	2
98	1.02	1.3	0.0	0.2	-0.0	-0.0	-0.0	2
98	0.00	0.5	0.0	0.1	-0.0	-0.1	0.0	3
98	1.02	1.3	0.0	0.1	-0.0	-0.0	-0.0	3
98	0.00	0.5	0.0	0.0	-0.0	-0.1	0.0	4
98	1.02	1.3	0.0	0.0	-0.0	-0.0	-0.0	4
99	0.00	-0.2	0.0	0.0	-0.0	0.0	0.0	1
99	1.02	0.6	0.0	0.0	-0.0	0.0	-0.0	1
99	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
99	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
99	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0	3
99	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0	3
99	0.00	-0.3	0.0	0.3	-0.0	-0.3	0.0	1
99	1.02	0.7	0.0	0.3	-0.0	-0.0	-0.0	1
99	0.00	-0.3	0.0	0.2	-0.0	-0.2	0.0	2
99	1.02	0.5	0.0	0.2	-0.0	-0.0	-0.0	2
99	0.00	-0.2	0.0	0.1	-0.0	-0.1	0.0	3
99	1.02	0.6	0.0	0.1	-0.0	-0.0	-0.0	3
99	0.00	-0.2	0.0	0.1	-0.0	-0.1	0.0	4
99	1.02	0.6	0.0	0.1	-0.0	-0.0	-0.0	4
100	0.00	-0.2	0.0	-0.0	-0.0	0.0	0.0	1
100	1.02	0.6	0.0	-0.0	-0.0	-0.0	-0.0	1
100	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
100	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
100	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0	3
100	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0	3
100	0.00	-0.3	0.0	0.3	-0.0	-0.3	0.0	1
100	1.02	0.7	0.0	0.3	-0.0	-0.0	-0.0	1
100	0.00	-0.2	0.0	0.2	-0.0	-0.2	0.0	2
100	1.02	0.6	0.0	0.2	-0.0	-0.0	-0.0	2
100	0.00	-0.2	0.0	0.1	-0.0	-0.1	0.0	3
100	1.02	0.6	0.0	0.1	-0.0	-0.0	-0.0	3
100	0.00	-0.2	0.0	0.1	-0.0	-0.1	0.0	4
100	1.02	0.6	0.0	0.1	-0.0	-0.0	-0.0	4
101	0.00	0.5	0.0	-0.0	-0.0	0.0	0.0	1
101	1.02	1.3	0.0	-0.0	-0.0	0.0	-0.0	1
101	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
101	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
101	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0	3
101	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3
101	0.00	0.6	0.0	0.2	-0.0	-0.3	0.0	1
101	1.02	1.7	0.0	0.2	-0.0	-0.0	-0.0	1
101	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0	2
101	1.02	1.3	0.0	0.1	-0.0	-0.0	-0.0	2
101	0.00	0.5	0.0	0.1	-0.0	-0.1	0.0	3
101	1.02	1.3	0.0	0.1	-0.0	-0.0	-0.0	3
101	0.00	0.5	0.0	0.0	-0.0	-0.1	0.0	4
101	1.02	1.3	0.0	0.0	-0.0	-0.0	-0.0	4
102	0.00	0.4	0.0	-0.0	-0.0	0.0	0.0	1
102	1.02	1.2	0.0	-0.0	-0.0	0.0	-0.0	1
102	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
102	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
102	0.00	0.0	0.0	0.1	-0.0	-0.2	0.0	3
102	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3
102	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0	1
102	1.02	1.6	0.0	0.2	-0.0	-0.0	-0.0	1
102	0.00	0.4	0.0	0.1	-0.0	-0.2	0.0	2
102	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0	2
102	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0	3
102	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0	3
102	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	4
102	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0	4
103	0.00	0.4	0.0	-0.0	-0.0	0.0	0.0	1
103	1.02	1.2	0.0	-0.0	-0.0	0.0	-0.0	1
103	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
103	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
103	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0	3
103	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3
103	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0	1
103	1.02	1.5	0.0	0.2	-0.0	-0.0	-0.0	1
103	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0	2
103	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0	2
103	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0	3
103	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0	3
103	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	4
103	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0	4
104	0.00	0.4	0.0	0.0	-0.0	0.0	0.0	1
104	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1
104	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
104	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
104	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0	3
104	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3
104	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0	1

104	1.02	1.5	0.0	0.2	-0.0	-0.0	-0.0	1
104	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0	2
104	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0	2
104	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0	3
104	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0	3
104	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	4
104	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0	4
105	0.00	0.4	-0.0	0.0	-0.0	0.0	-0.0	1
105	1.02	1.2	-0.0	0.0	-0.0	0.0	0.0	1
105	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
105	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
105	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0	3
105	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3
105	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0	1
105	1.02	1.5	-0.0	0.2	-0.0	-0.0	0.0	1
105	0.00	0.4	-0.0	0.1	-0.0	-0.2	-0.0	2
105	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0	2
105	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0	3
105	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0	3
105	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0	4
105	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0	4
106	0.00	0.4	-0.0	0.0	-0.0	0.0	-0.0	1
106	1.02	1.2	-0.0	0.0	-0.0	0.0	0.0	1
106	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
106	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
106	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0	3
106	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3
106	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0	1
106	1.02	1.5	-0.0	0.2	-0.0	-0.0	0.0	1
106	0.00	0.4	-0.0	0.1	-0.0	-0.2	-0.0	2
106	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0	2
106	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0	3
106	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0	3
106	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0	4
106	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0	4
107	0.00	0.5	-0.0	0.0	-0.0	0.0	-0.0	1
107	1.02	1.3	-0.0	0.0	-0.0	0.0	0.0	1
107	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
107	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
107	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0	3
107	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0	3
107	0.00	0.6	-0.0	0.2	-0.0	-0.3	-0.0	1
107	1.02	1.7	-0.0	0.2	-0.0	-0.0	0.0	1
107	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0	2
107	1.02	1.3	-0.0	0.2	-0.0	-0.0	0.0	2
107	0.00	0.5	-0.0	0.1	-0.0	-0.1	-0.0	3
107	1.02	1.3	-0.0	0.1	-0.0	-0.0	0.0	3
107	0.00	0.5	-0.0	0.0	-0.0	-0.1	-0.0	4
107	1.02	1.3	-0.0	0.0	-0.0	-0.0	0.0	4
108	0.00	-0.2	-0.0	0.0	-0.0	0.0	-0.0	1
108	1.02	0.6	-0.0	0.0	-0.0	0.0	0.0	1
108	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
108	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
108	0.00	0.0	0.0	0.2	-0.0	-0.2	0.0	3
108	1.02	0.0	0.0	0.2	-0.0	-0.0	-0.0	3
108	0.00	-0.3	-0.0	0.3	-0.0	-0.3	-0.0	1
108	1.02	0.8	-0.0	0.3	-0.0	-0.0	0.0	1
108	0.00	-0.2	-0.0	0.2	-0.0	-0.2	-0.0	2
108	1.02	0.6	-0.0	0.2	-0.0	-0.0	0.0	2
108	0.00	-0.2	-0.0	0.1	-0.0	-0.1	-0.0	3
108	1.02	0.6	-0.0	0.1	-0.0	-0.0	0.0	3
108	0.00	-0.2	-0.0	0.1	-0.0	-0.1	-0.0	4
108	1.02	0.6	-0.0	0.1	-0.0	-0.0	0.0	4
129	0.00	-33.0	0.6	-0.0	-0.0	0.0	0.1	1
129	0.27	-30.2	0.6	-0.0	-0.0	0.0	-0.1	1
129	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
129	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
129	0.00	0.2	-0.4	182.6	-6.8	-227.4	-0.1	3
129	0.27	0.2	-0.4	182.6	-6.8	-178.1	0.0	3
129	0.00	-42.6	0.2	273.8	-10.2	-341.1	0.0	1
129	0.27	-39.1	0.2	273.8	-10.2	-267.2	-0.0	1
129	0.00	-32.8	0.2	182.6	-6.8	-227.4	0.0	2
129	0.27	-30.1	0.2	182.6	-6.8	-178.1	-0.0	2
129	0.00	-32.9	0.4	91.3	-3.4	-113.7	0.0	3
129	0.27	-30.1	0.4	91.3	-3.4	-89.0	-0.1	3
129	0.00	-32.9	0.5	54.8	-2.0	-68.2	0.1	4
129	0.27	-30.2	0.5	54.8	-2.0	-53.4	-0.1	4
131	0.00	-28.6	-0.2	-0.0	-0.0	0.0	-0.1	1
131	1.02	-18.2	-0.2	-0.0	-0.0	-0.0	0.1	1
131	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
131	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
131	0.00	0.1	0.1	178.6	-10.3	-176.8	0.1	3
131	1.02	0.1	0.1	178.6	-10.3	5.4	-0.1	3
131	0.00	-37.0	-0.1	267.9	-15.4	-265.2	-0.0	1
131	1.02	-23.5	-0.1	267.9	-15.4	8.1	0.1	1
131	0.00	-28.5	-0.1	178.6	-10.3	-176.8	-0.0	2
131	1.02	-18.1	-0.1	178.6	-10.3	5.4	0.1	2
131	0.00	-28.6	-0.2	89.3	-5.1	-88.4	-0.1	3
131	1.02	-18.2	-0.2	89.3	-5.1	2.7	0.1	3
131	0.00	-28.6	-0.2	53.6	-3.1	-53.0	-0.1	4
131	1.02	-18.2	-0.2	53.6	-3.1	1.6	0.1	4
132	0.00	-17.8	1.3	0.0	-0.0	-0.0	0.3	1
132	1.02	-7.4	1.3	0.0	-0.0	-0.0	-1.0	1
132	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
132	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
132	0.00	-0.2	0.2	121.1	-16.4	-134.3	0.1	3
132	1.02	-0.2	0.2	121.1	-16.4	-10.9	-0.1	3
132	0.00	-23.4	1.9	181.6	-24.6	-201.5	0.6	1
132	1.02	-9.9	1.9	181.6	-24.6	-16.3	-1.4	1
132	0.00	-18.0	1.5	121.1	-16.4	-134.3	0.4	2
132	1.02	-7.6	1.5	121.1	-16.4	-10.9	-1.1	2
132	0.00	-17.9	1.4	60.5	-8.2	-67.2	0.4	3
132	1.02	-7.5	1.4	60.5	-8.2	-5.4	-1.0	3
132	0.00	-17.9	1.3	36.3	-4.9	-40.3	0.4	4
132	1.02	-7.5	1.3	36.3	-4.9	-3.3	-1.0	4
134	0.00	-21.8	-0.7	0.0	-0.0	-0.0	0.0	1
134	0.27	-19.1	-0.7	0.0	-0.0	-0.0	0.2	1
134	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
134	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2
134	0.00	-0.2	-1.0	116.3	-13.4	-166.5	-0.2	3
134	0.27	-0.2	-1.0	116.3	-13.4	-135.1	0.1	3
134	0.00	-28.7	-2.4	174.5	-20.1	-249.7	-0.2	1
134	0.27	-25.1	-2.4	174.5	-20.1	-202.6	0.5	1
134	0.00	-22.0	-1.7	116.3	-13.4	-166.5	-0.1	2
134	0.27	-19.3	-1.7	116.3	-13.4	-135.1	0.3	2
134	0.00	-21.9	-1.2	58.2	-6.7	-83.3	-0.0	3
134	0.27	-19.2	-1.2	58.2	-6.7	-67.5	0.3	3
134	0.00	-21.9	-1.0	34.9	-4.0	-50.0	-0.0	4

134	0.27	-19.1	-1.0	34.9	-4.0	-40.5	0.3		4
155	0.00	-0.3	-0.0	-0.0	-0.0	0.0	-0.0	1	
155	1.02	0.5	-0.0	-0.0	-0.0	-0.0	0.0	1	
155	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
155	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
155	0.00	0.0	0.0	0.2	-0.0	-0.2	0.0	3	
155	1.02	0.0	0.0	0.2	-0.0	-0.0	-0.0	3	
155	0.00	-0.3	-0.0	0.3	-0.0	-0.3	-0.0		1
155	1.02	0.7	-0.0	0.3	-0.0	-0.0	0.0		1
155	0.00	-0.3	-0.0	0.2	-0.0	-0.2	-0.0		2
155	1.02	0.5	-0.0	0.2	-0.0	-0.0	0.0		2
155	0.00	-0.3	-0.0	0.1	-0.0	-0.1	-0.0		3
155	1.02	0.5	-0.0	0.1	-0.0	-0.0	0.0		3
155	0.00	-0.3	-0.0	0.1	-0.0	-0.1	-0.0		4
155	1.02	0.5	-0.0	0.1	-0.0	-0.0	0.0		4
156	0.00	0.5	-0.0	-0.0	-0.0	0.0	-0.0	1	
156	1.02	1.3	-0.0	-0.0	-0.0	-0.0	0.0	1	
156	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
156	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
156	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0	3	
156	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
156	0.00	0.6	-0.0	0.2	-0.0	-0.2	-0.0		1
156	1.02	1.7	-0.0	0.2	-0.0	-0.0	0.0		1
156	0.00	0.5	-0.0	0.1	-0.0	-0.2	-0.0		2
156	1.02	1.3	-0.0	0.1	-0.0	-0.0	0.0		2
156	0.00	0.5	-0.0	0.1	-0.0	-0.1	-0.0		3
156	1.02	1.3	-0.0	0.1	-0.0	-0.0	0.0		3
156	0.00	0.5	-0.0	0.0	-0.0	-0.0	-0.0		4
156	1.02	1.3	-0.0	0.0	-0.0	-0.0	0.0		4
157	0.00	0.4	-0.0	-0.0	-0.0	0.0	-0.0	1	
157	1.02	1.2	-0.0	-0.0	-0.0	0.0	0.0	1	
157	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
157	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
157	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0	3	
157	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
157	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0		1
157	1.02	1.6	-0.0	0.2	-0.0	-0.0	0.0		1
157	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0		2
157	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0		2
157	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0		3
157	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0		3
157	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0		4
157	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		4
158	0.00	0.4	-0.0	-0.0	-0.0	0.0	-0.0	1	
158	1.02	1.2	-0.0	-0.0	-0.0	0.0	0.0	1	
158	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
158	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
158	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0	3	
158	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
158	0.00	0.5	-0.0	0.1	-0.0	-0.2	-0.0		1
158	1.02	1.5	-0.0	0.1	-0.0	-0.0	0.0		1
158	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0		2
158	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0		2
158	0.00	0.4	-0.0	0.0	-0.0	-0.1	-0.0		3
158	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		3
158	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0		4
158	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		4
159	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0	1	
159	1.02	1.2	-0.0	0.0	-0.0	0.0	0.0	1	
159	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
159	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
159	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0	3	
159	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
159	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0		1
159	1.02	1.5	0.0	0.1	-0.0	-0.1	-0.0		1
159	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		2
159	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		2
159	0.00	0.4	-0.0	0.0	-0.0	-0.1	-0.0		3
159	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		3
159	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0		4
159	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		4
160	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	1	
160	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1	
160	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
160	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
160	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0	3	
160	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
160	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0		1
160	1.02	1.5	0.0	0.1	-0.0	-0.1	-0.0		1
160	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		2
160	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		2
160	0.00	0.4	0.0	0.0	-0.0	-0.1	0.0		3
160	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		3
160	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0		4
160	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		4
161	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	1	
161	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1	
161	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
161	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
161	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0	3	
161	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
161	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0		1
161	1.02	1.6	0.0	0.1	-0.0	-0.1	-0.0		1
161	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		2
161	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		2
161	0.00	0.4	0.0	0.0	-0.0	-0.1	0.0		3
161	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		3
161	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0		4
161	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		4
162	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	1	
162	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1	
162	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
162	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
162	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0	3	
162	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
162	0.00	0.6	0.0	0.1	-0.0	-0.2	0.0		1
162	1.02	1.6	0.0	0.1	-0.0	-0.1	-0.0		1
162	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		2
162	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		2
162	0.00	0.4	0.0	0.0	-0.0	-0.1	0.0		3
162	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		3
162	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0		4
162	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		4
163	0.00	-0.7	0.0	0.0	-0.0	-0.0	0.0	1	
163	1.02	0.1	0.0	0.0	-0.0	-0.0	-0.0	1	
163	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
163	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
163	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0	3	

163	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
163	0.00	-0.9	0.0	0.2	-0.0	-0.2	0.0		1
163	1.02	0.1	0.0	0.2	-0.0	-0.0	-0.0		1
163	0.00	-0.7	0.0	0.1	-0.0	-0.1	0.0		2
163	1.02	0.1	0.0	0.1	-0.0	-0.0	-0.0		2
163	0.00	-0.7	0.0	0.1	-0.0	-0.1	0.0		3
163	1.02	0.1	0.0	0.1	-0.0	-0.0	-0.0		3
163	0.00	-0.7	0.0	0.0	-0.0	-0.0	0.0		4
163	1.02	0.1	0.0	0.0	-0.0	-0.0	-0.0		4

Di seguito si riportano le spiegazioni delle sigle usate nella tabella TENSIONI TRAVI E PILASTRI.

ELEM.	numero dell' elemento									
n.ro										
x	ascissa locale misurata dal nodo I al nodo J									
N/A	tensione da sforzo normale nel p.to x									
M2/W2	tensione da momento flettente ' ' ' intorno asse 2 locale									
M3/W3	tensione da momento flettente ' ' ' ' 3 '									

RISULTATI : TENSIONI TRAVI PER N.RO DI ELEMENTO

8	10.00	0.5	-14.6	0.7		4
9	0.00	0.4	0.0	0.4	1	
9	4.74	0.4	0.0	1.1	1	
9	10.00	0.4	0.0	0.7	1	
9	0.00	-0.0	-0.0	-0.0	2	
9	4.74	-0.0	-0.0	-0.0	2	
9	10.00	-0.0	-0.0	-0.0	2	
9	0.00	0.2	-49.1	-0.1	3	
9	4.74	0.2	-43.5	-0.1	3	
9	10.00	0.2	-37.3	-0.0	3	
9	0.00	0.9	-73.7	0.3		1
9	4.74	0.9	-65.3	1.4		1
9	10.00	0.9	-55.9	0.9		1
9	0.00	0.6	-49.1	0.3		2
9	4.74	0.6	-43.5	1.1		2
9	10.00	0.6	-37.3	0.7		2
9	0.00	0.5	-24.6	0.3		3
9	4.74	0.5	-21.7	1.1		3
9	10.00	0.5	-18.6	0.7		3
9	0.00	0.5	-14.7	0.3		4
9	4.74	0.5	-13.0	1.1		4
9	10.00	0.5	-11.2	0.7		4
10	0.00	0.4	0.0	0.5	1	
10	4.74	0.4	0.0	1.3	1	
10	10.00	0.4	0.0	1.0	1	
10	0.00	-0.0	-0.0	-0.0	2	
10	4.74	-0.0	-0.0	-0.0	2	
10	10.00	-0.0	-0.0	-0.0	2	
10	0.00	0.2	-37.9	-0.1	3	
10	4.74	0.2	-32.2	-0.0	3	
10	10.00	0.2	-25.8	-0.0	3	
10	0.00	0.9	-56.8	0.5		1
10	4.74	0.9	-48.2	1.7		1
10	10.00	0.9	-38.7	1.3		1
10	0.00	0.6	-37.9	0.4		2
10	4.74	0.6	-32.2	1.3		2
10	10.00	0.6	-25.8	1.0		2
10	0.00	0.5	-18.9	0.4		3
10	4.74	0.5	-16.1	1.3		3
10	10.00	0.5	-12.9	1.0		3
10	0.00	0.5	-11.4	0.5		4
10	4.74	0.5	-9.6	1.3		4
10	10.00	0.5	-7.7	1.0		4
11	0.00	0.4	0.0	0.9	1	
11	4.74	0.4	0.0	1.5	1	
11	10.00	0.4	0.0	1.0	1	
11	0.00	-0.0	-0.0	-0.0	2	
11	4.74	-0.0	-0.0	-0.0	2	
11	10.00	-0.0	-0.0	-0.0	2	
11	0.00	0.2	-26.4	-0.1	3	
11	4.74	0.2	-20.6	-0.0	3	
11	10.00	0.2	-14.1	0.0	3	
11	0.00	0.9	-39.6	1.1		1
11	4.74	0.9	-30.9	2.0		1
11	10.00	0.9	-21.2	1.3		1
11	0.00	0.6	-26.4	0.9		2
11	4.74	0.6	-20.6	1.5		2
11	10.00	0.6	-14.1	1.0		2
11	0.00	0.5	-13.2	0.9		3
11	4.74	0.5	-10.3	1.5		3
11	10.00	0.5	-7.1	1.0		3
11	0.00	0.5	-7.9	0.9		4
11	4.74	0.5	-6.2	1.5		4
11	10.00	0.5	-4.2	1.0		4
12	0.00	0.4	0.0	1.1	1	
12	4.74	0.4	-0.0	1.5	1	
12	10.00	0.4	-0.0	0.7	1	
12	0.00	-0.0	-0.0	-0.0	2	
12	4.74	-0.0	-0.0	-0.0	2	
12	10.00	-0.0	-0.0	-0.0	2	
12	0.00	0.2	-14.7	-0.0	3	
12	4.74	0.2	-8.8	0.0	3	
12	10.00	0.2	-2.2	0.0	3	
12	0.00	0.9	-22.0	1.3		1
12	4.74	0.9	-13.2	1.9		1
12	10.00	0.9	-3.4	0.9		1
12	0.00	0.6	-14.7	1.0		2
12	4.74	0.6	-8.8	1.5		2
12	10.00	0.6	-2.2	0.7		2
12	0.00	0.5	-7.3	1.0		3
12	4.74	0.5	-4.4	1.5		3
12	10.00	0.5	-1.1	0.7		3
12	0.00	0.5	-4.4	1.0		4
12	4.74	0.5	-2.6	1.5		4
12	10.00	0.5	-0.7	0.7		4
13	0.00	0.4	-0.0	0.9	1	
13	4.74	0.4	-0.0	1.0	1	
13	10.00	0.4	-0.0	0.0	1	
13	0.00	-0.0	-0.0	-0.0	2	
13	4.74	-0.0	-0.0	-0.0	2	
13	10.00	-0.0	-0.0	-0.0	2	
13	0.00	0.2	-2.7	-0.0	3	
13	4.74	0.2	3.3	0.0	3	
13	10.00	0.2	9.9	0.1	3	
13	0.00	0.9	-4.1	1.1		1
13	4.74	0.9	4.9	1.4		1
13	10.00	0.9	14.9	0.1		1
13	0.00	0.6	-2.8	0.9		2
13	4.74	0.6	3.3	1.1		2
13	10.00	0.6	9.9	0.1		2
13	0.00	0.5	-1.4	0.9		3
13	4.74	0.5	1.6	1.1		3
13	10.00	0.5	5.0	0.1		3
13	0.00	0.5	-0.8	0.9		4
13	4.74	0.5	1.0	1.1		4
13	10.00	0.5	3.0	0.0		4
14	0.00	0.4	-0.0	0.3	1	
14	4.74	0.4	-0.0	0.5	1	
14	10.00	0.4	-0.0	-0.5	1	
14	0.00	-0.0	-0.0	-0.0	2	
14	4.74	-0.0	-0.0	-0.0	2	
14	10.00	-0.0	-0.0	-0.0	2	
14	0.00	0.2	9.5	0.0	3	
14	4.74	0.2	15.6	0.0	3	
14	10.00	0.2	22.4	0.1	3	
14	0.00	0.9	14.2	0.4		1
14	4.74	0.9	23.4	0.7		1
14	10.00	0.9	33.6	-0.5		1

14	0.00	0.6	9.5	0.3		2
14	4.74	0.6	15.6	0.6		2
14	10.00	0.6	22.4	-0.4		2
14	0.00	0.5	4.7	0.3		3
14	4.74	0.5	7.8	0.5		3
14	10.00	0.5	11.2	-0.5		3
14	0.00	0.5	2.8	0.3		4
14	4.74	0.5	4.7	0.5		4
14	10.00	0.5	6.7	-0.5		4
15	0.00	0.4	-0.0	-0.2	1	
15	4.74	0.4	-0.0	0.6	1	
15	10.00	0.4	-0.0	0.1	1	
15	0.00	-0.0	-0.0	-0.0	2	
15	4.74	-0.0	-0.0	-0.0	2	
15	10.00	-0.0	-0.0	-0.0	2	
15	0.00	0.2	22.0	0.0	3	
15	4.74	0.2	28.3	0.1	3	
15	10.00	0.2	35.3	0.1	3	
15	0.00	0.9	33.0	-0.2		1
15	4.74	0.9	42.5	0.8		1
15	10.00	0.9	53.0	0.3		1
15	0.00	0.6	22.0	-0.1		2
15	4.74	0.6	28.3	0.6		2
15	10.00	0.6	35.3	0.2		2
15	0.00	0.5	11.0	-0.2		3
15	4.74	0.5	14.1	0.6		3
15	10.00	0.5	17.6	0.2		3
15	0.00	0.5	6.6	-0.2		4
15	4.74	0.5	8.5	0.6		4
15	10.00	0.5	10.6	0.2		4
16	0.00	0.4	-0.0	0.5	1	
16	4.74	0.4	-0.0	-2.7	1	
16	10.00	0.4	-0.0	-7.5	1	
16	0.00	-0.0	-0.0	-0.0	2	
16	4.74	-0.0	-0.0	-0.0	2	
16	10.00	-0.0	-0.0	-0.0	2	
16	0.00	0.2	35.0	0.0	3	
16	4.74	0.2	41.5	0.3	3	
16	10.00	0.2	48.7	0.5	3	
16	0.00	0.9	52.4	0.7		1
16	4.74	0.9	62.2	-3.1		1
16	10.00	0.9	73.0	-8.9		1
16	0.00	0.6	34.9	0.5		2
16	4.74	0.6	41.5	-2.4		2
16	10.00	0.6	48.7	-7.0		2
16	0.00	0.5	17.5	0.5		3
16	4.74	0.5	20.7	-2.6		3
16	10.00	0.5	24.3	-7.2		3
16	0.00	0.5	10.5	0.5		4
16	4.74	0.5	12.4	-2.6		4
16	10.00	0.5	14.6	-7.3		4
17	0.00	-0.1	0.0	-6.8	1	
17	4.74	-0.1	0.0	-4.4	1	
17	10.00	-0.1	0.0	-1.8	1	
17	0.00	-0.0	-0.0	-0.0	2	
17	4.74	-0.0	-0.0	-0.0	2	
17	10.00	-0.0	-0.0	-0.0	2	
17	0.00	-0.0	101.6	-0.6	3	
17	4.74	-0.0	67.4	-0.6	3	
17	10.00	-0.0	32.6	-0.5	3	
17	0.00	-0.2	152.4	-9.8		1
17	4.74	-0.2	101.1	-6.5		1
17	10.00	-0.2	49.0	-3.2		1
17	0.00	-0.1	101.6	-7.4		2
17	4.74	-0.1	67.4	-4.9		2
17	10.00	-0.1	32.7	-2.4		2
17	0.00	-0.1	50.8	-7.1		3
17	4.74	-0.1	33.7	-4.7		3
17	10.00	-0.1	16.3	-2.1		3
17	0.00	-0.1	30.5	-7.0		4
17	4.74	-0.1	20.2	-4.5		4
17	10.00	-0.1	9.8	-2.0		4
18	0.00	-0.1	0.0	-1.9	1	
18	4.74	-0.1	0.0	0.2	1	
18	10.00	-0.1	0.0	2.4	1	
18	0.00	-0.0	-0.0	-0.0	2	
18	4.74	-0.0	-0.0	-0.0	2	
18	10.00	-0.0	-0.0	-0.0	2	
18	0.00	-0.0	32.8	-0.5	3	
18	4.74	-0.0	4.4	-0.5	3	
18	10.00	-0.0	-23.8	-0.4	3	
18	0.00	-0.2	49.2	-3.2		1
18	4.74	-0.2	6.7	-0.4		1
18	10.00	-0.2	-35.7	2.6		1
18	0.00	-0.1	32.8	-2.4		2
18	4.74	-0.1	4.4	-0.2		2
18	10.00	-0.1	-23.8	2.0		2
18	0.00	-0.1	16.4	-2.1		3
18	4.74	-0.1	2.2	0.0		3
18	10.00	-0.1	-11.9	2.2		3
18	0.00	-0.1	9.8	-2.0		4
18	4.74	-0.1	1.3	0.1		4
18	10.00	-0.1	-7.1	2.3		4
19	0.00	-0.1	0.0	2.4	1	
19	4.74	-0.1	0.0	3.8	1	
19	10.00	-0.1	0.0	5.3	1	
19	0.00	-0.0	-0.0	-0.0	2	
19	4.74	-0.0	-0.0	-0.0	2	
19	10.00	-0.0	-0.0	-0.0	2	
19	0.00	-0.0	-23.6	-0.4	3	
19	4.74	-0.0	-46.1	-0.3	3	
19	10.00	-0.0	-67.9	-0.3	3	
19	0.00	-0.2	-35.5	2.5		1
19	4.74	-0.2	-69.2	4.5		1
19	10.00	-0.2	-101.8	6.5		1
19	0.00	-0.1	-23.6	2.0		2
19	4.74	-0.1	-46.1	3.5		2
19	10.00	-0.1	-67.9	5.0		2
19	0.00	-0.1	-11.8	2.2		3
19	4.74	-0.1	-23.1	3.7		3
19	10.00	-0.1	-33.9	5.2		3
19	0.00	-0.1	-7.1	2.3		4
19	4.74	-0.1	-13.8	3.7		4
19	10.00	-0.1	-20.4	5.2		4
20	0.00	-0.1	0.0	5.3	1	
20	4.74	-0.1	0.0	6.0	1	
20	10.00	-0.1	-0.0	6.8	1	
20	0.00	-0.0	-0.0	-0.0	2	

20	4.74	-0.0	-0.0	-0.0
20	10.00	-0.0	-0.0	-0.0
20	0.00	-0.0	-67.7	-0.3
20	4.74	-0.0	-84.4	-0.2
20	10.00	-0.0	-99.6	-0.1
20	0.00	-0.2	-101.6	6.5
20	4.74	-0.2	-126.5	7.6
20	10.00	-0.2	-149.4	8.6
20	0.00	-0.1	-67.7	5.0
20	4.74	-0.1	-84.4	5.8
20	10.00	-0.1	-99.6	6.6
20	0.00	-0.1	-33.9	5.1
20	4.74	-0.1	-42.2	5.9
20	10.00	-0.1	-49.8	6.7
20	0.00	-0.1	-20.3	5.2
20	4.74	-0.1	-25.3	6.0
20	10.00	-0.1	-29.9	6.7
21	0.00	-0.1	-0.0	6.8
21	4.74	-0.1	-0.0	6.9
21	10.00	-0.1	-0.0	6.9
21	0.00	-0.0	-0.0	-0.0
21	4.74	-0.0	-0.0	-0.0
21	10.00	-0.0	-0.0	-0.0
21	0.00	-0.0	-99.4	-0.1
21	4.74	-0.0	-110.2	-0.1
21	10.00	-0.0	-118.9	-0.0
21	0.00	-0.2	-149.2	8.6
21	4.74	-0.2	-165.3	8.8
21	10.00	-0.2	-178.4	8.9
21	0.00	-0.1	-99.4	6.6
21	4.74	-0.1	-110.2	6.8
21	10.00	-0.1	-118.9	6.9
21	0.00	-0.1	-49.7	6.7
21	4.74	-0.1	-55.1	6.8
21	10.00	-0.1	-59.5	6.9
21	0.00	-0.1	-29.8	6.7
21	4.74	-0.1	-33.1	6.9
21	10.00	-0.1	-35.7	6.9
22	0.00	-0.1	-0.0	6.9
22	4.74	-0.1	-0.0	6.4
22	10.00	-0.1	-0.0	5.7
22	0.00	-0.0	-0.0	-0.0
22	4.74	-0.0	-0.0	-0.0
22	10.00	-0.0	-0.0	-0.0
22	0.00	-0.0	-118.8	-0.0
22	4.74	-0.0	-123.7	0.0
22	10.00	-0.0	-125.9	0.1
22	0.00	-0.2	-178.2	8.9
22	4.74	-0.2	-185.6	8.4
22	10.00	-0.2	-188.9	7.5
22	0.00	-0.1	-118.8	6.9
22	4.74	-0.1	-123.7	6.4
22	10.00	-0.1	-125.9	5.8
22	0.00	-0.1	-59.4	6.9
22	4.74	-0.1	-61.9	6.4
22	10.00	-0.1	-63.0	5.7
22	0.00	-0.1	-35.6	6.9
22	4.74	-0.1	-37.1	6.4
22	10.00	-0.1	-37.8	5.7
23	0.00	-0.1	-0.0	5.7
23	4.74	-0.1	-0.0	4.5
23	10.00	-0.1	-0.0	3.1
23	0.00	-0.0	-0.0	-0.0
23	4.74	-0.0	-0.0	-0.0
23	10.00	-0.0	-0.0	-0.0
23	0.00	-0.0	-125.8	0.1
23	4.74	-0.0	-124.9	0.2
23	10.00	-0.0	-120.6	0.2
23	0.00	-0.2	-188.7	7.6
23	4.74	-0.2	-187.3	6.1
23	10.00	-0.2	-180.9	4.4
23	0.00	-0.1	-125.8	5.8
23	4.74	-0.1	-124.9	4.7
23	10.00	-0.1	-120.6	3.3
23	0.00	-0.1	-62.9	5.7
23	4.74	-0.1	-62.5	4.6
23	10.00	-0.1	-60.3	3.2
23	0.00	-0.1	-37.7	5.7
23	4.74	-0.1	-37.5	4.6
23	10.00	-0.1	-36.2	3.2
24	0.00	-0.1	-0.0	3.1
24	4.74	-0.1	-0.0	1.3
24	10.00	-0.1	-0.0	-0.8
24	0.00	-0.0	-0.0	-0.0
24	4.74	-0.0	-0.0	-0.0
24	10.00	-0.0	-0.0	-0.0
24	0.00	-0.0	-120.5	0.2
24	4.74	-0.0	-113.7	0.3
24	10.00	-0.0	-102.9	0.4
24	0.00	-0.2	-180.7	4.4
24	4.74	-0.2	-170.6	2.2
24	10.00	-0.2	-154.4	-0.5
24	0.00	-0.1	-120.5	3.4
24	4.74	-0.1	-113.7	1.6
24	10.00	-0.1	-102.9	-0.5
24	0.00	-0.1	-60.3	3.2
24	4.74	-0.1	-56.9	1.5
24	10.00	-0.1	-51.5	-0.6
24	0.00	-0.1	-36.2	3.2
24	4.74	-0.1	-34.1	1.4
24	10.00	-0.1	-30.9	-0.7
25	0.00	-0.1	-0.0	-0.8
25	4.74	-0.1	-0.0	-3.3
25	10.00	-0.1	-0.0	-6.2
25	0.00	-0.0	-0.0	-0.0
25	4.74	-0.0	-0.0	-0.0
25	10.00	-0.0	-0.0	-0.0
25	0.00	-0.0	-102.8	0.4
25	4.74	-0.0	-90.2	0.4
25	10.00	-0.0	-72.9	0.5
25	0.00	-0.2	-154.2	-0.5
25	4.74	-0.2	-135.3	-3.7
25	10.00	-0.2	-109.4	-7.3
25	0.00	-0.1	-102.8	-0.4
25	4.74	-0.1	-90.2	-2.9
25	10.00	-0.1	-73.0	-5.7
25	0.00	-0.1	-51.4	-0.6
25	4.74	-0.1	-45.1	-3.1

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25	10.00	-0.1	-36.5	-6.0		3
25	0.00	-0.1	-30.9	-0.7		4
25	4.74	-0.1	-27.1	-3.2		4
25	10.00	-0.1	-21.9	-6.1		4
26	0.00	-0.1	-0.0	-6.2	1	
26	4.74	-0.1	-0.0	-9.1	1	
26	10.00	-0.1	-0.0	-12.5	1	
26	0.00	-0.0	-0.0	-0.0	2	
26	4.74	-0.0	-0.0	-0.0	2	
26	10.00	-0.0	-0.0	-0.0	2	
26	0.00	-0.0	-72.9	0.5	3	
26	4.74	-0.0	-54.4	0.5	3	
26	10.00	-0.0	-30.7	0.6	3	
26	0.00	-0.2	-109.3	-7.3		1
26	4.74	-0.2	-81.6	-11.0		1
26	10.00	-0.2	-46.0	-15.3		1
26	0.00	-0.1	-72.9	-5.7		2
26	4.74	-0.1	-54.4	-8.6		2
26	10.00	-0.1	-30.7	-11.9		2
26	0.00	-0.1	-36.4	-5.9		3
26	4.74	-0.1	-27.2	-8.8		3
26	10.00	-0.1	-15.4	-12.2		3
26	0.00	-0.1	-21.9	-6.0		4
26	4.74	-0.1	-16.3	-8.9		4
26	10.00	-0.1	-9.2	-12.3		4
45	0.00	-0.1	-0.0	-5.1	1	
45	4.74	-0.1	-0.0	-7.8	1	
45	10.00	-0.1	-0.0	-10.9	1	
45	0.00	-0.0	-0.0	-0.0	2	
45	4.74	-0.0	-0.0	-0.0	2	
45	10.00	-0.0	-0.0	-0.0	2	
45	0.00	-0.0	-29.0	0.2	3	
45	4.74	-0.0	-4.7	0.2	3	
45	10.00	-0.0	25.6	0.2	3	
45	0.00	-0.2	-43.6	-6.4		1
45	4.74	-0.2	-7.1	-9.9		1
45	10.00	-0.2	38.4	-13.9		1
45	0.00	-0.1	-29.0	-5.0		2
45	4.74	-0.1	-4.7	-7.6		2
45	10.00	-0.1	25.6	-10.7		2
45	0.00	-0.1	-14.5	-5.1		3
45	4.74	-0.1	-2.4	-7.7		3
45	10.00	-0.1	12.8	-10.8		3
45	0.00	-0.1	-8.7	-5.1		4
45	4.74	-0.1	-1.4	-7.8		4
45	10.00	-0.1	7.7	-10.8		4
46	0.00	-0.1	-0.0	-0.4	1	
46	4.74	-0.1	-0.0	-2.6	1	
46	10.00	-0.1	-0.0	-5.2	1	
46	0.00	-0.0	-0.0	-0.0	2	
46	4.74	-0.0	-0.0	-0.0	2	
46	10.00	-0.0	-0.0	-0.0	2	
46	0.00	-0.0	-71.4	0.1	3	
46	4.74	-0.0	-52.9	0.1	3	
46	10.00	-0.0	-29.1	0.2	3	
46	0.00	-0.2	-107.2	-0.3		1
46	4.74	-0.2	-79.4	-3.1		1
46	10.00	-0.2	-43.6	-6.5		1
46	0.00	-0.1	-71.4	-0.2		2
46	4.74	-0.1	-52.9	-2.4		2
46	10.00	-0.1	-29.1	-5.0		2
46	0.00	-0.1	-35.7	-0.3		3
46	4.74	-0.1	-26.5	-2.5		3
46	10.00	-0.1	-14.5	-5.1		3
46	0.00	-0.1	-21.4	-0.3		4
46	4.74	-0.1	-15.9	-2.5		4
46	10.00	-0.1	-8.7	-5.1		4
47	0.00	-0.1	-0.0	3.0	1	
47	4.74	-0.1	-0.0	1.5	1	
47	10.00	-0.1	-0.0	-0.4	1	
47	0.00	-0.0	-0.0	-0.0	2	
47	4.74	-0.0	-0.0	-0.0	2	
47	10.00	-0.0	-0.0	-0.0	2	
47	0.00	-0.0	-101.5	0.1	3	
47	4.74	-0.0	-88.8	0.1	3	
47	10.00	-0.0	-71.5	0.1	3	
47	0.00	-0.2	-152.3	4.1		1
47	4.74	-0.2	-133.3	2.1		1
47	10.00	-0.2	-107.2	-0.3		1
47	0.00	-0.1	-101.5	3.1		2
47	4.74	-0.1	-88.8	1.6		2
47	10.00	-0.1	-71.5	-0.2		2
47	0.00	-0.1	-50.8	3.0		3
47	4.74	-0.1	-44.4	1.5		3
47	10.00	-0.1	-35.7	-0.3		3
47	0.00	-0.1	-30.5	3.0		4
47	4.74	-0.1	-26.7	1.5		4
47	10.00	-0.1	-21.5	-0.3		4
48	0.00	-0.1	-0.0	5.0	1	
48	4.74	-0.1	-0.0	4.1	1	
48	10.00	-0.1	-0.0	3.0	1	
48	0.00	-0.0	-0.0	-0.0	2	
48	4.74	-0.0	-0.0	-0.0	2	
48	10.00	-0.0	-0.0	-0.0	2	
48	0.00	-0.0	-119.3	0.1	3	
48	4.74	-0.0	-112.4	0.1	3	
48	10.00	-0.0	-101.6	0.1	3	
48	0.00	-0.2	-179.0	6.6		1
48	4.74	-0.2	-168.7	5.5		1
48	10.00	-0.2	-152.4	4.0		1
48	0.00	-0.1	-119.3	5.0		2
48	4.74	-0.1	-112.5	4.2		2
48	10.00	-0.1	-101.6	3.1		2
48	0.00	-0.1	-59.7	5.0		3
48	4.74	-0.1	-56.2	4.1		3
48	10.00	-0.1	-50.8	3.0		3
48	0.00	-0.1	-35.8	5.0		4
48	4.74	-0.1	-33.7	4.1		4
48	10.00	-0.1	-30.5	3.0		4
49	0.00	-0.1	-0.0	5.6	1	
49	4.74	-0.1	-0.0	5.3	1	
49	10.00	-0.1	-0.0	4.9	1	
49	0.00	-0.0	-0.0	-0.0	2	
49	4.74	-0.0	-0.0	-0.0	2	
49	10.00	-0.0	-0.0	-0.0	2	
49	0.00	-0.0	-124.7	0.1	3	
49	4.74	-0.0	-123.7	0.1	3	
49	10.00	-0.0	-119.3	0.1	3	

49	0.00	-0.2	-187.1	7.3		1
49	4.74	-0.2	-185.6	7.1		1
49	10.00	-0.2	-179.0	6.6		1
49	0.00	-0.1	-124.7	5.6		2
49	4.74	-0.1	-123.7	5.4		2
49	10.00	-0.1	-119.4	5.0		2
49	0.00	-0.1	-62.4	5.6		3
49	4.74	-0.1	-61.9	5.4		3
49	10.00	-0.1	-59.7	5.0		3
49	0.00	-0.1	-37.4	5.6		4
49	4.74	-0.1	-37.1	5.4		4
49	10.00	-0.1	-35.8	5.0		4
50	0.00	-0.1	-0.0	4.8	1	
50	4.74	-0.1	-0.0	5.3	1	
50	10.00	-0.1	-0.0	5.6	1	
50	0.00	-0.0	-0.0	-0.0	2	
50	4.74	-0.0	-0.0	-0.0	2	
50	10.00	-0.0	-0.0	-0.0	2	
50	0.00	-0.0	-117.8	0.0	3	
50	4.74	-0.0	-122.7	0.1	3	
50	10.00	-0.0	-124.8	0.1	3	
50	0.00	-0.2	-176.8	6.4		1
50	4.74	-0.2	-184.0	6.9		1
50	10.00	-0.2	-187.2	7.3		1
50	0.00	-0.1	-117.9	4.9		2
50	4.74	-0.1	-122.7	5.3		2
50	10.00	-0.1	-124.8	5.6		2
50	0.00	-0.1	-58.9	4.9		3
50	4.74	-0.1	-61.4	5.3		3
50	10.00	-0.1	-62.4	5.6		3
50	0.00	-0.1	-35.4	4.9		4
50	4.74	-0.1	-36.8	5.3		4
50	10.00	-0.1	-37.5	5.6		4
51	0.00	-0.1	-0.0	2.8	1	
51	4.74	-0.1	-0.0	3.8	1	
51	10.00	-0.1	-0.0	4.8	1	
51	0.00	-0.0	-0.0	-0.0	2	
51	4.74	-0.0	-0.0	-0.0	2	
51	10.00	-0.0	-0.0	-0.0	2	
51	0.00	-0.0	-98.6	0.0	3	
51	4.74	-0.0	-109.3	0.0	3	
51	10.00	-0.0	-117.9	0.1	3	
51	0.00	-0.2	-147.9	3.6		1
51	4.74	-0.2	-164.0	5.0		1
51	10.00	-0.2	-176.9	6.4		1
51	0.00	-0.1	-98.6	2.8		2
51	4.74	-0.1	-109.3	3.9		2
51	10.00	-0.1	-117.9	4.9		2
51	0.00	-0.1	-49.3	2.8		3
51	4.74	-0.1	-54.7	3.8		3
51	10.00	-0.1	-59.0	4.9		3
51	0.00	-0.1	-29.6	2.8		4
51	4.74	-0.1	-32.8	3.8		4
51	10.00	-0.1	-35.4	4.9		4
52	0.00	-0.1	-0.0	-0.7	1	
52	4.74	-0.1	-0.0	1.0	1	
52	10.00	-0.1	-0.0	2.8	1	
52	0.00	-0.0	-0.0	-0.0	2	
52	4.74	-0.0	-0.0	-0.0	2	
52	10.00	-0.0	-0.0	-0.0	2	
52	0.00	-0.0	-67.0	0.0	3	
52	4.74	-0.0	-83.6	0.0	3	
52	10.00	-0.0	-98.7	0.0	3	
52	0.00	-0.2	-100.6	-0.9		1
52	4.74	-0.2	-125.4	1.3		1
52	10.00	-0.2	-148.0	3.6		1
52	0.00	-0.1	-67.1	-0.7		2
52	4.74	-0.1	-83.6	1.0		2
52	10.00	-0.1	-98.7	2.8		2
52	0.00	-0.1	-33.5	-0.7		3
52	4.74	-0.1	-41.8	1.0		3
52	10.00	-0.1	-49.4	2.8		3
52	0.00	-0.1	-20.1	-0.7		4
52	4.74	-0.1	-25.1	1.0		4
52	10.00	-0.1	-29.6	2.8		4
53	0.00	-0.1	-0.0	-5.6	1	
53	4.74	-0.1	-0.0	-3.2	1	
53	10.00	-0.1	-0.0	-0.7	1	
53	0.00	-0.0	-0.0	-0.0	2	
53	4.74	-0.0	-0.0	-0.0	2	
53	10.00	-0.0	-0.0	-0.0	2	
53	0.00	-0.0	-23.2	-0.0	3	
53	4.74	-0.0	-45.5	-0.0	3	
53	10.00	-0.0	-67.1	0.0	3	
53	0.00	-0.2	-34.8	-7.3		1
53	4.74	-0.2	-68.3	-4.2		1
53	10.00	-0.2	-100.7	-0.9		1
53	0.00	-0.1	-23.2	-5.6		2
53	4.74	-0.1	-45.6	-3.2		2
53	10.00	-0.1	-67.1	-0.7		2
53	0.00	-0.1	-11.6	-5.6		3
53	4.74	-0.1	-22.8	-3.2		3
53	10.00	-0.1	-33.6	-0.7		3
53	0.00	-0.1	-7.0	-5.6		4
53	4.74	-0.1	-13.7	-3.2		4
53	10.00	-0.1	-20.2	-0.7		4
54	0.00	-0.1	-0.0	-11.5	1	
54	4.74	-0.1	-0.0	-8.6	1	
54	10.00	-0.1	-0.0	-5.6	1	
54	0.00	-0.0	-0.0	-0.0	2	
54	4.74	-0.0	-0.0	-0.0	2	
54	10.00	-0.0	-0.0	-0.0	2	
54	0.00	-0.0	33.0	-0.0	3	
54	4.74	-0.0	4.8	-0.0	3	
54	10.00	-0.0	-23.3	-0.0	3	
54	0.00	-0.2	49.5	-14.9		1
54	4.74	-0.2	7.2	-11.2		1
54	10.00	-0.2	-34.9	-7.3		1
54	0.00	-0.1	33.0	-11.5		2
54	4.74	-0.1	4.8	-8.6		2
54	10.00	-0.1	-23.3	-5.6		2
54	0.00	-0.1	16.5	-11.5		3
54	4.74	-0.1	2.4	-8.6		3
54	10.00	-0.1	-11.6	-5.6		3
54	0.00	-0.1	9.9	-11.5		4
54	4.74	-0.1	1.4	-8.6		4
54	10.00	-0.1	-7.0	-5.6		4
55	0.00	0.2	0.0	0.5	1	

55	4.74	0.2	0.0	-2.1	1	
55	10.00	0.2	0.0	-6.3	1	
55	0.00	-0.0	-0.0	-0.0	2	
55	4.74	-0.0	-0.0	-0.0	2	
55	10.00	-0.0	-0.0	-0.0	2	
55	0.00	0.3	13.3	0.0	3	
55	4.74	0.3	16.8	0.1	3	
55	10.00	0.3	20.6	0.1	3	
55	0.00	0.8	20.0	0.7		1
55	4.74	0.8	25.2	-2.6		1
55	10.00	0.8	31.0	-8.0		1
55	0.00	0.6	13.3	0.5		2
55	4.74	0.6	16.8	-2.0		2
55	10.00	0.6	20.6	-6.2		2
55	0.00	0.4	6.7	0.5		3
55	4.74	0.4	8.4	-2.1		3
55	10.00	0.4	10.3	-6.2		3
55	0.00	0.3	4.0	0.5		4
55	4.74	0.3	5.0	-2.1		4
55	10.00	0.3	6.2	-6.2		4
56	0.00	0.2	0.0	-0.2	1	
56	4.74	0.2	0.0	0.6	1	
56	10.00	0.2	0.0	0.3	1	
56	0.00	-0.0	-0.0	-0.0	2	
56	4.74	-0.0	-0.0	-0.0	2	
56	10.00	-0.0	-0.0	-0.0	2	
56	0.00	0.3	6.6	0.0	3	
56	4.74	0.3	9.8	0.0	3	
56	10.00	0.3	13.4	0.0	3	
56	0.00	0.8	9.9	-0.2		1
56	4.74	0.8	14.7	0.8		1
56	10.00	0.8	20.1	0.4		1
56	0.00	0.6	6.6	-0.1		2
56	4.74	0.6	9.8	0.6		2
56	10.00	0.6	13.4	0.3		2
56	0.00	0.4	3.3	-0.2		3
56	4.74	0.4	4.9	0.6		3
56	10.00	0.4	6.7	0.3		3
56	0.00	0.3	2.0	-0.2		4
56	4.74	0.3	3.0	0.6		4
56	10.00	0.3	4.0	0.3		4
57	0.00	0.2	0.0	0.2	1	
57	4.74	0.2	0.0	0.5	1	
57	10.00	0.2	0.0	-0.4	1	
57	0.00	-0.0	-0.0	-0.0	2	
57	4.74	-0.0	-0.0	-0.0	2	
57	10.00	-0.0	-0.0	-0.0	2	
57	0.00	0.3	0.3	0.0	3	
57	4.74	0.3	3.3	0.0	3	
57	10.00	0.3	6.7	0.0	3	
57	0.00	0.8	0.4	0.3		1
57	4.74	0.8	5.0	0.7		1
57	10.00	0.8	10.1	-0.5		1
57	0.00	0.6	0.3	0.3		2
57	4.74	0.6	3.3	0.5		2
57	10.00	0.6	6.7	-0.4		2
57	0.00	0.4	0.1	0.3		3
57	4.74	0.4	1.7	0.5		3
57	10.00	0.4	3.4	-0.4		3
57	0.00	0.3	0.1	0.3		4
57	4.74	0.3	1.0	0.5		4
57	10.00	0.3	2.0	-0.4		4
58	0.00	0.2	-0.0	0.7	1	
58	4.74	0.2	-0.0	1.0	1	
58	10.00	0.2	0.0	0.0	1	
58	0.00	-0.0	-0.0	-0.0	2	
58	4.74	-0.0	-0.0	-0.0	2	
58	10.00	-0.0	-0.0	-0.0	2	
58	0.00	0.3	-5.7	0.0	3	
58	4.74	0.3	-2.8	0.0	3	
58	10.00	0.3	0.4	0.0	3	
58	0.00	0.8	-8.6	0.9		1
58	4.74	0.8	-4.2	1.3		1
58	10.00	0.8	0.6	0.1		1
58	0.00	0.6	-5.7	0.7		2
58	4.74	0.6	-2.8	1.0		2
58	10.00	0.6	0.4	0.1		2
58	0.00	0.4	-2.9	0.7		3
58	4.74	0.4	-1.4	1.0		3
58	10.00	0.4	0.2	0.1		3
58	0.00	0.3	-1.7	0.7		4
58	4.74	0.3	-0.8	1.0		4
58	10.00	0.3	0.1	0.0		4
59	0.00	0.2	-0.0	0.8	1	
59	4.74	0.2	-0.0	1.2	1	
59	10.00	0.2	-0.0	0.6	1	
59	0.00	-0.0	-0.0	-0.0	2	
59	4.74	-0.0	-0.0	-0.0	2	
59	10.00	-0.0	-0.0	-0.0	2	
59	0.00	0.3	-11.4	0.0	3	
59	4.74	0.3	-8.6	0.0	3	
59	10.00	0.3	-5.5	0.0	3	
59	0.00	0.8	-17.0	1.0		1
59	4.74	0.8	-12.9	1.6		1
59	10.00	0.8	-8.3	0.8		1
59	0.00	0.6	-11.4	0.8		2
59	4.74	0.6	-8.6	1.3		2
59	10.00	0.6	-5.5	0.6		2
59	0.00	0.4	-5.7	0.8		3
59	4.74	0.4	-4.3	1.3		3
59	10.00	0.4	-2.8	0.6		3
59	0.00	0.3	-3.4	0.8		4
59	4.74	0.3	-2.6	1.3		4
59	10.00	0.3	-1.7	0.6		4
60	0.00	0.2	-0.0	0.5	1	
60	4.74	0.2	-0.0	1.2	1	
60	10.00	0.2	-0.0	0.8	1	
60	0.00	-0.0	-0.0	-0.0	2	
60	4.74	-0.0	-0.0	-0.0	2	
60	10.00	-0.0	-0.0	-0.0	2	
60	0.00	0.3	-16.7	0.0	3	
60	4.74	0.3	-14.1	0.0	3	
60	10.00	0.3	-11.1	0.0	3	
60	0.00	0.8	-25.1	0.7		1
60	4.74	0.8	-21.1	1.6		1
60	10.00	0.8	-16.7	1.0		1
60	0.00	0.6	-16.7	0.5		2
60	4.74	0.6	-14.1	1.2		2

60	10.00	0.6	-11.1	0.8		2
60	0.00	0.4	-8.4	0.5		3
60	4.74	0.4	-7.0	1.2		3
60	10.00	0.4	-5.6	0.8		3
60	0.00	0.3	-5.0	0.5		4
60	4.74	0.3	-4.2	1.2		4
60	10.00	0.3	-3.3	0.8		4
61	0.00	0.2	-0.0	-0.0	1	
61	4.74	0.2	-0.0	0.9	1	
61	10.00	0.2	-0.0	0.7	1	
61	0.00	-0.0	-0.0	-0.0	2	
61	4.74	-0.0	-0.0	-0.0	2	
61	10.00	-0.0	-0.0	-0.0	2	
61	0.00	0.3	-21.7	-0.0	3	
61	4.74	0.3	-19.2	0.0	3	
61	10.00	0.3	-16.4	0.0	3	
61	0.00	0.8	-32.6	-0.0		1
61	4.74	0.8	-28.8	1.2		1
61	10.00	0.8	-24.6	0.9		1
61	0.00	0.6	-21.7	-0.0		2
61	4.74	0.6	-19.2	0.9		2
61	10.00	0.6	-16.4	0.7		2
61	0.00	0.4	-10.9	-0.0		3
61	4.74	0.4	-9.6	0.9		3
61	10.00	0.4	-8.2	0.7		3
61	0.00	0.3	-6.5	-0.0		4
61	4.74	0.3	-5.8	0.9		4
61	10.00	0.3	-4.9	0.7		4
62	0.00	0.2	-0.0	-0.5	1	
62	4.74	0.2	-0.0	0.4	1	
62	10.00	0.2	-0.0	0.2	1	
62	0.00	-0.0	-0.0	-0.0	2	
62	4.74	-0.0	-0.0	-0.0	2	
62	10.00	-0.0	-0.0	-0.0	2	
62	0.00	0.3	-26.4	0.0	3	
62	4.74	0.3	-24.1	0.0	3	
62	10.00	0.3	-21.4	0.0	3	
62	0.00	0.8	-39.7	-0.6		1
62	4.74	0.8	-36.1	0.6		1
62	10.00	0.8	-32.2	0.3		1
62	0.00	0.6	-26.5	-0.5		2
62	4.74	0.6	-24.1	0.4		2
62	10.00	0.6	-21.4	0.2		2
62	0.00	0.4	-13.2	-0.5		3
62	4.74	0.4	-12.0	0.4		3
62	10.00	0.4	-10.7	0.2		3
62	0.00	0.3	-7.9	-0.5		4
62	4.74	0.3	-7.2	0.4		4
62	10.00	0.3	-6.4	0.2		4
63	0.00	0.2	-0.0	0.2	1	
63	4.74	0.2	-0.0	0.6	1	
63	10.00	0.2	-0.0	-0.2	1	
63	0.00	-0.0	-0.0	-0.0	2	
63	4.74	-0.0	-0.0	-0.0	2	
63	10.00	-0.0	-0.0	-0.0	2	
63	0.00	0.3	-30.8	0.0	3	
63	4.74	0.3	-28.6	0.0	3	
63	10.00	0.3	-26.1	0.0	3	
63	0.00	0.8	-46.2	0.3		1
63	4.74	0.8	-42.9	0.8		1
63	10.00	0.8	-39.2	-0.3		1
63	0.00	0.6	-30.8	0.2		2
63	4.74	0.6	-28.6	0.6		2
63	10.00	0.6	-26.1	-0.2		2
63	0.00	0.4	-15.4	0.2		3
63	4.74	0.4	-14.3	0.6		3
63	10.00	0.4	-13.1	-0.2		3
63	0.00	0.3	-9.3	0.2		4
63	4.74	0.3	-8.6	0.6		4
63	10.00	0.3	-7.8	-0.2		4
64	0.00	0.2	-0.0	-6.1	1	
64	4.74	0.2	-0.0	-2.4	1	
64	10.00	0.2	-0.0	0.4	1	
64	0.00	-0.0	-0.0	-0.0	2	
64	4.74	-0.0	-0.0	-0.0	2	
64	10.00	-0.0	-0.0	-0.0	2	
64	0.00	0.3	-34.7	-0.4	3	
64	4.74	0.3	-32.7	-0.2	3	
64	10.00	0.3	-30.4	0.0	3	
64	0.00	0.8	-52.1	-8.5		1
64	4.74	0.8	-49.0	-3.4		1
64	10.00	0.8	-45.7	0.6		1
64	0.00	0.6	-34.7	-6.5		2
64	4.74	0.6	-32.7	-2.6		2
64	10.00	0.6	-30.5	0.5		2
64	0.00	0.4	-17.4	-6.3		3
64	4.74	0.4	-16.4	-2.5		3
64	10.00	0.4	-15.2	0.5		3
64	0.00	0.3	-10.4	-6.2		4
64	4.74	0.3	-9.8	-2.5		4
64	10.00	0.3	-9.1	0.4		4
66	0.00	0.0	-0.0	0.0	1	
66	1.89	0.0	-0.0	-2.9	1	
66	4.00	0.0	-0.0	-6.1	1	
66	0.00	-0.0	-0.0	-0.0	2	
66	1.89	-0.0	-0.0	-0.0	2	
66	4.00	-0.0	-0.0	-0.0	2	
66	0.00	15.5	-8.9	-1181.4	3	
66	1.89	15.5	-8.9	-1181.4	3	
66	4.00	15.5	-8.9	-1181.4	3	
66	0.00	23.3	-13.3	-1772.2		1
66	1.89	23.3	-13.3	-1775.9		1
66	4.00	23.3	-13.3	-1780.0		1
66	0.00	15.5	-8.9	-1181.4		2
66	1.89	15.5	-8.9	-1184.3		2
66	4.00	15.5	-8.9	-1187.5		2
66	0.00	7.8	-4.4	-590.7		3
66	1.89	7.8	-4.5	-593.6		3
66	4.00	7.8	-4.5	-596.8		3
66	0.00	4.7	-2.7	-354.4		4
66	1.89	4.7	-2.7	-357.3		4
66	4.00	4.7	-2.7	-360.5		4
69	0.00	0.0	0.0	0.0	1	
69	1.89	0.0	0.0	-2.9	1	
69	4.00	0.0	0.0	-6.1	1	
69	0.00	-0.0	-0.0	-0.0	2	
69	1.89	-0.0	-0.0	-0.0	2	
69	4.00	-0.0	-0.0	-0.0	2	

69	0.00	15.5	8.9	-1181.4	3	
69	1.89	15.5	8.9	-1181.4	3	
69	4.00	15.5	8.9	-1181.4	3	
69	0.00	23.3	13.3	-1772.2		1
69	1.89	23.3	13.3	-1775.9		1
69	4.00	23.3	13.3	-1780.0		1
69	0.00	15.5	8.9	-1181.4		2
69	1.89	15.5	8.9	-1184.3		2
69	4.00	15.5	8.9	-1187.5		2
69	0.00	7.8	4.4	-590.7		3
69	1.89	7.8	4.5	-593.6		3
69	4.00	7.8	4.5	-596.8		3
69	0.00	4.7	2.7	-354.4		4
69	1.89	4.7	2.7	-357.3		4
69	4.00	4.7	2.7	-360.5		4
71	0.00	0.2	-0.0	-6.7	1	
71	4.74	0.2	-0.0	-2.7	1	
71	10.00	0.2	-0.0	0.6	1	
71	0.00	-0.0	-0.0	-0.0	2	
71	4.74	-0.0	-0.0	-0.0	2	
71	10.00	-0.0	-0.0	-0.0	2	
71	0.00	0.4	-4.8	-0.1	3	
71	4.74	0.4	-5.5	-0.0	3	
71	10.00	0.4	-6.3	0.0	3	
71	0.00	0.8	-7.1	-8.8		1
71	4.74	0.8	-8.3	-3.5		1
71	10.00	0.8	-9.5	0.7		1
71	0.00	0.6	-4.8	-6.7		2
71	4.74	0.6	-5.5	-2.7		2
71	10.00	0.6	-6.3	0.6		2
71	0.00	0.4	-2.4	-6.7		3
71	4.74	0.4	-2.8	-2.7		3
71	10.00	0.4	-3.2	0.6		3
71	0.00	0.3	-1.4	-6.7		4
71	4.74	0.3	-1.7	-2.7		4
71	10.00	0.3	-1.9	0.6		4
72	0.00	0.2	-0.0	0.3	1	
72	4.74	0.2	-0.0	0.7	1	
72	10.00	0.2	-0.0	-0.1	1	
72	0.00	-0.0	-0.0	-0.0	2	
72	4.74	-0.0	-0.0	-0.0	2	
72	10.00	-0.0	-0.0	-0.0	2	
72	0.00	0.4	-6.4	0.0	3	
72	4.74	0.4	-7.0	0.0	3	
72	10.00	0.4	-7.5	0.0	3	
72	0.00	0.8	-9.7	0.4		1
72	4.74	0.8	-10.4	0.9		1
72	10.00	0.8	-11.3	-0.2		1
72	0.00	0.6	-6.4	0.3		2
72	4.74	0.6	-7.0	0.7		2
72	10.00	0.6	-7.5	-0.1		2
72	0.00	0.4	-3.2	0.3		3
72	4.74	0.4	-3.5	0.7		3
72	10.00	0.4	-3.8	-0.1		3
72	0.00	0.3	-1.9	0.3		4
72	4.74	0.3	-2.1	0.7		4
72	10.00	0.3	-2.3	-0.1		4
73	0.00	0.2	-0.0	-0.4	1	
73	4.74	0.2	-0.0	0.5	1	
73	10.00	0.2	-0.0	0.3	1	
73	0.00	-0.0	-0.0	-0.0	2	
73	4.74	-0.0	-0.0	-0.0	2	
73	10.00	-0.0	-0.0	-0.0	2	
73	0.00	0.4	-7.6	0.0	3	
73	4.74	0.4	-8.0	0.0	3	
73	10.00	0.4	-8.4	0.0	3	
73	0.00	0.8	-11.4	-0.5		1
73	4.74	0.8	-12.0	0.7		1
73	10.00	0.8	-12.5	0.4		1
73	0.00	0.6	-7.6	-0.4		2
73	4.74	0.6	-8.0	0.5		2
73	10.00	0.6	-8.4	0.3		2
73	0.00	0.4	-3.8	-0.4		3
73	4.74	0.4	-4.0	0.5		3
73	10.00	0.4	-4.2	0.3		3
73	0.00	0.3	-2.3	-0.4		4
73	4.74	0.3	-2.4	0.5		4
73	10.00	0.3	-2.5	0.3		4
74	0.00	0.2	-0.0	0.0	1	
74	4.74	0.2	-0.0	0.9	1	
74	10.00	0.2	-0.0	0.7	1	
74	0.00	-0.0	-0.0	-0.0	2	
74	4.74	-0.0	-0.0	-0.0	2	
74	10.00	-0.0	-0.0	-0.0	2	
74	0.00	0.4	-8.4	0.0	3	
74	4.74	0.4	-8.6	0.0	3	
74	10.00	0.4	-8.8	0.0	3	
74	0.00	0.8	-12.6	0.1		1
74	4.74	0.8	-12.9	1.2		1
74	10.00	0.8	-13.2	0.9		1
74	0.00	0.6	-8.4	0.1		2
74	4.74	0.6	-8.6	1.0		2
74	10.00	0.6	-8.8	0.7		2
74	0.00	0.4	-4.2	0.0		3
74	4.74	0.4	-4.3	0.9		3
74	10.00	0.4	-4.4	0.7		3
74	0.00	0.3	-2.5	0.0		4
74	4.74	0.3	-2.6	0.9		4
74	10.00	0.3	-2.7	0.7		4
75	0.00	0.2	-0.0	0.6	1	
75	4.74	0.2	-0.0	1.3	1	
75	10.00	0.2	-0.0	0.8	1	
75	0.00	-0.0	-0.0	-0.0	2	
75	4.74	-0.0	-0.0	-0.0	2	
75	10.00	-0.0	-0.0	-0.0	2	
75	0.00	0.4	-8.9	0.0	3	
75	4.74	0.4	-8.9	0.0	3	
75	10.00	0.4	-9.0	0.0	3	
75	0.00	0.8	-13.3	0.8		1
75	4.74	0.8	-13.4	1.7		1
75	10.00	0.8	-13.5	1.0		1
75	0.00	0.6	-8.9	0.6		2
75	4.74	0.6	-8.9	1.3		2
75	10.00	0.6	-9.0	0.8		2
75	0.00	0.4	-4.4	0.6		3
75	4.74	0.4	-4.5	1.3		3
75	10.00	0.4	-4.5	0.8		3
75	0.00	0.3	-2.7	0.6		4

75	4.74	0.3	-2.7	1.3		4
75	10.00	0.3	-2.7	0.8		4
76	0.00	0.2	-0.0	0.8	1	
76	4.74	0.2	-0.0	1.3	1	
76	10.00	0.2	-0.0	0.6	1	
76	0.00	-0.0	-0.0	-0.0	2	
76	4.74	-0.0	-0.0	-0.0	2	
76	10.00	-0.0	-0.0	-0.0	2	
76	0.00	0.4	-9.0	0.0	3	
76	4.74	0.4	-8.9	0.0	3	
76	10.00	0.4	-8.9	0.0	3	
76	0.00	0.8	-13.5	1.0		1
76	4.74	0.8	-13.4	1.7		1
76	10.00	0.8	-13.3	0.8		1
76	0.00	0.6	-9.0	0.8		2
76	4.74	0.6	-8.9	1.3		2
76	10.00	0.6	-8.9	0.6		2
76	0.00	0.4	-4.5	0.8		3
76	4.74	0.4	-4.5	1.3		3
76	10.00	0.4	-4.4	0.6		3
76	0.00	0.3	-2.7	0.8		4
76	4.74	0.3	-2.7	1.3		4
76	10.00	0.3	-2.7	0.6		4
77	0.00	0.2	-0.0	0.7	1	
77	4.74	0.2	-0.0	1.0	1	
77	10.00	0.2	-0.0	0.0	1	
77	0.00	-0.0	-0.0	-0.0	2	
77	4.74	-0.0	-0.0	-0.0	2	
77	10.00	-0.0	-0.0	-0.0	2	
77	0.00	0.4	-8.8	0.0	3	
77	4.74	0.4	-8.6	0.0	3	
77	10.00	0.4	-8.4	0.0	3	
77	0.00	0.8	-13.2	0.9		1
77	4.74	0.8	-13.0	1.3		1
77	10.00	0.8	-12.6	0.1		1
77	0.00	0.6	-8.8	0.7		2
77	4.74	0.6	-8.6	1.0		2
77	10.00	0.6	-8.4	0.1		2
77	0.00	0.4	-4.4	0.7		3
77	4.74	0.4	-4.3	1.0		3
77	10.00	0.4	-4.2	0.0		3
77	0.00	0.3	-2.7	0.7		4
77	4.74	0.3	-2.6	1.0		4
77	10.00	0.3	-2.5	0.0		4
78	0.00	0.2	-0.0	0.3	1	
78	4.74	0.2	-0.0	0.5	1	
78	10.00	0.2	-0.0	-0.4	1	
78	0.00	-0.0	-0.0	-0.0	2	
78	4.74	-0.0	-0.0	-0.0	2	
78	10.00	-0.0	-0.0	-0.0	2	
78	0.00	0.4	-8.4	0.0	3	
78	4.74	0.4	-8.0	0.0	3	
78	10.00	0.4	-7.6	0.0	3	
78	0.00	0.8	-12.5	0.4		1
78	4.74	0.8	-12.0	0.7		1
78	10.00	0.8	-11.4	-0.5		1
78	0.00	0.6	-8.4	0.3		2
78	4.74	0.6	-8.0	0.6		2
78	10.00	0.6	-7.6	-0.4		2
78	0.00	0.4	-4.2	0.3		3
78	4.74	0.4	-4.0	0.5		3
78	10.00	0.4	-3.8	-0.4		3
78	0.00	0.3	-2.5	0.3		4
78	4.74	0.3	-2.4	0.5		4
78	10.00	0.3	-2.3	-0.4		4
79	0.00	0.2	-0.0	-0.1	1	
79	4.74	0.2	-0.0	0.6	1	
79	10.00	0.2	-0.0	0.3	1	
79	0.00	-0.0	-0.0	-0.0	2	
79	4.74	-0.0	-0.0	-0.0	2	
79	10.00	-0.0	-0.0	-0.0	2	
79	0.00	0.4	-7.5	0.0	3	
79	4.74	0.4	-7.0	0.0	3	
79	10.00	0.4	-6.4	0.0	3	
79	0.00	0.8	-11.3	-0.2		1
79	4.74	0.8	-10.5	0.9		1
79	10.00	0.8	-9.7	0.4		1
79	0.00	0.6	-7.5	-0.1		2
79	4.74	0.6	-7.0	0.7		2
79	10.00	0.6	-6.4	0.3		2
79	0.00	0.4	-3.8	-0.1		3
79	4.74	0.4	-3.5	0.7		3
79	10.00	0.4	-3.2	0.3		3
79	0.00	0.3	-2.3	-0.1		4
79	4.74	0.3	-2.1	0.7		4
79	10.00	0.3	-1.9	0.3		4
80	0.00	0.2	-0.0	0.6	1	
80	4.74	0.2	-0.0	-2.3	1	
80	10.00	0.2	-0.0	-6.7	1	
80	0.00	-0.0	-0.0	-0.0	2	
80	4.74	-0.0	-0.0	-0.0	2	
80	10.00	-0.0	-0.0	-0.0	2	
80	0.00	0.4	-6.3	0.0	3	
80	4.74	0.4	-5.6	-0.0	3	
80	10.00	0.4	-4.8	-0.1	3	
80	0.00	0.8	-9.5	0.7		1
80	4.74	0.8	-8.4	-3.0		1
80	10.00	0.8	-7.1	-8.8		1
80	0.00	0.6	-6.3	0.6		2
80	4.74	0.6	-5.6	-2.3		2
80	10.00	0.6	-4.8	-6.7		2
80	0.00	0.4	-3.2	0.6		3
80	4.74	0.4	-2.8	-2.3		3
80	10.00	0.4	-2.4	-6.7		3
80	0.00	0.3	-1.9	0.6		4
80	4.74	0.3	-1.7	-2.3		4
80	10.00	0.3	-1.4	-6.7		4
81	0.00	-0.1	-0.0	-11.0	1	
81	4.74	-0.1	-0.0	-8.2	1	
81	10.00	-0.1	-0.0	-5.2	1	
81	0.00	-0.0	-0.0	-0.0	2	
81	4.74	-0.0	-0.0	-0.0	2	
81	10.00	-0.0	-0.0	-0.0	2	
81	0.00	-0.0	43.9	0.0	3	
81	4.74	-0.0	16.1	0.0	3	
81	10.00	-0.0	-11.5	0.0	3	
81	0.00	-0.2	65.9	-14.2		1
81	4.74	-0.2	24.1	-10.5		1

81	10.00	-0.2	-17.3	-6.7		1
81	0.00	-0.1	43.9	-10.9		2
81	4.74	-0.1	16.1	-8.1		2
81	10.00	-0.1	-11.5	-5.1		2
81	0.00	-0.1	22.0	-10.9		3
81	4.74	-0.1	8.0	-8.1		3
81	10.00	-0.1	-5.8	-5.2		3
81	0.00	-0.1	13.2	-11.0		4
81	4.74	-0.1	4.8	-8.1		4
81	10.00	-0.1	-3.5	-5.2		4
82	0.00	-0.1	-0.0	-5.2	1	
82	4.74	-0.1	-0.0	-2.8	1	
82	10.00	-0.1	-0.0	-0.3	1	
82	0.00	-0.0	-0.0	-0.0	2	
82	4.74	-0.0	-0.0	-0.0	2	
82	10.00	-0.0	-0.0	-0.0	2	
82	0.00	-0.0	-11.5	0.0	3	
82	4.74	-0.0	-33.5	0.0	3	
82	10.00	-0.0	-54.7	0.0	3	
82	0.00	-0.2	-17.3	-6.7		1
82	4.74	-0.2	-50.3	-3.6		1
82	10.00	-0.2	-82.0	-0.4		1
82	0.00	-0.1	-11.5	-5.1		2
82	4.74	-0.1	-33.5	-2.8		2
82	10.00	-0.1	-54.7	-0.3		2
82	0.00	-0.1	-5.8	-5.2		3
82	4.74	-0.1	-16.8	-2.8		3
82	10.00	-0.1	-27.3	-0.3		3
82	0.00	-0.1	-3.5	-5.2		4
82	4.74	-0.1	-10.1	-2.8		4
82	10.00	-0.1	-16.4	-0.3		4
83	0.00	-0.1	-0.0	-0.4	1	
83	4.74	-0.1	-0.0	1.3	1	
83	10.00	-0.1	-0.0	3.1	1	
83	0.00	-0.0	-0.0	-0.0	2	
83	4.74	-0.0	-0.0	-0.0	2	
83	10.00	-0.0	-0.0	-0.0	2	
83	0.00	-0.0	-54.6	0.0	3	
83	4.74	-0.0	-70.8	0.0	3	
83	10.00	-0.0	-85.5	0.0	3	
83	0.00	-0.2	-82.0	-0.4		1
83	4.74	-0.2	-106.2	1.8		1
83	10.00	-0.2	-128.3	4.0		1
83	0.00	-0.1	-54.7	-0.3		2
83	4.74	-0.1	-70.8	1.4		2
83	10.00	-0.1	-85.5	3.1		2
83	0.00	-0.1	-27.3	-0.3		3
83	4.74	-0.1	-35.4	1.4		3
83	10.00	-0.1	-42.8	3.1		3
83	0.00	-0.1	-16.4	-0.3		4
83	4.74	-0.1	-21.2	1.3		4
83	10.00	-0.1	-25.7	3.1		4
84	0.00	-0.1	-0.0	3.0	1	
84	4.74	-0.1	-0.0	4.1	1	
84	10.00	-0.1	-0.0	5.1	1	
84	0.00	-0.0	-0.0	-0.0	2	
84	4.74	-0.0	-0.0	-0.0	2	
84	10.00	-0.0	-0.0	-0.0	2	
84	0.00	-0.0	-85.5	0.0	3	
84	4.74	-0.0	-95.8	0.0	3	
84	10.00	-0.0	-104.0	0.0	3	
84	0.00	-0.2	-128.2	4.0		1
84	4.74	-0.2	-143.7	5.4		1
84	10.00	-0.2	-156.0	6.7		1
84	0.00	-0.1	-85.5	3.1		2
84	4.74	-0.1	-95.8	4.1		2
84	10.00	-0.1	-104.0	5.1		2
84	0.00	-0.1	-42.7	3.1		3
84	4.74	-0.1	-47.9	4.1		3
84	10.00	-0.1	-52.0	5.1		3
84	0.00	-0.1	-25.7	3.1		4
84	4.74	-0.1	-28.7	4.1		4
84	10.00	-0.1	-31.2	5.1		4
85	0.00	-0.1	-0.0	5.1	1	
85	4.74	-0.1	-0.0	5.5	1	
85	10.00	-0.1	-0.0	5.7	1	
85	0.00	-0.0	-0.0	-0.0	2	
85	4.74	-0.0	-0.0	-0.0	2	
85	10.00	-0.0	-0.0	-0.0	2	
85	0.00	-0.0	-104.0	0.0	3	
85	4.74	-0.0	-108.5	0.0	3	
85	10.00	-0.0	-110.2	0.0	3	
85	0.00	-0.2	-156.0	6.7		1
85	4.74	-0.2	-162.7	7.2		1
85	10.00	-0.2	-165.2	7.5		1
85	0.00	-0.1	-104.0	5.1		2
85	4.74	-0.1	-108.5	5.5		2
85	10.00	-0.1	-110.2	5.8		2
85	0.00	-0.1	-52.0	5.1		3
85	4.74	-0.1	-54.2	5.5		3
85	10.00	-0.1	-55.1	5.8		3
85	0.00	-0.1	-31.2	5.1		4
85	4.74	-0.1	-32.5	5.5		4
85	10.00	-0.1	-33.1	5.8		4
86	0.00	-0.1	-0.0	5.7	1	
86	4.74	-0.1	-0.0	5.5	1	
86	10.00	-0.1	-0.0	5.1	1	
86	0.00	-0.0	-0.0	-0.0	2	
86	4.74	-0.0	-0.0	-0.0	2	
86	10.00	-0.0	-0.0	-0.0	2	
86	0.00	-0.0	-110.2	0.0	3	
86	4.74	-0.0	-108.8	0.0	3	
86	10.00	-0.0	-104.0	0.0	3	
86	0.00	-0.2	-165.2	7.5		1
86	4.74	-0.2	-163.2	7.2		1
86	10.00	-0.2	-156.0	6.7		1
86	0.00	-0.1	-110.2	5.8		2
86	4.74	-0.1	-108.8	5.5		2
86	10.00	-0.1	-104.0	5.1		2
86	0.00	-0.1	-55.1	5.8		3
86	4.74	-0.1	-54.4	5.5		3
86	10.00	-0.1	-52.0	5.1		3
86	0.00	-0.1	-33.1	5.8		4
86	4.74	-0.1	-32.6	5.5		4
86	10.00	-0.1	-31.2	5.1		4
87	0.00	-0.1	-0.0	5.1	1	
87	4.74	-0.1	-0.0	4.2	1	
87	10.00	-0.1	-0.0	3.0	1	

87	0.00	-0.0	-0.0	-0.0	2	
87	4.74	-0.0	-0.0	-0.0	2	
87	10.00	-0.0	-0.0	-0.0	2	
87	0.00	-0.0	-104.0	0.0	3	
87	4.74	-0.0	-96.8	0.0	3	
87	10.00	-0.0	-85.5	0.0	3	
87	0.00	-0.2	-156.0	6.7		1
87	4.74	-0.2	-145.2	5.5		1
87	10.00	-0.2	-128.2	4.0		1
87	0.00	-0.1	-104.0	5.1		2
87	4.74	-0.1	-96.8	4.2		2
87	10.00	-0.1	-85.5	3.1		2
87	0.00	-0.1	-52.0	5.1		3
87	4.74	-0.1	-48.4	4.2		3
87	10.00	-0.1	-42.7	3.1		3
87	0.00	-0.1	-31.2	5.1		4
87	4.74	-0.1	-29.0	4.2		4
87	10.00	-0.1	-25.7	3.1		4
88	0.00	-0.1	-0.0	3.1	1	
88	4.74	-0.1	-0.0	1.5	1	
88	10.00	-0.1	-0.0	-0.4	1	
88	0.00	-0.0	-0.0	-0.0	2	
88	4.74	-0.0	-0.0	-0.0	2	
88	10.00	-0.0	-0.0	-0.0	2	
88	0.00	-0.0	-85.5	0.0	3	
88	4.74	-0.0	-72.4	0.0	3	
88	10.00	-0.0	-54.6	0.0	3	
88	0.00	-0.2	-128.3	4.0		1
88	4.74	-0.2	-108.7	2.0		1
88	10.00	-0.2	-82.0	-0.4		1
88	0.00	-0.1	-85.5	3.1		2
88	4.74	-0.1	-72.4	1.6		2
88	10.00	-0.1	-54.7	-0.3		2
88	0.00	-0.1	-42.8	3.1		3
88	4.74	-0.1	-36.2	1.5		3
88	10.00	-0.1	-27.3	-0.3		3
88	0.00	-0.1	-25.7	3.1		4
88	4.74	-0.1	-21.7	1.5		4
88	10.00	-0.1	-16.4	-0.3		4
89	0.00	-0.1	-0.0	-0.3	1	
89	4.74	-0.1	-0.0	-2.6	1	
89	10.00	-0.1	-0.0	-5.2	1	
89	0.00	-0.0	-0.0	-0.0	2	
89	4.74	-0.0	-0.0	-0.0	2	
89	10.00	-0.0	-0.0	-0.0	2	
89	0.00	-0.0	-54.7	0.0	3	
89	4.74	-0.0	-35.8	0.0	3	
89	10.00	-0.0	-11.5	0.0	3	
89	0.00	-0.2	-82.0	-0.4		1
89	4.74	-0.2	-53.7	-3.3		1
89	10.00	-0.2	-17.3	-6.7		1
89	0.00	-0.1	-54.7	-0.3		2
89	4.74	-0.1	-35.8	-2.5		2
89	10.00	-0.1	-11.5	-5.1		2
89	0.00	-0.1	-27.3	-0.3		3
89	4.74	-0.1	-17.9	-2.5		3
89	10.00	-0.1	-5.8	-5.2		3
89	0.00	-0.1	-16.4	-0.3		4
89	4.74	-0.1	-10.7	-2.6		4
89	10.00	-0.1	-3.5	-5.2		4
90	0.00	-0.1	-0.0	-5.2	1	
90	4.74	-0.1	-0.0	-7.9	1	
90	10.00	-0.1	-0.0	-11.0	1	
90	0.00	-0.0	-0.0	-0.0	2	
90	4.74	-0.0	-0.0	-0.0	2	
90	10.00	-0.0	-0.0	-0.0	2	
90	0.00	-0.0	-11.5	0.0	3	
90	4.74	-0.0	13.2	0.0	3	
90	10.00	-0.0	43.9	0.0	3	
90	0.00	-0.2	-17.3	-6.7		1
90	4.74	-0.2	19.8	-10.1		1
90	10.00	-0.2	65.9	-14.2		1
90	0.00	-0.1	-11.5	-5.1		2
90	4.74	-0.1	13.2	-7.8		2
90	10.00	-0.1	43.9	-10.9		2
90	0.00	-0.1	-5.8	-5.2		3
90	4.74	-0.1	6.6	-7.8		3
90	10.00	-0.1	22.0	-10.9		3
90	0.00	-0.1	-3.5	-5.2		4
90	4.74	-0.1	3.9	-7.8		4
90	10.00	-0.1	13.2	-11.0		4
109	0.00	-0.1	-0.0	-5.6	1	
109	4.74	-0.1	-0.0	-8.3	1	
109	10.00	-0.1	-0.0	-11.5	1	
109	0.00	-0.0	-0.0	-0.0	2	
109	4.74	-0.0	-0.0	-0.0	2	
109	10.00	-0.0	-0.0	-0.0	2	
109	0.00	-0.0	-23.3	-0.0	3	
109	4.74	-0.0	1.8	-0.0	3	
109	10.00	-0.0	33.0	-0.0	3	
109	0.00	-0.2	-34.9	-7.3		1
109	4.74	-0.2	2.8	-10.8		1
109	10.00	-0.2	49.5	-14.9		1
109	0.00	-0.1	-23.3	-5.6		2
109	4.74	-0.1	1.8	-8.3		2
109	10.00	-0.1	33.0	-11.5		2
109	0.00	-0.1	-11.6	-5.6		3
109	4.74	-0.1	0.9	-8.3		3
109	10.00	-0.1	16.5	-11.5		3
109	0.00	-0.1	-7.0	-5.6		4
109	4.74	-0.1	0.5	-8.3		4
109	10.00	-0.1	9.9	-11.5		4
110	0.00	-0.1	-0.0	-0.7	1	
110	4.74	-0.1	-0.0	-2.9	1	
110	10.00	-0.1	-0.0	-5.6	1	
110	0.00	-0.0	-0.0	-0.0	2	
110	4.74	-0.0	-0.0	-0.0	2	
110	10.00	-0.0	-0.0	-0.0	2	
110	0.00	-0.0	-67.1	0.0	3	
110	4.74	-0.0	-47.9	-0.0	3	
110	10.00	-0.0	-23.2	-0.0	3	
110	0.00	-0.2	-100.7	-0.9		1
110	4.74	-0.2	-71.8	-3.8		1
110	10.00	-0.2	-34.8	-7.3		1
110	0.00	-0.1	-67.1	-0.7		2
110	4.74	-0.1	-47.9	-2.9		2
110	10.00	-0.1	-23.2	-5.6		2
110	0.00	-0.1	-33.6	-0.7		3

110	4.74	-0.1	-23.9	-2.9		3
110	10.00	-0.1	-11.6	-5.6		3
110	0.00	-0.1	-20.2	-0.7		4
110	4.74	-0.1	-14.4	-2.9		4
110	10.00	-0.1	-7.0	-5.6		4
111	0.00	-0.1	-0.0	2.8	1	
111	4.74	-0.1	-0.0	1.2	1	
111	10.00	-0.1	-0.0	-0.7	1	
111	0.00	-0.0	-0.0	-0.0	2	
111	4.74	-0.0	-0.0	-0.0	2	
111	10.00	-0.0	-0.0	-0.0	2	
111	0.00	-0.0	-98.7	0.0	3	
111	4.74	-0.0	-85.2	0.0	3	
111	10.00	-0.0	-67.0	0.0	3	
111	0.00	-0.2	-148.0	3.6		1
111	4.74	-0.2	-127.9	1.6		1
111	10.00	-0.2	-100.6	-0.9		1
111	0.00	-0.1	-98.7	2.8		2
111	4.74	-0.1	-85.3	1.2		2
111	10.00	-0.1	-67.1	-0.7		2
111	0.00	-0.1	-49.4	2.8		3
111	4.74	-0.1	-42.6	1.2		3
111	10.00	-0.1	-33.5	-0.7		3
111	0.00	-0.1	-29.6	2.8		4
111	4.74	-0.1	-25.6	1.2		4
111	10.00	-0.1	-20.1	-0.7		4
112	0.00	-0.1	-0.0	4.8	1	
112	4.74	-0.1	-0.0	3.9	1	
112	10.00	-0.1	-0.0	2.8	1	
112	0.00	-0.0	-0.0	-0.0	2	
112	4.74	-0.0	-0.0	-0.0	2	
112	10.00	-0.0	-0.0	-0.0	2	
112	0.00	-0.0	-117.9	0.1	3	
112	4.74	-0.0	-110.3	0.0	3	
112	10.00	-0.0	-98.6	0.0	3	
112	0.00	-0.2	-176.9	6.4		1
112	4.74	-0.2	-165.5	5.2		1
112	10.00	-0.2	-147.9	3.6		1
112	0.00	-0.1	-117.9	4.9		2
112	4.74	-0.1	-110.3	4.0		2
112	10.00	-0.1	-98.6	2.8		2
112	0.00	-0.1	-59.0	4.9		3
112	4.74	-0.1	-55.2	3.9		3
112	10.00	-0.1	-49.3	2.8		3
112	0.00	-0.1	-35.4	4.9		4
112	4.74	-0.1	-33.1	3.9		4
112	10.00	-0.1	-29.6	2.8		4
113	0.00	-0.1	-0.0	5.6	1	
113	4.74	-0.1	-0.0	5.3	1	
113	10.00	-0.1	-0.0	4.8	1	
113	0.00	-0.0	-0.0	-0.0	2	
113	4.74	-0.0	-0.0	-0.0	2	
113	10.00	-0.0	-0.0	-0.0	2	
113	0.00	-0.0	-124.8	0.1	3	
113	4.74	-0.0	-123.0	0.1	3	
113	10.00	-0.0	-117.8	0.0	3	
113	0.00	-0.2	-187.2	7.3		1
113	4.74	-0.2	-184.6	7.0		1
113	10.00	-0.2	-176.8	6.4		1
113	0.00	-0.1	-124.8	5.6		2
113	4.74	-0.1	-123.1	5.4		2
113	10.00	-0.1	-117.9	4.9		2
113	0.00	-0.1	-62.4	5.6		3
113	4.74	-0.1	-61.5	5.3		3
113	10.00	-0.1	-58.9	4.9		3
113	0.00	-0.1	-37.5	5.6		4
113	4.74	-0.1	-36.9	5.3		4
113	10.00	-0.1	-35.4	4.9		4
114	0.00	-0.1	-0.0	4.9	1	
114	4.74	-0.1	-0.0	5.3	1	
114	10.00	-0.1	-0.0	5.6	1	
114	0.00	-0.0	-0.0	-0.0	2	
114	4.74	-0.0	-0.0	-0.0	2	
114	10.00	-0.0	-0.0	-0.0	2	
114	0.00	-0.0	-119.3	0.1	3	
114	4.74	-0.0	-123.4	0.1	3	
114	10.00	-0.0	-124.7	0.1	3	
114	0.00	-0.2	-179.0	6.6		1
114	4.74	-0.2	-185.2	7.0		1
114	10.00	-0.2	-187.1	7.3		1
114	0.00	-0.1	-119.4	5.0		2
114	4.74	-0.1	-123.5	5.4		2
114	10.00	-0.1	-124.7	5.6		2
114	0.00	-0.1	-59.7	5.0		3
114	4.74	-0.1	-61.7	5.4		3
114	10.00	-0.1	-62.4	5.6		3
114	0.00	-0.1	-35.8	5.0		4
114	4.74	-0.1	-37.0	5.3		4
114	10.00	-0.1	-37.4	5.6		4
115	0.00	-0.1	-0.0	3.0	1	
115	4.74	-0.1	-0.0	4.0	1	
115	10.00	-0.1	-0.0	5.0	1	
115	0.00	-0.0	-0.0	-0.0	2	
115	4.74	-0.0	-0.0	-0.0	2	
115	10.00	-0.0	-0.0	-0.0	2	
115	0.00	-0.0	-101.6	0.1	3	
115	4.74	-0.0	-111.5	0.1	3	
115	10.00	-0.0	-119.3	0.1	3	
115	0.00	-0.2	-152.4	4.0		1
115	4.74	-0.2	-167.3	5.3		1
115	10.00	-0.2	-179.0	6.6		1
115	0.00	-0.1	-101.6	3.1		2
115	4.74	-0.1	-111.5	4.1		2
115	10.00	-0.1	-119.3	5.0		2
115	0.00	-0.1	-50.8	3.0		3
115	4.74	-0.1	-55.8	4.0		3
115	10.00	-0.1	-59.7	5.0		3
115	0.00	-0.1	-30.5	3.0		4
115	4.74	-0.1	-33.5	4.0		4
115	10.00	-0.1	-35.8	5.0		4
116	0.00	-0.1	-0.0	-0.4	1	
116	4.74	-0.1	-0.0	1.3	1	
116	10.00	-0.1	-0.0	3.0	1	
116	0.00	-0.0	-0.0	-0.0	2	
116	4.74	-0.0	-0.0	-0.0	2	
116	10.00	-0.0	-0.0	-0.0	2	
116	0.00	-0.0	-71.5	0.1	3	
116	4.74	-0.0	-87.3	0.1	3	

116	10.00	-0.0	-101.5	0.1	3	
116	0.00	-0.2	-107.2	-0.3		1
116	4.74	-0.2	-130.9	1.9		1
116	10.00	-0.2	-152.3	4.1		1
116	0.00	-0.1	-71.5	-0.2		2
116	4.74	-0.1	-87.3	1.4		2
116	10.00	-0.1	-101.5	3.1		2
116	0.00	-0.1	-35.7	-0.3		3
116	4.74	-0.1	-43.6	1.4		3
116	10.00	-0.1	-50.8	3.0		3
116	0.00	-0.1	-21.5	-0.3		4
116	4.74	-0.1	-26.2	1.3		4
116	10.00	-0.1	-30.5	3.0		4
117	0.00	-0.1	-0.0	-5.2	1	
117	4.74	-0.1	-0.0	-2.8	1	
117	10.00	-0.1	-0.0	-0.4	1	
117	0.00	-0.0	-0.0	-0.0	2	
117	4.74	-0.0	-0.0	-0.0	2	
117	10.00	-0.0	-0.0	-0.0	2	
117	0.00	-0.0	-29.1	0.2	3	
117	4.74	-0.0	-50.7	0.1	3	
117	10.00	-0.0	-71.4	0.1	3	
117	0.00	-0.2	-43.6	-6.5		1
117	4.74	-0.2	-76.0	-3.4		1
117	10.00	-0.2	-107.2	-0.3		1
117	0.00	-0.1	-29.1	-5.0		2
117	4.74	-0.1	-50.7	-2.7		2
117	10.00	-0.1	-71.4	-0.2		2
117	0.00	-0.1	-14.5	-5.1		3
117	4.74	-0.1	-25.4	-2.7		3
117	10.00	-0.1	-35.7	-0.3		3
117	0.00	-0.1	-8.7	-5.1		4
117	4.74	-0.1	-15.2	-2.8		4
117	10.00	-0.1	-21.4	-0.3		4
118	0.00	-0.1	-0.0	-10.9	1	
118	4.74	-0.1	-0.0	-8.1	1	
118	10.00	-0.1	-0.0	-5.1	1	
118	0.00	-0.0	-0.0	-0.0	2	
118	4.74	-0.0	-0.0	-0.0	2	
118	10.00	-0.0	-0.0	-0.0	2	
118	0.00	-0.0	25.6	0.2	3	
118	4.74	-0.0	-1.8	0.2	3	
118	10.00	-0.0	-29.0	0.2	3	
118	0.00	-0.2	38.4	-13.9		1
118	4.74	-0.2	-2.7	-10.3		1
118	10.00	-0.2	-43.6	-6.4		1
118	0.00	-0.1	25.6	-10.7		2
118	4.74	-0.1	-1.8	-7.9		2
118	10.00	-0.1	-29.0	-5.0		2
118	0.00	-0.1	12.8	-10.8		3
118	4.74	-0.1	-0.9	-8.0		3
118	10.00	-0.1	-14.5	-5.1		3
118	0.00	-0.1	7.7	-10.8		4
118	4.74	-0.1	-0.6	-8.1		4
118	10.00	-0.1	-8.7	-5.1		4
119	0.00	0.2	-0.0	0.4	1	
119	4.74	0.2	-0.0	-2.1	1	
119	10.00	0.2	-0.0	-6.1	1	
119	0.00	-0.0	-0.0	-0.0	2	
119	4.74	-0.0	-0.0	-0.0	2	
119	10.00	-0.0	-0.0	-0.0	2	
119	0.00	0.3	-30.4	0.0	3	
119	4.74	0.3	-32.5	-0.2	3	
119	10.00	0.3	-34.7	-0.4	3	
119	0.00	0.8	-45.7	0.6		1
119	4.74	0.8	-48.7	-2.9		1
119	10.00	0.8	-52.1	-8.5		1
119	0.00	0.6	-30.5	0.5		2
119	4.74	0.6	-32.5	-2.2		2
119	10.00	0.6	-34.7	-6.5		2
119	0.00	0.4	-15.2	0.5		3
119	4.74	0.4	-16.2	-2.2		3
119	10.00	0.4	-17.4	-6.3		3
119	0.00	0.3	-9.1	0.4		4
119	4.74	0.3	-9.8	-2.1		4
119	10.00	0.3	-10.4	-6.2		4
120	0.00	0.2	-0.0	-0.2	1	
120	4.74	0.2	-0.0	0.6	1	
120	10.00	0.2	-0.0	0.2	1	
120	0.00	-0.0	-0.0	-0.0	2	
120	4.74	-0.0	-0.0	-0.0	2	
120	10.00	-0.0	-0.0	-0.0	2	
120	0.00	0.3	-26.1	0.0	3	
120	4.74	0.3	-28.3	0.0	3	
120	10.00	0.3	-30.8	0.0	3	
120	0.00	0.8	-39.2	-0.3		1
120	4.74	0.8	-42.5	0.7		1
120	10.00	0.8	-46.2	0.3		1
120	0.00	0.6	-26.1	-0.2		2
120	4.74	0.6	-28.3	0.6		2
120	10.00	0.6	-30.8	0.2		2
120	0.00	0.4	-13.1	-0.2		3
120	4.74	0.4	-14.2	0.6		3
120	10.00	0.4	-15.4	0.2		3
120	0.00	0.3	-7.8	-0.2		4
120	4.74	0.3	-8.5	0.6		4
120	10.00	0.3	-9.3	0.2		4
121	0.00	0.2	-0.0	0.2	1	
121	4.74	0.2	-0.0	0.5	1	
121	10.00	0.2	-0.0	-0.5	1	
121	0.00	-0.0	-0.0	-0.0	2	
121	4.74	-0.0	-0.0	-0.0	2	
121	10.00	-0.0	-0.0	-0.0	2	
121	0.00	0.3	-21.4	0.0	3	
121	4.74	0.3	-23.8	0.0	3	
121	10.00	0.3	-26.4	0.0	3	
121	0.00	0.8	-32.2	0.3		1
121	4.74	0.8	-35.7	0.6		1
121	10.00	0.8	-39.7	-0.6		1
121	0.00	0.6	-21.4	0.2		2
121	4.74	0.6	-23.8	0.5		2
121	10.00	0.6	-26.5	-0.5		2
121	0.00	0.4	-10.7	0.2		3
121	4.74	0.4	-11.9	0.5		3
121	10.00	0.4	-13.2	-0.5		3
121	0.00	0.3	-6.4	0.2		4
121	4.74	0.3	-7.2	0.5		4
121	10.00	0.3	-7.9	-0.5		4

122	0.00	0.2	-0.0	0.7	1	
122	4.74	0.2	-0.0	0.9	1	
122	10.00	0.2	-0.0	-0.0	1	
122	0.00	-0.0	-0.0	-0.0	2	
122	4.74	-0.0	-0.0	-0.0	2	
122	10.00	-0.0	-0.0	-0.0	2	
122	0.00	0.3	-16.4	0.0	3	
122	4.74	0.3	-18.9	0.0	3	
122	10.00	0.3	-21.7	-0.0	3	
122	0.00	0.8	-24.6	0.9		1
122	4.74	0.8	-28.4	1.2		1
122	10.00	0.8	-32.6	-0.0		1
122	0.00	0.6	-16.4	0.7		2
122	4.74	0.6	-18.9	0.9		2
122	10.00	0.6	-21.7	-0.0		2
122	0.00	0.4	-8.2	0.7		3
122	4.74	0.4	-9.5	0.9		3
122	10.00	0.4	-10.9	-0.0		3
122	0.00	0.3	-4.9	0.7		4
122	4.74	0.3	-5.7	0.9		4
122	10.00	0.3	-6.5	-0.0		4
123	0.00	0.2	-0.0	0.8	1	
123	4.74	0.2	-0.0	1.2	1	
123	10.00	0.2	-0.0	0.5	1	
123	0.00	-0.0	-0.0	-0.0	2	
123	4.74	-0.0	-0.0	-0.0	2	
123	10.00	-0.0	-0.0	-0.0	2	
123	0.00	0.3	-11.1	0.0	3	
123	4.74	0.3	-13.8	0.0	3	
123	10.00	0.3	-16.7	0.0	3	
123	0.00	0.8	-16.7	1.0		1
123	4.74	0.8	-20.7	1.6		1
123	10.00	0.8	-25.1	0.7		1
123	0.00	0.6	-11.1	0.8		2
123	4.74	0.6	-13.8	1.3		2
123	10.00	0.6	-16.7	0.5		2
123	0.00	0.4	-5.6	0.8		3
123	4.74	0.4	-6.9	1.2		3
123	10.00	0.4	-8.4	0.5		3
123	0.00	0.3	-3.3	0.8		4
123	4.74	0.3	-4.1	1.2		4
123	10.00	0.3	-5.0	0.5		4
124	0.00	0.2	-0.0	0.6	1	
124	4.74	0.2	-0.0	1.2	1	
124	10.00	0.2	-0.0	0.8	1	
124	0.00	-0.0	-0.0	-0.0	2	
124	4.74	-0.0	-0.0	-0.0	2	
124	10.00	-0.0	-0.0	-0.0	2	
124	0.00	0.3	-5.5	0.0	3	
124	4.74	0.3	-8.3	0.0	3	
124	10.00	0.3	-11.4	0.0	3	
124	0.00	0.8	-8.3	0.8		1
124	4.74	0.8	-12.4	1.6		1
124	10.00	0.8	-17.0	1.0		1
124	0.00	0.6	-5.5	0.6		2
124	4.74	0.6	-8.3	1.3		2
124	10.00	0.6	-11.4	0.8		2
124	0.00	0.4	-2.8	0.6		3
124	4.74	0.4	-4.1	1.2		3
124	10.00	0.4	-5.7	0.8		3
124	0.00	0.3	-1.7	0.6		4
124	4.74	0.3	-2.5	1.2		4
124	10.00	0.3	-3.4	0.8		4
125	0.00	0.2	0.0	0.0	1	
125	4.74	0.2	-0.0	0.9	1	
125	10.00	0.2	-0.0	0.7	1	
125	0.00	-0.0	-0.0	-0.0	2	
125	4.74	-0.0	-0.0	-0.0	2	
125	10.00	-0.0	-0.0	-0.0	2	
125	0.00	0.3	0.4	0.0	3	
125	4.74	0.3	-2.5	0.0	3	
125	10.00	0.3	-5.7	0.0	3	
125	0.00	0.8	0.6	0.1		1
125	4.74	0.8	-3.7	1.2		1
125	10.00	0.8	-8.6	0.9		1
125	0.00	0.6	0.4	0.1		2
125	4.74	0.6	-2.5	0.9		2
125	10.00	0.6	-5.7	0.7		2
125	0.00	0.4	0.2	0.1		3
125	4.74	0.4	-1.2	0.9		3
125	10.00	0.4	-2.9	0.7		3
125	0.00	0.3	0.1	0.0		4
125	4.74	0.3	-0.7	0.9		4
125	10.00	0.3	-1.7	0.7		4
126	0.00	0.2	0.0	-0.4	1	
126	4.74	0.2	0.0	0.5	1	
126	10.00	0.2	0.0	0.2	1	
126	0.00	-0.0	-0.0	-0.0	2	
126	4.74	-0.0	-0.0	-0.0	2	
126	10.00	-0.0	-0.0	-0.0	2	
126	0.00	0.3	6.7	0.0	3	
126	4.74	0.3	3.7	0.0	3	
126	10.00	0.3	0.3	0.0	3	
126	0.00	0.8	10.1	-0.5		1
126	4.74	0.8	5.5	0.7		1
126	10.00	0.8	0.4	0.3		1
126	0.00	0.6	6.7	-0.4		2
126	4.74	0.6	3.7	0.5		2
126	10.00	0.6	0.3	0.3		2
126	0.00	0.4	3.4	-0.4		3
126	4.74	0.4	1.8	0.5		3
126	10.00	0.4	0.1	0.3		3
126	0.00	0.3	2.0	-0.4		4
126	4.74	0.3	1.1	0.5		4
126	10.00	0.3	0.1	0.3		4
127	0.00	0.2	0.0	0.3	1	
127	4.74	0.2	0.0	0.6	1	
127	10.00	0.2	0.0	-0.2	1	
127	0.00	-0.0	-0.0	-0.0	2	
127	4.74	-0.0	-0.0	-0.0	2	
127	10.00	-0.0	-0.0	-0.0	2	
127	0.00	0.3	13.4	0.0	3	
127	4.74	0.3	10.2	0.0	3	
127	10.00	0.3	6.6	0.0	3	
127	0.00	0.8	20.1	0.4		1
127	4.74	0.8	15.3	0.9		1
127	10.00	0.8	9.9	-0.2		1
127	0.00	0.6	13.4	0.3		2

127	4.74	0.6	10.2	0.7	2
127	10.00	0.6	6.6	-0.1	2
127	0.00	0.4	6.7	0.3	3
127	4.74	0.4	5.1	0.7	3
127	10.00	0.4	3.3	-0.2	3
127	0.00	0.3	4.0	0.3	4
127	4.74	0.3	3.1	0.7	4
127	10.00	0.3	2.0	-0.2	4
128	0.00	0.2	0.0	-6.3	1
128	4.74	0.2	0.0	-2.5	1
128	10.00	0.2	0.0	0.5	1
128	0.00	-0.0	-0.0	-0.0	2
128	4.74	-0.0	-0.0	-0.0	2
128	10.00	-0.0	-0.0	-0.0	2
128	0.00	0.3	20.6	0.1	3
128	4.74	0.3	17.2	0.1	3
128	10.00	0.3	13.3	0.0	3
128	0.00	0.8	31.0	-8.0	1
128	4.74	0.8	25.8	-3.1	1
128	10.00	0.8	20.0	0.7	1
128	0.00	0.6	20.6	-6.2	2
128	4.74	0.6	17.2	-2.4	2
128	10.00	0.6	13.3	0.5	2
128	0.00	0.4	10.3	-6.2	3
128	4.74	0.4	8.6	-2.4	3
128	10.00	0.4	6.7	0.5	3
128	0.00	0.3	6.2	-6.2	4
128	4.74	0.3	5.2	-2.5	4
128	10.00	0.3	4.0	0.5	4
130	0.00	-0.0	0.0	0.0	1
130	1.89	-0.0	0.1	-2.9	1
130	4.00	-0.0	0.1	-6.2	1
130	0.00	-0.0	-0.0	-0.0	2
130	1.89	-0.0	-0.0	-0.0	2
130	4.00	-0.0	-0.0	-0.0	2
130	0.00	14.1	31.9	-1069.9	3
130	1.89	14.1	31.9	-1069.9	3
130	4.00	14.1	31.8	-1069.9	3
130	0.00	21.1	47.9	-1604.8	1
130	1.89	21.1	47.9	-1608.6	1
130	4.00	21.1	47.9	-1612.9	1
130	0.00	14.1	31.9	-1069.9	2
130	1.89	14.1	31.9	-1072.8	2
130	4.00	14.1	32.0	-1076.1	2
130	0.00	7.0	16.0	-534.9	3
130	1.89	7.0	16.0	-537.9	3
130	4.00	7.0	16.0	-541.1	3
130	0.00	4.2	9.6	-320.9	4
130	1.89	4.2	9.6	-323.9	4
130	4.00	4.2	9.7	-327.2	4
133	0.00	0.0	0.0	-0.0	1
133	1.89	0.0	-0.1	-2.0	1
133	4.00	0.0	-0.1	-4.2	1
133	0.00	-0.0	-0.0	-0.0	2
133	1.89	-0.0	-0.0	-0.0	2
133	4.00	-0.0	-0.0	-0.0	2
133	0.00	9.0	63.1	-783.3	3
133	1.89	9.0	63.0	-783.4	3
133	4.00	9.0	62.9	-783.4	3
133	0.00	13.5	94.6	-1175.0	1
133	1.89	13.5	94.4	-1177.6	1
133	4.00	13.5	94.2	-1180.5	1
133	0.00	9.0	63.1	-783.4	2
133	1.89	9.0	62.9	-785.3	2
133	4.00	9.0	62.8	-787.6	2
133	0.00	4.5	31.6	-391.7	3
133	1.89	4.5	31.4	-393.7	3
133	4.00	4.5	31.3	-395.9	3
133	0.00	2.7	18.9	-235.0	4
133	1.89	2.7	18.8	-237.0	4
133	4.00	2.7	18.7	-239.2	4
135	0.00	0.4	-0.0	-7.5	1
135	4.74	0.4	-0.0	-3.1	1
135	10.00	0.4	-0.0	0.5	1
135	0.00	-0.0	-0.0	-0.0	2
135	4.74	-0.0	-0.0	-0.0	2
135	10.00	-0.0	-0.0	-0.0	2
135	0.00	0.2	48.7	0.5	3
135	4.74	0.2	42.2	0.3	3
135	10.00	0.2	35.0	0.0	3
135	0.00	0.9	73.0	-8.9	1
135	4.74	0.9	63.3	-3.6	1
135	10.00	0.9	52.4	0.7	1
135	0.00	0.6	48.7	-7.0	2
135	4.74	0.6	42.2	-2.8	2
135	10.00	0.6	34.9	0.5	2
135	0.00	0.5	24.3	-7.2	3
135	4.74	0.5	21.1	-3.0	3
135	10.00	0.5	17.5	0.5	3
135	0.00	0.5	14.6	-7.3	4
135	4.74	0.5	12.6	-3.0	4
135	10.00	0.5	10.5	0.5	4
136	0.00	0.4	-0.0	0.1	1
136	4.74	0.4	-0.0	0.6	1
136	10.00	0.4	-0.0	-0.2	1
136	0.00	-0.0	-0.0	-0.0	2
136	4.74	-0.0	-0.0	-0.0	2
136	10.00	-0.0	-0.0	-0.0	2
136	0.00	0.2	35.3	0.1	3
136	4.74	0.2	29.0	0.1	3
136	10.00	0.2	22.0	0.0	3
136	0.00	0.9	53.0	0.3	1
136	4.74	0.9	43.5	0.8	1
136	10.00	0.9	33.0	-0.2	1
136	0.00	0.6	35.3	0.2	2
136	4.74	0.6	29.0	0.6	2
136	10.00	0.6	22.0	-0.1	2
136	0.00	0.5	17.6	0.2	3
136	4.74	0.5	14.5	0.6	3
136	10.00	0.5	11.0	-0.2	3
136	0.00	0.5	10.6	0.2	4
136	4.74	0.5	8.7	0.6	4
136	10.00	0.5	6.6	-0.2	4
137	0.00	0.4	-0.0	-0.5	1
137	4.74	0.4	-0.0	0.5	1
137	10.00	0.4	-0.0	0.3	1
137	0.00	-0.0	-0.0	-0.0	2
137	4.74	-0.0	-0.0	-0.0	2

137	10.00	-0.0	-0.0	-0.0	2	
137	0.00	0.2	22.4	0.1	3	
137	4.74	0.2	16.3	0.1	3	
137	10.00	0.2	9.5	0.0	3	
137	0.00	0.9	33.6	-0.5		1
137	4.74	0.9	24.4	0.7		1
137	10.00	0.9	14.2	0.4		1
137	0.00	0.6	22.4	-0.4		2
137	4.74	0.6	16.3	0.5		2
137	10.00	0.6	9.5	0.3		2
137	0.00	0.5	11.2	-0.5		3
137	4.74	0.5	8.1	0.5		3
137	10.00	0.5	4.7	0.3		3
137	0.00	0.5	6.7	-0.5		4
137	4.74	0.5	4.9	0.5		4
137	10.00	0.5	2.8	0.3		4
138	0.00	0.4	-0.0	0.0	1	
138	4.74	0.4	-0.0	1.0	1	
138	10.00	0.4	-0.0	0.9	1	
138	0.00	-0.0	-0.0	-0.0	2	
138	4.74	-0.0	-0.0	-0.0	2	
138	10.00	-0.0	-0.0	-0.0	2	
138	0.00	0.2	9.9	0.1	3	
138	4.74	0.2	3.9	0.0	3	
138	10.00	0.2	-2.7	-0.0	3	
138	0.00	0.9	14.9	0.1		1
138	4.74	0.9	5.9	1.4		1
138	10.00	0.9	-4.1	1.1		1
138	0.00	0.6	9.9	0.1		2
138	4.74	0.6	3.9	1.0		2
138	10.00	0.6	-2.8	0.9		2
138	0.00	0.5	5.0	0.1		3
138	4.74	0.5	2.0	1.0		3
138	10.00	0.5	-1.4	0.9		3
138	0.00	0.5	3.0	0.0		4
138	4.74	0.5	1.2	1.0		4
138	10.00	0.5	-0.8	0.9		4
139	0.00	0.4	-0.0	0.7	1	
139	4.74	0.4	-0.0	1.4	1	
139	10.00	0.4	0.0	1.1	1	
139	0.00	-0.0	-0.0	-0.0	2	
139	4.74	-0.0	-0.0	-0.0	2	
139	10.00	-0.0	-0.0	-0.0	2	
139	0.00	0.2	-2.2	0.0	3	
139	4.74	0.2	-8.1	0.0	3	
139	10.00	0.2	-14.7	-0.0	3	
139	0.00	0.9	-3.4	0.9		1
139	4.74	0.9	-12.2	1.9		1
139	10.00	0.9	-22.0	1.3		1
139	0.00	0.6	-2.2	0.7		2
139	4.74	0.6	-8.1	1.4		2
139	10.00	0.6	-14.7	1.0		2
139	0.00	0.5	-1.1	0.7		3
139	4.74	0.5	-4.1	1.4		3
139	10.00	0.5	-7.3	1.0		3
139	0.00	0.5	-0.7	0.7		4
139	4.74	0.5	-2.4	1.4		4
139	10.00	0.5	-4.4	1.0		4
140	0.00	0.4	0.0	1.0	1	
140	4.74	0.4	0.0	1.5	1	
140	10.00	0.4	0.0	0.9	1	
140	0.00	-0.0	-0.0	-0.0	2	
140	4.74	-0.0	-0.0	-0.0	2	
140	10.00	-0.0	-0.0	-0.0	2	
140	0.00	0.2	-14.1	0.0	3	
140	4.74	0.2	-19.9	-0.0	3	
140	10.00	0.2	-26.4	-0.1	3	
140	0.00	0.9	-21.2	1.3		1
140	4.74	0.9	-29.9	2.0		1
140	10.00	0.9	-39.6	1.1		1
140	0.00	0.6	-14.1	1.0		2
140	4.74	0.6	-19.9	1.5		2
140	10.00	0.6	-26.4	0.9		2
140	0.00	0.5	-7.1	1.0		3
140	4.74	0.5	-10.0	1.5		3
140	10.00	0.5	-13.2	0.9		3
140	0.00	0.5	-4.2	1.0		4
140	4.74	0.5	-6.0	1.5		4
140	10.00	0.5	-7.9	0.9		4
141	0.00	0.4	0.0	1.0	1	
141	4.74	0.4	0.0	1.4	1	
141	10.00	0.4	0.0	0.5	1	
141	0.00	-0.0	-0.0	-0.0	2	
141	4.74	-0.0	-0.0	-0.0	2	
141	10.00	-0.0	-0.0	-0.0	2	
141	0.00	0.2	-25.8	-0.0	3	
141	4.74	0.2	-31.5	-0.0	3	
141	10.00	0.2	-37.9	-0.1	3	
141	0.00	0.9	-38.7	1.3		1
141	4.74	0.9	-47.3	1.7		1
141	10.00	0.9	-56.8	0.5		1
141	0.00	0.6	-25.8	1.0		2
141	4.74	0.6	-31.5	1.3		2
141	10.00	0.6	-37.9	0.4		2
141	0.00	0.5	-12.9	1.0		3
141	4.74	0.5	-15.8	1.3		3
141	10.00	0.5	-18.9	0.4		3
141	0.00	0.5	-7.7	1.0		4
141	4.74	0.5	-9.5	1.3		4
141	10.00	0.5	-11.4	0.5		4
142	0.00	0.4	0.0	0.7	1	
142	4.74	0.4	0.0	1.1	1	
142	10.00	0.4	0.0	0.4	1	
142	0.00	-0.0	-0.0	-0.0	2	
142	4.74	-0.0	-0.0	-0.0	2	
142	10.00	-0.0	-0.0	-0.0	2	
142	0.00	0.2	-37.3	-0.0	3	
142	4.74	0.2	-42.9	-0.1	3	
142	10.00	0.2	-49.1	-0.1	3	
142	0.00	0.9	-55.9	0.9		1
142	4.74	0.9	-64.3	1.4		1
142	10.00	0.9	-73.7	0.3		1
142	0.00	0.6	-37.3	0.7		2
142	4.74	0.6	-42.9	1.1		2
142	10.00	0.6	-49.1	0.3		2
142	0.00	0.5	-18.6	0.7		3
142	4.74	0.5	-21.4	1.1		3
142	10.00	0.5	-24.6	0.3		3

142	0.00	0.5	-11.2	0.7		4
142	4.74	0.5	-12.9	1.1		4
142	10.00	0.5	-14.7	0.3		4
143	0.00	0.4	0.0	0.7	1	
143	4.74	0.4	0.0	1.4	1	
143	10.00	0.4	0.0	0.9	1	
143	0.00	-0.0	-0.0	-0.0	2	
143	4.74	-0.0	-0.0	-0.0	2	
143	10.00	-0.0	-0.0	-0.0	2	
143	0.00	0.2	-48.5	-0.1	3	
143	4.74	0.2	-54.1	-0.1	3	
143	10.00	0.2	-60.2	-0.1	3	
143	0.00	0.9	-72.8	0.9		1
143	4.74	0.9	-81.1	1.7		1
143	10.00	0.9	-90.3	1.1		1
143	0.00	0.6	-48.5	0.7		2
143	4.74	0.6	-54.0	1.3		2
143	10.00	0.6	-60.2	0.8		2
143	0.00	0.5	-24.3	0.7		3
143	4.74	0.5	-27.0	1.4		3
143	10.00	0.5	-30.1	0.9		3
143	0.00	0.5	-14.6	0.7		4
143	4.74	0.5	-16.2	1.4		4
143	10.00	0.5	-18.0	0.9		4
144	0.00	0.4	0.0	1.4	1	
144	4.74	0.4	0.0	-4.1	1	
144	10.00	0.4	0.0	-11.4	1	
144	0.00	-0.0	-0.0	-0.0	2	
144	4.74	-0.0	-0.0	-0.0	2	
144	10.00	-0.0	-0.0	-0.0	2	
144	0.00	0.2	-59.6	-0.1	3	
144	4.74	0.2	-65.0	-0.1	3	
144	10.00	0.2	-71.0	-0.1	3	
144	0.00	0.9	-89.4	1.7		1
144	4.74	0.9	-97.5	-5.5		1
144	10.00	0.9	-106.4	-15.0		1
144	0.00	0.6	-59.6	1.3		2
144	4.74	0.6	-65.0	-4.2		2
144	10.00	0.6	-71.0	-11.5		2
144	0.00	0.5	-29.8	1.3		3
144	4.74	0.5	-32.5	-4.1		3
144	10.00	0.5	-35.5	-11.5		3
144	0.00	0.5	-17.9	1.4		4
144	4.74	0.5	-19.5	-4.1		4
144	10.00	0.5	-21.3	-11.4		4
145	0.00	-0.1	-0.0	-12.5	1	
145	4.74	-0.1	-0.0	-9.4	1	
145	10.00	-0.1	-0.0	-6.2	1	
145	0.00	-0.0	-0.0	-0.0	2	
145	4.74	-0.0	-0.0	-0.0	2	
145	10.00	-0.0	-0.0	-0.0	2	
145	0.00	-0.0	-30.7	0.6	3	
145	4.74	-0.0	-52.2	0.5	3	
145	10.00	-0.0	-72.9	0.5	3	
145	0.00	-0.2	-46.0	-15.3		1
145	4.74	-0.2	-78.3	-11.5		1
145	10.00	-0.2	-109.3	-7.3		1
145	0.00	-0.1	-30.7	-11.9		2
145	4.74	-0.1	-52.2	-8.9		2
145	10.00	-0.1	-72.9	-5.7		2
145	0.00	-0.1	-15.4	-12.2		3
145	4.74	-0.1	-26.1	-9.2		3
145	10.00	-0.1	-36.4	-5.9		3
145	0.00	-0.1	-9.2	-12.3		4
145	4.74	-0.1	-15.7	-9.3		4
145	10.00	-0.1	-21.9	-6.0		4
146	0.00	-0.1	-0.0	-6.2	1	
146	4.74	-0.1	-0.0	-3.6	1	
146	10.00	-0.1	-0.0	-0.8	1	
146	0.00	-0.0	-0.0	-0.0	2	
146	4.74	-0.0	-0.0	-0.0	2	
146	10.00	-0.0	-0.0	-0.0	2	
146	0.00	-0.0	-72.9	0.5	3	
146	4.74	-0.0	-88.6	0.4	3	
146	10.00	-0.0	-102.8	0.4	3	
146	0.00	-0.2	-109.4	-7.3		1
146	4.74	-0.2	-133.0	-4.0		1
146	10.00	-0.2	-154.2	-0.5		1
146	0.00	-0.1	-73.0	-5.7		2
146	4.74	-0.1	-88.7	-3.2		2
146	10.00	-0.1	-102.8	-0.4		2
146	0.00	-0.1	-36.5	-6.0		3
146	4.74	-0.1	-44.3	-3.4		3
146	10.00	-0.1	-51.4	-0.6		3
146	0.00	-0.1	-21.9	-6.1		4
146	4.74	-0.1	-26.6	-3.5		4
146	10.00	-0.1	-30.9	-0.7		4
147	0.00	-0.1	-0.0	-0.8	1	
147	4.74	-0.1	-0.0	1.1	1	
147	10.00	-0.1	-0.0	3.1	1	
147	0.00	-0.0	-0.0	-0.0	2	
147	4.74	-0.0	-0.0	-0.0	2	
147	10.00	-0.0	-0.0	-0.0	2	
147	0.00	-0.0	-102.9	0.4	3	
147	4.74	-0.0	-112.8	0.3	3	
147	10.00	-0.0	-120.5	0.2	3	
147	0.00	-0.2	-154.4	-0.5		1
147	4.74	-0.2	-169.2	1.9		1
147	10.00	-0.2	-180.7	4.4		1
147	0.00	-0.1	-102.9	-0.5		2
147	4.74	-0.1	-112.8	1.4		2
147	10.00	-0.1	-120.5	3.4		2
147	0.00	-0.1	-51.5	-0.6		3
147	4.74	-0.1	-56.4	1.3		3
147	10.00	-0.1	-60.3	3.2		3
147	0.00	-0.1	-30.9	-0.7		4
147	4.74	-0.1	-33.8	1.2		4
147	10.00	-0.1	-36.2	3.2		4
148	0.00	-0.1	-0.0	3.1	1	
148	4.74	-0.1	-0.0	4.4	1	
148	10.00	-0.1	-0.0	5.7	1	
148	0.00	-0.0	-0.0	-0.0	2	
148	4.74	-0.0	-0.0	-0.0	2	
148	10.00	-0.0	-0.0	-0.0	2	
148	0.00	-0.0	-120.6	0.2	3	
148	4.74	-0.0	-124.6	0.2	3	
148	10.00	-0.0	-125.8	0.1	3	
148	0.00	-0.2	-180.9	4.4		1

148	4.74	-0.2	-186.9	6.0		1
148	10.00	-0.2	-188.7	7.6		1
148	0.00	-0.1	-120.6	3.3		2
148	4.74	-0.1	-124.6	4.6		2
148	10.00	-0.1	-125.8	5.8		2
148	0.00	-0.1	-60.3	3.2		3
148	4.74	-0.1	-62.3	4.5		3
148	10.00	-0.1	-62.9	5.7		3
148	0.00	-0.1	-36.2	3.2		4
148	4.74	-0.1	-37.4	4.5		4
148	10.00	-0.1	-37.7	5.7		4
149	0.00	-0.1	-0.0	5.7	1	
149	4.74	-0.1	-0.0	6.3	1	
149	10.00	-0.1	-0.0	6.9	1	
149	0.00	-0.0	-0.0	-0.0	2	
149	4.74	-0.0	-0.0	-0.0	2	
149	10.00	-0.0	-0.0	-0.0	2	
149	0.00	-0.0	-125.9	0.1	3	
149	4.74	-0.0	-124.1	0.1	3	
149	10.00	-0.0	-118.8	-0.0	3	
149	0.00	-0.2	-188.9	7.5		1
149	4.74	-0.2	-186.2	8.3		1
149	10.00	-0.2	-178.2	8.9		1
149	0.00	-0.1	-125.9	5.8		2
149	4.74	-0.1	-124.1	6.4		2
149	10.00	-0.1	-118.8	6.9		2
149	0.00	-0.1	-63.0	5.7		3
149	4.74	-0.1	-62.1	6.3		3
149	10.00	-0.1	-59.4	6.9		3
149	0.00	-0.1	-37.8	5.7		4
149	4.74	-0.1	-37.2	6.3		4
149	10.00	-0.1	-35.6	6.9		4
150	0.00	-0.1	-0.0	6.9	1	
150	4.74	-0.1	-0.0	6.9	1	
150	10.00	-0.1	-0.0	6.8	1	
150	0.00	-0.0	-0.0	-0.0	2	
150	4.74	-0.0	-0.0	-0.0	2	
150	10.00	-0.0	-0.0	-0.0	2	
150	0.00	-0.0	-118.9	-0.0	3	
150	4.74	-0.0	-111.2	-0.1	3	
150	10.00	-0.0	-99.4	-0.1	3	
150	0.00	-0.2	-178.4	8.9		1
150	4.74	-0.2	-166.9	8.9		1
150	10.00	-0.2	-149.2	8.6		1
150	0.00	-0.1	-118.9	6.9		2
150	4.74	-0.1	-111.3	6.8		2
150	10.00	-0.1	-99.4	6.6		2
150	0.00	-0.1	-59.5	6.9		3
150	4.74	-0.1	-55.6	6.9		3
150	10.00	-0.1	-49.7	6.7		3
150	0.00	-0.1	-35.7	6.9		4
150	4.74	-0.1	-33.4	6.9		4
150	10.00	-0.1	-29.8	6.7		4
151	0.00	-0.1	-0.0	6.8	1	
151	4.74	-0.1	0.0	6.1	1	
151	10.00	-0.1	0.0	5.3	1	
151	0.00	-0.0	-0.0	-0.0	2	
151	4.74	-0.0	-0.0	-0.0	2	
151	10.00	-0.0	-0.0	-0.0	2	
151	0.00	-0.0	-99.6	-0.1	3	
151	4.74	-0.0	-86.0	-0.2	3	
151	10.00	-0.0	-67.7	-0.3	3	
151	0.00	-0.2	-149.4	8.6		1
151	4.74	-0.2	-129.1	7.7		1
151	10.00	-0.2	-101.6	6.5		1
151	0.00	-0.1	-99.6	6.6		2
151	4.74	-0.1	-86.0	5.9		2
151	10.00	-0.1	-67.7	5.0		2
151	0.00	-0.1	-49.8	6.7		3
151	4.74	-0.1	-43.0	6.0		3
151	10.00	-0.1	-33.9	5.1		3
151	0.00	-0.1	-29.9	6.7		4
151	4.74	-0.1	-25.8	6.1		4
151	10.00	-0.1	-20.3	5.2		4
152	0.00	-0.1	0.0	5.3	1	
152	4.74	-0.1	0.0	4.0	1	
152	10.00	-0.1	0.0	2.4	1	
152	0.00	-0.0	-0.0	-0.0	2	
152	4.74	-0.0	-0.0	-0.0	2	
152	10.00	-0.0	-0.0	-0.0	2	
152	0.00	-0.0	-67.9	-0.3	3	
152	4.74	-0.0	-48.5	-0.3	3	
152	10.00	-0.0	-23.6	-0.4	3	
152	0.00	-0.2	-101.8	6.5		1
152	4.74	-0.2	-72.7	4.7		1
152	10.00	-0.2	-35.5	2.5		1
152	0.00	-0.1	-67.9	5.0		2
152	4.74	-0.1	-48.5	3.7		2
152	10.00	-0.1	-23.6	2.0		2
152	0.00	-0.1	-33.9	5.2		3
152	4.74	-0.1	-24.2	3.8		3
152	10.00	-0.1	-11.8	2.2		3
152	0.00	-0.1	-20.4	5.2		4
152	4.74	-0.1	-14.5	3.9		4
152	10.00	-0.1	-7.1	2.3		4
153	0.00	-0.1	0.0	2.4	1	
153	4.74	-0.1	0.0	0.5	1	
153	10.00	-0.1	0.0	-1.9	1	
153	0.00	-0.0	-0.0	-0.0	2	
153	4.74	-0.0	-0.0	-0.0	2	
153	10.00	-0.0	-0.0	-0.0	2	
153	0.00	-0.0	-23.8	-0.4	3	
153	4.74	-0.0	1.5	-0.4	3	
153	10.00	-0.0	32.8	-0.5	3	
153	0.00	-0.2	-35.7	2.6		1
153	4.74	-0.2	2.2	-0.1		1
153	10.00	-0.2	49.2	-3.2		1
153	0.00	-0.1	-23.8	2.0		2
153	4.74	-0.1	1.5	0.0		2
153	10.00	-0.1	32.8	-2.4		2
153	0.00	-0.1	-11.9	2.2		3
153	4.74	-0.1	0.7	0.2		3
153	10.00	-0.1	16.4	-2.1		3
153	0.00	-0.1	-7.1	2.3		4
153	4.74	-0.1	0.4	0.3		4
153	10.00	-0.1	9.8	-2.0		4
154	0.00	-0.1	0.0	-1.8	1	
154	4.74	-0.1	0.0	-4.1	1	

154	10.00	-0.1	0.0	-6.8	1
154	0.00	-0.0	-0.0	-0.0	2
154	4.74	-0.0	-0.0	-0.0	2
154	10.00	-0.0	-0.0	-0.0	2
154	0.00	-0.0	32.6	-0.5	3
154	4.74	-0.0	63.8	-0.6	3
154	10.00	-0.0	101.6	-0.6	3
154	0.00	-0.2	49.0	-3.2	1
154	4.74	-0.2	95.6	-6.2	1
154	10.00	-0.2	152.4	-9.8	1
154	0.00	-0.1	32.7	-2.4	2
154	4.74	-0.1	63.8	-4.7	2
154	10.00	-0.1	101.6	-7.4	2
154	0.00	-0.1	16.3	-2.1	3
154	4.74	-0.1	31.9	-4.4	3
154	10.00	-0.1	50.8	-7.1	3
154	0.00	-0.1	9.8	-2.0	4
154	4.74	-0.1	19.1	-4.3	4
154	10.00	-0.1	30.5	-7.0	4

RISULTATI : TENSIONI PILASTRI PER N.RO DI ELEMENTO

ELEM.	ascissa	N/A	M2/W2	M3/W3	CDC	COMB.
n.ro	(cm)	=====	(Kg/cm2)	=====	n.ro	n.ro
1	0.00	-1.7	-0.0	-0.2	1	
1	12.79	-1.6	-0.0	-0.7	1	
1	27.00	-1.5	-0.0	-1.2	1	
1	0.00	-0.0	-0.0	-0.0	2	
1	12.79	-0.0	-0.0	-0.0	2	
1	27.00	-0.0	-0.0	-0.0	2	
1	0.00	-0.0	-783.3	0.8	3	
1	12.79	-0.0	-713.3	0.2	3	
1	27.00	-0.0	-635.6	-0.4	3	
1	0.00	-2.2	-1175.0	0.9		1
1	12.79	-2.1	-1070.1	-0.6		1
1	27.00	-1.9	-953.4	-2.2		1
1	0.00	-1.7	-783.4	0.6		2
1	12.79	-1.6	-713.4	-0.5		2
1	27.00	-1.5	-635.6	-1.6		2
1	0.00	-1.7	-391.7	0.2		3
1	12.79	-1.6	-356.7	-0.6		3
1	27.00	-1.5	-317.8	-1.4		3
1	0.00	-1.7	-235.0	0.0		4
1	12.79	-1.6	-214.0	-0.6		4
1	27.00	-1.5	-190.7	-1.3		4
3	0.00	-1.4	-0.0	-1.6	1	
3	48.32	-1.0	-0.0	1.3	1	
3	102.00	-0.6	-0.0	4.6	1	
3	0.00	-0.0	-0.0	-0.0	2	
3	48.32	-0.0	-0.0	-0.0	2	
3	102.00	-0.0	-0.0	-0.0	2	
3	0.00	-0.0	-632.1	-0.4	3	
3	48.32	-0.0	-356.9	-0.0	3	
3	102.00	-0.0	-51.1	0.4	3	
3	0.00	-1.8	-948.1	-2.7		1
3	48.32	-1.3	-535.3	1.7		1
3	102.00	-0.8	-76.7	6.6		1
3	0.00	-1.4	-632.1	-2.0		2
3	48.32	-1.0	-356.9	1.3		2
3	102.00	-0.6	-51.1	5.0		2
3	0.00	-1.4	-316.1	-1.8		3
3	48.32	-1.0	-178.5	1.3		3
3	102.00	-0.6	-25.6	4.8		3
3	0.00	-1.4	-189.6	-1.7		4
3	48.32	-1.0	-107.1	1.3		4
3	102.00	-0.6	-15.3	4.7		4
4	0.00	-2.2	0.0	0.4	1	
4	48.32	-1.8	0.0	-0.1	1	
4	102.00	-1.4	-0.0	-0.7	1	
4	0.00	-0.0	-0.0	-0.0	2	
4	48.32	-0.0	-0.0	-0.0	2	
4	102.00	-0.0	-0.0	-0.0	2	
4	0.00	0.0	-831.7	-0.2	3	
4	48.32	0.0	-425.7	0.1	3	
4	102.00	0.0	25.4	0.4	3	
4	0.00	-2.9	-1247.5	0.2		1
4	48.32	-2.4	-638.5	-0.0		1
4	102.00	-1.8	38.1	-0.3		1
4	0.00	-2.2	-831.7	0.2		2
4	48.32	-1.8	-425.7	-0.0		2
4	102.00	-1.4	25.4	-0.3		2
4	0.00	-2.2	-415.8	0.3		3
4	48.32	-1.8	-212.8	-0.1		3
4	102.00	-1.4	12.7	-0.5		3
4	0.00	-2.2	-249.5	0.4		4
4	48.32	-1.8	-127.7	-0.1		4
4	102.00	-1.4	7.6	-0.6		4
6	0.00	-2.5	0.0	-0.4	1	
6	12.79	-2.4	0.0	-0.0	1	
6	27.00	-2.3	0.0	0.4	1	
6	0.00	-0.0	-0.0	-0.0	2	
6	12.79	-0.0	-0.0	-0.0	2	
6	27.00	-0.0	-0.0	-0.0	2	
6	0.00	0.0	-1069.9	0.3	3	
6	12.79	0.0	-960.0	0.1	3	
6	27.00	0.0	-838.0	-0.2	3	
6	0.00	-3.3	-1604.8	-0.0		1
6	12.79	-3.2	-1440.0	0.1		1
6	27.00	-3.0	-1256.9	0.2		1
6	0.00	-2.5	-1069.9	-0.1		2
6	12.79	-2.4	-960.0	0.1		2
6	27.00	-2.3	-838.0	0.2		2
6	0.00	-2.5	-534.9	-0.2		3
6	12.79	-2.4	-480.0	0.0		3
6	27.00	-2.3	-419.0	0.3		3
6	0.00	-2.5	-320.9	-0.3		4
6	12.79	-2.4	-288.0	0.0		4
6	27.00	-2.3	-251.4	0.3		4
27	0.00	-0.7	-0.0	-2.2	1	
27	48.32	-0.3	-0.0	-0.2	1	
27	102.00	0.1	-0.0	2.0	1	
27	0.00	-0.0	-0.0	-0.0	2	
27	48.32	-0.0	-0.0	-0.0	2	
27	102.00	-0.0	-0.0	-0.0	2	
27	0.00	-0.0	-88.7	-0.1	3	
27	48.32	-0.0	-54.6	-0.0	3	
27	102.00	-0.0	-16.6	0.1	3	

27	0.00	-0.9	-133.0	-3.1	1
27	48.32	-0.4	-81.8	-0.3	1
27	102.00	0.1	-24.9	2.8	1
27	0.00	-0.7	-88.7	-2.4	2
27	48.32	-0.3	-54.6	-0.2	2
27	102.00	0.1	-16.6	2.1	2
27	0.00	-0.7	-44.4	-2.3	3
27	48.32	-0.3	-27.3	-0.2	3
27	102.00	0.1	-8.3	2.1	3
27	0.00	-0.7	-26.6	-2.3	4
27	48.32	-0.3	-16.4	-0.2	4
27	102.00	0.1	-5.0	2.0	4
28	0.00	0.4	-0.0	-1.8	1
28	48.32	0.8	-0.0	-0.1	1
28	102.00	1.2	0.0	1.7	1
28	0.00	-0.0	-0.0	-0.0	2
28	48.32	-0.0	-0.0	-0.0	2
28	102.00	-0.0	-0.0	-0.0	2
28	0.00	0.0	-78.2	-0.2	3
28	48.32	0.0	-51.2	-0.0	3
28	102.00	0.0	-21.2	0.2	3
28	0.00	0.6	-117.3	-2.6	1
28	48.32	1.1	-76.8	-0.1	1
28	102.00	1.6	-31.7	2.5	1
28	0.00	0.4	-78.2	-1.9	2
28	48.32	0.8	-51.2	-0.1	2
28	102.00	1.2	-21.2	1.9	2
28	0.00	0.4	-39.1	-1.8	3
28	48.32	0.8	-25.6	-0.1	3
28	102.00	1.2	-10.6	1.8	3
28	0.00	0.4	-23.5	-1.8	4
28	48.32	0.8	-15.4	-0.1	4
28	102.00	1.2	-6.3	1.8	4
29	0.00	0.4	-0.0	-1.2	1
29	48.32	0.8	-0.0	-0.1	1
29	102.00	1.2	0.0	1.2	1
29	0.00	-0.0	-0.0	-0.0	2
29	48.32	-0.0	-0.0	-0.0	2
29	102.00	-0.0	-0.0	-0.0	2
29	0.00	0.0	-72.7	-0.2	3
29	48.32	0.0	-49.2	-0.0	3
29	102.00	0.0	-23.1	0.2	3
29	0.00	0.5	-109.0	-1.9	1
29	48.32	1.0	-73.8	-0.1	1
29	102.00	1.6	-34.6	2.0	1
29	0.00	0.4	-72.7	-1.5	2
29	48.32	0.8	-49.2	-0.1	2
29	102.00	1.2	-23.1	1.5	2
29	0.00	0.4	-36.3	-1.3	3
29	48.32	0.8	-24.6	-0.1	3
29	102.00	1.2	-11.5	1.4	3
29	0.00	0.4	-21.8	-1.3	4
29	48.32	0.8	-14.8	-0.1	4
29	102.00	1.2	-6.9	1.3	4
30	0.00	0.4	-0.0	-0.5	1
30	48.32	0.7	-0.0	-0.0	1
30	102.00	1.2	0.0	0.5	1
30	0.00	-0.0	-0.0	-0.0	2
30	48.32	-0.0	-0.0	-0.0	2
30	102.00	-0.0	-0.0	-0.0	2
30	0.00	0.0	-71.1	-0.3	3
30	48.32	0.0	-48.4	-0.0	3
30	102.00	0.0	-23.1	0.3	3
30	0.00	0.5	-106.6	-1.1	1
30	48.32	1.0	-72.6	-0.1	1
30	102.00	1.5	-34.7	1.1	1
30	0.00	0.4	-71.1	-0.8	2
30	48.32	0.7	-48.4	-0.0	2
30	102.00	1.2	-23.1	0.8	2
30	0.00	0.4	-35.5	-0.7	3
30	48.32	0.7	-24.2	-0.0	3
30	102.00	1.2	-11.6	0.7	3
30	0.00	0.4	-21.3	-0.6	4
30	48.32	0.7	-14.5	-0.0	4
30	102.00	1.2	-6.9	0.6	4
31	0.00	0.4	-0.0	0.3	1
31	48.32	0.7	-0.0	0.0	1
31	102.00	1.2	0.0	-0.3	1
31	0.00	-0.0	-0.0	-0.0	2
31	48.32	-0.0	-0.0	-0.0	2
31	102.00	-0.0	-0.0	-0.0	2
31	0.00	0.0	-73.0	-0.3	3
31	48.32	0.0	-48.7	-0.0	3
31	102.00	0.0	-21.8	0.3	3
31	0.00	0.5	-109.5	-0.1	1
31	48.32	1.0	-73.1	-0.0	1
31	102.00	1.5	-32.7	0.1	1
31	0.00	0.4	-73.0	-0.0	2
31	48.32	0.7	-48.7	-0.0	2
31	102.00	1.2	-21.8	0.0	2
31	0.00	0.4	-36.5	0.1	3
31	48.32	0.7	-24.4	0.0	3
31	102.00	1.2	-10.9	-0.1	3
31	0.00	0.4	-21.9	0.2	4
31	48.32	0.7	-14.6	0.0	4
31	102.00	1.2	-6.5	-0.2	4
32	0.00	0.4	0.0	1.0	1
32	48.32	0.7	0.0	0.1	1
32	102.00	1.2	0.0	-1.0	1
32	0.00	-0.0	-0.0	-0.0	2
32	48.32	-0.0	-0.0	-0.0	2
32	102.00	-0.0	-78.2	-0.3	3
32	0.00	-0.0	-50.3	-0.0	3
32	48.32	-0.0	-19.3	0.3	3
32	0.00	0.5	-117.3	0.9	1
32	48.32	1.0	-75.5	0.0	1
32	102.00	1.5	-29.0	-0.9	1
32	0.00	0.4	-78.2	0.7	2
32	48.32	0.7	-50.3	0.0	2
32	102.00	1.2	-19.3	-0.7	2
32	0.00	0.4	-39.1	0.9	3
32	48.32	0.7	-25.2	0.0	3
32	102.00	1.2	-9.7	-0.9	3
32	0.00	0.4	-23.5	0.9	4
32	48.32	0.7	-15.1	0.0	4
32	102.00	1.2	-5.8	-0.9	4
33	0.00	0.4	0.0	1.5	1

33	48.32	0.8	0.0	0.1	1	
33	102.00	1.2	0.0	-1.5	1	
33	0.00	-0.0	-0.0	-0.0	2	
33	48.32	-0.0	-0.0	-0.0	2	
33	102.00	-0.0	-0.0	-0.0	2	
33	0.00	-0.0	-86.8	-0.2	3	
33	48.32	-0.0	-53.1	-0.0	3	
33	102.00	-0.0	-15.7	0.2	3	
33	0.00	0.5	-130.2	1.6		1
33	48.32	1.0	-79.7	0.1		1
33	102.00	1.6	-23.6	-1.6		1
33	0.00	0.4	-86.8	1.3		2
33	48.32	0.8	-53.1	0.1		2
33	102.00	1.2	-15.7	-1.3		2
33	0.00	0.4	-43.4	1.4		3
33	48.32	0.8	-26.6	0.1		3
33	102.00	1.2	-7.9	-1.4		3
33	0.00	0.4	-26.0	1.4		4
33	48.32	0.8	-15.9	0.1		4
33	102.00	1.2	-4.7	-1.4		4
34	0.00	0.5	0.0	1.7	1	
34	48.32	0.9	0.0	0.1	1	
34	102.00	1.3	-0.0	-1.7	1	
34	0.00	-0.0	-0.0	-0.0	2	
34	48.32	-0.0	-0.0	-0.0	2	
34	102.00	-0.0	-0.0	-0.0	2	
34	0.00	-0.0	-99.1	-0.2	3	
34	48.32	-0.0	-57.4	-0.0	3	
34	102.00	-0.0	-10.9	0.2	3	
34	0.00	0.6	-148.7	1.8		1
34	48.32	1.1	-86.0	0.1		1
34	102.00	1.7	-16.4	-1.8		1
34	0.00	0.5	-99.1	1.4		2
34	48.32	0.9	-57.4	0.1		2
34	102.00	1.3	-10.9	-1.4		2
34	0.00	0.5	-49.6	1.5		3
34	48.32	0.9	-28.7	0.1		3
34	102.00	1.3	-5.5	-1.6		3
34	0.00	0.5	-29.7	1.6		4
34	48.32	0.9	-17.2	0.1		4
34	102.00	1.3	-3.3	-1.6		4
35	0.00	-0.3	0.0	1.7	1	
35	48.32	0.1	0.0	0.2	1	
35	102.00	0.5	-0.0	-1.5	1	
35	0.00	-0.0	-0.0	-0.0	2	
35	48.32	-0.0	-0.0	-0.0	2	
35	102.00	-0.0	-0.0	-0.0	2	
35	0.00	0.0	-116.0	-0.2	3	
35	48.32	0.0	-63.2	-0.0	3	
35	102.00	0.0	-4.5	0.2	3	
35	0.00	-0.3	-174.1	1.9		1
35	48.32	0.2	-94.8	0.2		1
35	102.00	0.7	-6.7	-1.6		1
35	0.00	-0.3	-116.0	1.5		2
35	48.32	0.1	-63.2	0.2		2
35	102.00	0.5	-4.5	-1.3		2
35	0.00	-0.3	-58.0	1.6		3
35	48.32	0.1	-31.6	0.2		3
35	102.00	0.5	-2.2	-1.4		3
35	0.00	-0.3	-34.8	1.6		4
35	48.32	0.1	-19.0	0.2		4
35	102.00	0.5	-1.3	-1.4		4
36	0.00	-0.2	0.0	1.3	1	
36	48.32	0.2	0.0	0.2	1	
36	102.00	0.6	0.0	-1.1	1	
36	0.00	-0.0	-0.0	-0.0	2	
36	48.32	-0.0	-0.0	-0.0	2	
36	102.00	-0.0	-0.0	-0.0	2	
36	0.00	0.0	-128.1	-0.0	3	
36	48.32	0.0	-69.9	-0.0	3	
36	102.00	0.0	-5.3	0.0	3	
36	0.00	-0.3	-192.2	1.6		1
36	48.32	0.2	-104.9	0.2		1
36	102.00	0.8	-7.9	-1.4		1
36	0.00	-0.2	-128.1	1.3		2
36	48.32	0.2	-69.9	0.2		2
36	102.00	0.6	-5.3	-1.1		2
36	0.00	-0.2	-64.1	1.3		3
36	48.32	0.2	-35.0	0.2		3
36	102.00	0.6	-2.6	-1.1		3
36	0.00	-0.2	-38.4	1.3		4
36	48.32	0.2	-21.0	0.2		4
36	102.00	0.6	-1.6	-1.1		4
37	0.00	0.5	0.0	1.2	1	
37	48.32	0.9	0.0	0.1	1	
37	102.00	1.3	0.0	-1.2	1	
37	0.00	-0.0	-0.0	-0.0	2	
37	48.32	-0.0	-0.0	-0.0	2	
37	102.00	-0.0	-0.0	-0.0	2	
37	0.00	-0.0	-110.2	-0.1	3	
37	48.32	-0.0	-63.7	-0.0	3	
37	102.00	-0.0	-12.0	0.1	3	
37	0.00	0.6	-165.2	1.5		1
37	48.32	1.1	-95.5	0.1		1
37	102.00	1.7	-18.0	-1.5		1
37	0.00	0.5	-110.2	1.2		2
37	48.32	0.9	-63.7	0.1		2
37	102.00	1.3	-12.0	-1.2		2
37	0.00	0.5	-55.1	1.2		3
37	48.32	0.9	-31.8	0.1		3
37	102.00	1.3	-6.0	-1.2		3
37	0.00	0.5	-33.0	1.2		4
37	48.32	0.9	-19.1	0.1		4
37	102.00	1.3	-3.6	-1.2		4
38	0.00	0.4	0.0	1.1	1	
38	48.32	0.8	0.0	0.0	1	
38	102.00	1.2	0.0	-1.1	1	
38	0.00	-0.0	-0.0	-0.0	2	
38	48.32	-0.0	-0.0	-0.0	2	
38	102.00	-0.0	-0.0	-0.0	2	
38	0.00	-0.0	-97.9	-0.1	3	
38	48.32	-0.0	-59.2	-0.0	3	
38	102.00	-0.0	-16.3	0.1	3	
38	0.00	0.5	-146.8	1.3		1
38	48.32	1.0	-88.8	0.1		1
38	102.00	1.5	-24.4	-1.3		1
38	0.00	0.4	-97.9	1.0		2
38	48.32	0.8	-59.2	0.0		2

38	102.00	1.2	-16.3	-1.0		2
38	0.00	0.4	-48.9	1.0		3
38	48.32	0.8	-29.6	0.0		3
38	102.00	1.2	-8.1	-1.0		3
38	0.00	0.4	-29.4	1.0		4
38	48.32	0.8	-17.8	0.0		4
38	102.00	1.2	-4.9	-1.0		4
39	0.00	0.4	0.0	0.6	1	
39	48.32	0.7	0.0	0.0	1	
39	102.00	1.2	0.0	-0.6	1	
39	0.00	-0.0	-0.0	-0.0	2	
39	48.32	-0.0	-0.0	-0.0	2	
39	102.00	-0.0	-0.0	-0.0	2	
39	0.00	-0.0	-90.3	-0.1	3	
39	48.32	-0.0	-56.4	-0.0	3	
39	102.00	-0.0	-18.7	0.1	3	
39	0.00	0.5	-135.4	0.7		1
39	48.32	1.0	-84.6	0.0		1
39	102.00	1.5	-28.1	-0.7		1
39	0.00	0.4	-90.3	0.5		2
39	48.32	0.7	-56.4	0.0		2
39	102.00	1.2	-18.7	-0.5		2
39	0.00	0.4	-45.1	0.6		3
39	48.32	0.7	-28.2	0.0		3
39	102.00	1.2	-9.4	-0.6		3
39	0.00	0.4	-27.1	0.6		4
39	48.32	0.7	-16.9	0.0		4
39	102.00	1.2	-5.6	-0.6		4
40	0.00	0.4	0.0	-0.0	1	
40	48.32	0.7	0.0	-0.0	1	
40	102.00	1.2	0.0	0.0	1	
40	0.00	-0.0	-0.0	-0.0	2	
40	48.32	-0.0	-0.0	-0.0	2	
40	102.00	-0.0	-0.0	-0.0	2	
40	0.00	-0.0	-86.9	-0.1	3	
40	48.32	-0.0	-55.0	-0.0	3	
40	102.00	-0.0	-19.6	0.1	3	
40	0.00	0.5	-130.3	-0.1		1
40	48.32	1.0	-82.5	-0.0		1
40	102.00	1.5	-29.4	0.1		1
40	0.00	0.4	-86.9	-0.1		2
40	48.32	0.7	-55.0	-0.0		2
40	102.00	1.2	-19.6	0.1		2
40	0.00	0.4	-43.4	-0.1		3
40	48.32	0.7	-27.5	-0.0		3
40	102.00	1.2	-9.8	0.1		3
40	0.00	0.4	-26.1	-0.0		4
40	48.32	0.7	-16.5	-0.0		4
40	102.00	1.2	-5.9	0.0		4
41	0.00	0.4	0.0	-0.6	1	
41	48.32	0.7	0.0	-0.0	1	
41	102.00	1.2	0.0	0.6	1	
41	0.00	-0.0	-0.0	-0.0	2	
41	48.32	-0.0	-0.0	-0.0	2	
41	102.00	-0.0	-0.0	-0.0	2	
41	0.00	-0.0	-87.5	-0.1	3	
41	48.32	-0.0	-55.1	-0.0	3	
41	102.00	-0.0	-19.0	0.1	3	
41	0.00	0.5	-131.2	-1.0		1
41	48.32	1.0	-82.6	-0.0		1
41	102.00	1.5	-28.6	1.0		1
41	0.00	0.4	-87.5	-0.7		2
41	48.32	0.7	-55.1	-0.0		2
41	102.00	1.2	-19.0	0.7		2
41	0.00	0.4	-43.7	-0.7		3
41	48.32	0.7	-27.5	-0.0		3
41	102.00	1.2	-9.5	0.7		3
41	0.00	0.4	-26.2	-0.7		4
41	48.32	0.7	-16.5	-0.0		4
41	102.00	1.2	-5.7	0.7		4
42	0.00	0.4	0.0	-1.1	1	
42	48.32	0.8	0.0	-0.0	1	
42	102.00	1.2	0.0	1.1	1	
42	0.00	-0.0	-0.0	-0.0	2	
42	48.32	-0.0	-0.0	-0.0	2	
42	102.00	-0.0	-0.0	-0.0	2	
42	0.00	0.0	-92.2	-0.1	3	
42	48.32	0.0	-56.5	-0.0	3	
42	102.00	0.0	-16.9	0.1	3	
42	0.00	0.5	-138.3	-1.5		1
42	48.32	1.0	-84.8	-0.1		1
42	102.00	1.6	-25.3	1.5		1
42	0.00	0.4	-92.2	-1.2		2
42	48.32	0.8	-56.5	-0.1		2
42	102.00	1.2	-16.9	1.2		2
42	0.00	0.4	-46.1	-1.1		3
42	48.32	0.8	-28.3	-0.1		3
42	102.00	1.2	-8.4	1.1		3
42	0.00	0.4	-27.7	-1.1		4
42	48.32	0.8	-17.0	-0.1		4
42	102.00	1.2	-5.1	1.1		4
43	0.00	0.5	0.0	-1.2	1	
43	48.32	0.9	0.0	-0.1	1	
43	102.00	1.3	0.0	1.2	1	
43	0.00	-0.0	-0.0	-0.0	2	
43	48.32	-0.0	-0.0	-0.0	2	
43	102.00	-0.0	-0.0	-0.0	2	
43	0.00	-0.0	-101.6	-0.1	3	
43	48.32	-0.0	-59.6	-0.0	3	
43	102.00	-0.0	-12.8	0.1	3	
43	0.00	0.6	-152.5	-1.7		1
43	48.32	1.1	-89.3	-0.1		1
43	102.00	1.7	-19.2	1.7		1
43	0.00	0.5	-101.6	-1.3		2
43	48.32	0.9	-59.5	-0.1		2
43	102.00	1.3	-12.8	1.3		2
43	0.00	0.5	-50.8	-1.2		3
43	48.32	0.9	-29.8	-0.1		3
43	102.00	1.3	-6.4	1.3		3
43	0.00	0.5	-30.5	-1.2		4
43	48.32	0.9	-17.9	-0.1		4
43	102.00	1.3	-3.8	1.2		4
44	0.00	-0.2	0.0	-1.2	1	
44	48.32	0.2	0.0	-0.2	1	
44	102.00	0.6	-0.0	1.0	1	
44	0.00	-0.0	-0.0	-0.0	2	
44	48.32	-0.0	-0.0	-0.0	2	
44	102.00	-0.0	-0.0	-0.0	2	

44	0.00	-0.0	-116.7	-0.1	3	
44	48.32	-0.0	-64.3	-0.0	3	
44	102.00	-0.0	-6.0	0.1	3	
44	0.00	-0.3	-175.0	-1.7		1
44	48.32	0.2	-96.4	-0.2		1
44	102.00	0.7	-9.1	1.5		1
44	0.00	-0.2	-116.7	-1.3		2
44	48.32	0.2	-64.3	-0.2		2
44	102.00	0.6	-6.0	1.1		2
44	0.00	-0.2	-58.3	-1.3		3
44	48.32	0.2	-32.1	-0.2		3
44	102.00	0.6	-3.0	1.1		3
44	0.00	-0.2	-35.0	-1.3		4
44	48.32	0.2	-19.3	-0.2		4
44	102.00	0.6	-1.8	1.1		4
65	0.00	-2.5	0.0	-0.1	1	
65	12.79	-2.4	0.0	-0.0	1	
65	27.00	-2.3	0.0	0.0	1	
65	0.00	-0.0	-0.0	-0.0	2	
65	12.79	-0.0	-0.0	-0.0	2	
65	27.00	-0.0	-0.0	-0.0	2	
65	0.00	0.0	-1181.4	0.1	3	
65	12.79	0.0	-1060.4	0.0	3	
65	27.00	0.0	-926.0	-0.0	3	
65	0.00	-3.2	-1772.2	-0.0		1
65	12.79	-3.1	-1590.6	-0.0		1
65	27.00	-2.9	-1388.9	0.0		1
65	0.00	-2.5	-1181.4	-0.0		2
65	12.79	-2.4	-1060.4	-0.0		2
65	27.00	-2.3	-926.0	0.0		2
65	0.00	-2.5	-590.7	-0.1		3
65	12.79	-2.4	-530.2	-0.0		3
65	27.00	-2.3	-463.0	0.0		3
65	0.00	-2.5	-354.4	-0.1		4
65	12.79	-2.4	-318.1	-0.0		4
65	27.00	-2.3	-277.8	0.0		4
67	0.00	-2.1	0.0	0.0	1	
67	48.32	-1.8	0.0	0.0	1	
67	102.00	-1.3	0.0	0.0	1	
67	0.00	-0.0	-0.0	-0.0	2	
67	48.32	-0.0	-0.0	-0.0	2	
67	102.00	-0.0	-0.0	-0.0	2	
67	0.00	0.0	-918.9	-0.0	3	
67	48.32	0.0	-470.1	0.0	3	
67	102.00	0.0	28.5	0.1	3	
67	0.00	-2.8	-1378.3	-0.0		1
67	48.32	-2.3	-705.2	0.1		1
67	102.00	-1.7	42.7	0.2		1
67	0.00	-2.1	-918.9	-0.0		2
67	48.32	-1.8	-470.1	0.1		2
67	102.00	-1.3	28.5	0.1		2
67	0.00	-2.1	-459.4	0.0		3
67	48.32	-1.8	-235.1	0.0		3
67	102.00	-1.3	14.3	0.1		3
67	0.00	-2.1	-275.7	0.0		4
67	48.32	-1.8	-141.0	0.0		4
67	102.00	-1.3	8.6	0.1		4
68	0.00	-2.1	0.0	-0.0	1	
68	48.32	-1.8	0.0	-0.0	1	
68	102.00	-1.3	0.0	-0.0	1	
68	0.00	-0.0	-0.0	-0.0	2	
68	48.32	-0.0	-0.0	-0.0	2	
68	102.00	-0.0	-0.0	-0.0	2	
68	0.00	0.0	-918.9	0.0	3	
68	48.32	0.0	-470.1	-0.0	3	
68	102.00	0.0	28.5	-0.1	3	
68	0.00	-2.8	-1378.3	0.0		1
68	48.32	-2.3	-705.2	-0.1		1
68	102.00	-1.7	42.7	-0.2		1
68	0.00	-2.1	-918.9	0.0		2
68	48.32	-1.8	-470.1	-0.1		2
68	102.00	-1.3	28.5	-0.1		2
68	0.00	-2.1	-459.4	-0.0		3
68	48.32	-1.8	-235.1	-0.0		3
68	102.00	-1.3	14.3	-0.1		3
68	0.00	-2.1	-275.7	-0.0		4
68	48.32	-1.8	-141.0	-0.0		4
68	102.00	-1.3	8.6	-0.1		4
70	0.00	-2.5	0.0	0.1	1	
70	12.79	-2.4	0.0	0.0	1	
70	27.00	-2.3	0.0	-0.0	1	
70	0.00	-0.0	-0.0	-0.0	2	
70	12.79	-0.0	-0.0	-0.0	2	
70	27.00	-0.0	-0.0	-0.0	2	
70	0.00	0.0	-1181.4	-0.1	3	
70	12.79	0.0	-1060.4	-0.0	3	
70	27.00	0.0	-926.0	0.0	3	
70	0.00	-3.2	-1772.2	0.0		1
70	12.79	-3.1	-1590.6	0.0		1
70	27.00	-2.9	-1388.9	-0.0		1
70	0.00	-2.5	-1181.4	0.0		2
70	12.79	-2.4	-1060.4	0.0		2
70	27.00	-2.3	-926.0	-0.0		2
70	0.00	-2.5	-590.7	0.1		3
70	12.79	-2.4	-530.2	0.0		3
70	27.00	-2.3	-463.0	-0.0		3
70	0.00	-2.5	-354.4	0.1		4
70	12.79	-2.4	-318.1	0.0		4
70	27.00	-2.3	-277.8	-0.0		4
91	0.00	-0.2	0.0	-1.4	1	
91	48.32	0.1	0.0	-0.2	1	
91	102.00	0.6	0.0	1.2	1	
91	0.00	-0.0	-0.0	-0.0	2	
91	48.32	-0.0	-0.0	-0.0	2	
91	102.00	-0.0	-0.0	-0.0	2	
91	0.00	-0.0	-128.1	-0.0	3	
91	48.32	-0.0	-70.5	-0.0	3	
91	102.00	-0.0	-6.5	0.0	3	
91	0.00	-0.3	-192.1	-1.8		1
91	48.32	0.2	-105.7	-0.2		1
91	102.00	0.7	-9.7	1.5		1
91	0.00	-0.3	-128.1	-1.4		2
91	48.32	0.1	-70.5	-0.2		2
91	102.00	0.5	-6.5	1.2		2
91	0.00	-0.2	-64.0	-1.4		3
91	48.32	0.1	-35.2	-0.2		3
91	102.00	0.6	-3.2	1.2		3
91	0.00	-0.2	-38.4	-1.4		4

91	48.32	0.1	-21.1	-0.2		4
91	102.00	0.6	-1.9	1.2		4
92	0.00	0.5	0.0	-1.3	1	
92	48.32	0.9	0.0	-0.1	1	
92	102.00	1.3	0.0	1.3	1	
92	0.00	-0.0	-0.0	-0.0	2	
92	48.32	-0.0	-0.0	-0.0	2	
92	102.00	-0.0	-0.0	-0.0	2	
92	0.00	-0.0	-110.4	-0.0	3	
92	48.32	-0.0	-64.7	-0.0	3	
92	102.00	-0.0	-14.0	0.0	3	
92	0.00	0.6	-165.6	-1.7		1
92	48.32	1.1	-97.1	-0.1		1
92	102.00	1.7	-20.9	1.7		1
92	0.00	0.5	-110.4	-1.3		2
92	48.32	0.9	-64.7	-0.1		2
92	102.00	1.3	-14.0	1.3		2
92	0.00	0.5	-55.2	-1.3		3
92	48.32	0.9	-32.4	-0.1		3
92	102.00	1.3	-7.0	1.3		3
92	0.00	0.5	-33.1	-1.3		4
92	48.32	0.9	-19.4	-0.1		4
92	102.00	1.3	-4.2	1.3		4
93	0.00	0.4	-0.0	-1.1	1	
93	48.32	0.8	0.0	-0.1	1	
93	102.00	1.2	0.0	1.1	1	
93	0.00	-0.0	-0.0	-0.0	2	
93	48.32	-0.0	-0.0	-0.0	2	
93	102.00	-0.0	-0.0	-0.0	2	
93	0.00	0.0	-98.8	-0.0	3	
93	48.32	0.0	-60.8	-0.0	3	
93	102.00	0.0	-18.7	0.0	3	
93	0.00	0.5	-148.1	-1.4		1
93	48.32	1.0	-91.2	-0.1		1
93	102.00	1.6	-28.0	1.5		1
93	0.00	0.4	-98.8	-1.1		2
93	48.32	0.8	-60.8	-0.1		2
93	102.00	1.2	-18.7	1.1		2
93	0.00	0.4	-49.4	-1.1		3
93	48.32	0.8	-30.4	-0.1		3
93	102.00	1.2	-9.3	1.1		3
93	0.00	0.4	-29.6	-1.1		4
93	48.32	0.8	-18.2	-0.1		4
93	102.00	1.2	-5.6	1.1		4
94	0.00	0.4	-0.0	-0.6	1	
94	48.32	0.7	0.0	-0.0	1	
94	102.00	1.2	0.0	0.6	1	
94	0.00	-0.0	-0.0	-0.0	2	
94	48.32	-0.0	-0.0	-0.0	2	
94	102.00	-0.0	-0.0	-0.0	2	
94	0.00	-0.0	-92.1	-0.0	3	
94	48.32	-0.0	-58.6	-0.0	3	
94	102.00	-0.0	-21.3	0.0	3	
94	0.00	0.5	-138.2	-0.8		1
94	48.32	1.0	-87.9	-0.0		1
94	102.00	1.5	-31.9	0.8		1
94	0.00	0.4	-92.1	-0.6		2
94	48.32	0.7	-58.6	-0.0		2
94	102.00	1.2	-21.3	0.6		2
94	0.00	0.4	-46.1	-0.6		3
94	48.32	0.7	-29.3	-0.0		3
94	102.00	1.2	-10.6	0.6		3
94	0.00	0.4	-27.6	-0.6		4
94	48.32	0.7	-17.6	-0.0		4
94	102.00	1.2	-6.4	0.6		4
95	0.00	0.4	-0.0	0.0	1	
95	48.32	0.7	0.0	0.0	1	
95	102.00	1.2	0.0	0.0	1	
95	0.00	-0.0	-0.0	-0.0	2	
95	48.32	-0.0	-0.0	-0.0	2	
95	102.00	-0.0	-0.0	-0.0	2	
95	0.00	-0.0	-90.0	-0.0	3	
95	48.32	-0.0	-57.8	-0.0	3	
95	102.00	-0.0	-22.1	-0.0	3	
95	0.00	0.5	-135.0	0.0		1
95	48.32	1.0	-86.8	0.0		1
95	102.00	1.5	-33.2	0.0		1
95	0.00	0.4	-90.0	0.0		2
95	48.32	0.7	-57.8	0.0		2
95	102.00	1.2	-22.1	0.0		2
95	0.00	0.4	-45.0	0.0		3
95	48.32	0.7	-28.9	0.0		3
95	102.00	1.2	-11.1	0.0		3
95	0.00	0.4	-27.0	0.0		4
95	48.32	0.7	-17.4	0.0		4
95	102.00	1.2	-6.6	0.0		4
96	0.00	0.4	-0.0	0.6	1	
96	48.32	0.7	0.0	0.0	1	
96	102.00	1.2	0.0	-0.6	1	
96	0.00	-0.0	-0.0	-0.0	2	
96	48.32	-0.0	-0.0	-0.0	2	
96	102.00	-0.0	-0.0	-0.0	2	
96	0.00	-0.0	-92.1	0.0	3	
96	48.32	-0.0	-58.6	0.0	3	
96	102.00	-0.0	-21.3	-0.0	3	
96	0.00	0.5	-138.2	0.8		1
96	48.32	1.0	-87.9	0.0		1
96	102.00	1.5	-31.9	-0.8		1
96	0.00	0.4	-92.1	0.6		2
96	48.32	0.7	-58.6	0.0		2
96	102.00	1.2	-21.3	-0.6		2
96	0.00	0.4	-46.1	0.6		3
96	48.32	0.7	-29.3	0.0		3
96	102.00	1.2	-10.6	-0.6		3
96	0.00	0.4	-27.6	0.6		4
96	48.32	0.7	-17.6	0.0		4
96	102.00	1.2	-6.4	-0.6		4
97	0.00	0.4	-0.0	1.1	1	
97	48.32	0.8	0.0	0.1	1	
97	102.00	1.2	0.0	-1.1	1	
97	0.00	-0.0	-0.0	-0.0	2	
97	48.32	-0.0	-0.0	-0.0	2	
97	102.00	-0.0	-0.0	-0.0	2	
97	0.00	0.0	-98.8	0.0	3	
97	48.32	0.0	-60.8	0.0	3	
97	102.00	0.0	-18.7	-0.0	3	
97	0.00	0.5	-148.1	1.4		1
97	48.32	1.0	-91.2	0.1		1

97	102.00	1.6	-28.0	-1.5		1
97	0.00	0.4	-98.8	1.1		2
97	48.32	0.8	-60.8	0.1		2
97	102.00	1.2	-18.7	-1.1		2
97	0.00	0.4	-49.4	1.1		3
97	48.32	0.8	-30.4	0.1		3
97	102.00	1.2	-9.3	-1.1		3
97	0.00	0.4	-29.6	1.1		4
97	48.32	0.8	-18.2	0.1		4
97	102.00	1.2	-5.6	-1.1		4
98	0.00	0.5	0.0	1.3	1	
98	48.32	0.9	0.0	0.1	1	
98	102.00	1.3	0.0	-1.3	1	
98	0.00	-0.0	-0.0	-0.0	2	
98	48.32	-0.0	-0.0	-0.0	2	
98	102.00	-0.0	-0.0	-0.0	2	
98	0.00	-0.0	-110.4	0.0	3	
98	48.32	-0.0	-64.7	0.0	3	
98	102.00	-0.0	-14.0	-0.0	3	
98	0.00	0.6	-165.6	1.7		1
98	48.32	1.1	-97.1	0.1		1
98	102.00	1.7	-20.9	-1.7		1
98	0.00	0.5	-110.4	1.3		2
98	48.32	0.9	-64.7	0.1		2
98	102.00	1.3	-14.0	-1.3		2
98	0.00	0.5	-55.2	1.3		3
98	48.32	0.9	-32.4	0.1		3
98	102.00	1.3	-7.0	-1.3		3
98	0.00	0.5	-33.1	1.3		4
98	48.32	0.9	-19.4	0.1		4
98	102.00	1.3	-4.2	-1.3		4
99	0.00	-0.2	0.0	1.4	1	
99	48.32	0.1	0.0	0.2	1	
99	102.00	0.6	0.0	-1.2	1	
99	0.00	-0.0	-0.0	-0.0	2	
99	48.32	-0.0	-0.0	-0.0	2	
99	102.00	-0.0	-0.0	-0.0	2	
99	0.00	-0.0	-128.1	0.0	3	
99	48.32	-0.0	-70.5	0.0	3	
99	102.00	-0.0	-6.5	-0.0	3	
99	0.00	-0.3	-192.1	1.8		1
99	48.32	0.2	-105.7	0.2		1
99	102.00	0.7	-9.7	-1.5		1
99	0.00	-0.3	-128.1	1.4		2
99	48.32	0.1	-70.5	0.2		2
99	102.00	0.5	-6.5	-1.2		2
99	0.00	-0.2	-64.0	1.4		3
99	48.32	0.1	-35.2	0.2		3
99	102.00	0.6	-3.2	-1.2		3
99	0.00	-0.2	-38.4	1.4		4
99	48.32	0.1	-21.1	0.2		4
99	102.00	0.6	-1.9	-1.2		4
100	0.00	-0.2	0.0	1.2	1	
100	48.32	0.2	0.0	0.2	1	
100	102.00	0.6	-0.0	-1.0	1	
100	0.00	-0.0	-0.0	-0.0	2	
100	48.32	-0.0	-0.0	-0.0	2	
100	102.00	-0.0	-0.0	-0.0	2	
100	0.00	-0.0	-116.7	0.1	3	
100	48.32	-0.0	-64.3	0.0	3	
100	102.00	-0.0	-6.0	-0.1	3	
100	0.00	-0.3	-175.0	1.7		1
100	48.32	0.2	-96.4	0.2		1
100	102.00	0.7	-9.1	-1.5		1
100	0.00	-0.2	-116.7	1.3		2
100	48.32	0.2	-64.3	0.2		2
100	102.00	0.6	-6.0	-1.1		2
100	0.00	-0.2	-58.3	1.3		3
100	48.32	0.2	-32.1	0.2		3
100	102.00	0.6	-3.0	-1.1		3
100	0.00	-0.2	-35.0	1.3		4
100	48.32	0.2	-19.3	0.2		4
100	102.00	0.6	-1.8	-1.1		4
101	0.00	0.5	0.0	1.2	1	
101	48.32	0.9	0.0	0.1	1	
101	102.00	1.3	0.0	-1.2	1	
101	0.00	-0.0	-0.0	-0.0	2	
101	48.32	-0.0	-0.0	-0.0	2	
101	102.00	-0.0	-0.0	-0.0	2	
101	0.00	-0.0	-101.6	0.1	3	
101	48.32	-0.0	-59.6	0.0	3	
101	102.00	-0.0	-12.8	-0.1	3	
101	0.00	0.6	-152.5	1.7		1
101	48.32	1.1	-89.3	0.1		1
101	102.00	1.7	-19.2	-1.7		1
101	0.00	0.5	-101.6	1.3		2
101	48.32	0.9	-59.5	0.1		2
101	102.00	1.3	-12.8	-1.3		2
101	0.00	0.5	-50.8	1.2		3
101	48.32	0.9	-29.8	0.1		3
101	102.00	1.3	-6.4	-1.3		3
101	0.00	0.5	-30.5	1.2		4
101	48.32	0.9	-17.9	0.1		4
101	102.00	1.3	-3.8	-1.2		4
102	0.00	0.4	0.0	1.1	1	
102	48.32	0.8	0.0	0.0	1	
102	102.00	1.2	0.0	-1.1	1	
102	0.00	-0.0	-0.0	-0.0	2	
102	48.32	-0.0	-0.0	-0.0	2	
102	102.00	-0.0	-0.0	-0.0	2	
102	0.00	0.0	-92.2	0.1	3	
102	48.32	0.0	-56.5	0.0	3	
102	102.00	0.0	-16.9	-0.1	3	
102	0.00	0.5	-138.3	1.5		1
102	48.32	1.0	-84.8	0.1		1
102	102.00	1.6	-25.3	-1.5		1
102	0.00	0.4	-92.2	1.2		2
102	48.32	0.8	-56.5	0.1		2
102	102.00	1.2	-16.9	-1.2		2
102	0.00	0.4	-46.1	1.1		3
102	48.32	0.8	-28.3	0.1		3
102	102.00	1.2	-8.4	-1.1		3
102	0.00	0.4	-27.7	1.1		4
102	48.32	0.8	-17.0	0.1		4
102	102.00	1.2	-5.1	-1.1		4
103	0.00	0.4	0.0	0.6	1	
103	48.32	0.7	0.0	0.0	1	
103	102.00	1.2	0.0	-0.6	1	

103	0.00	-0.0	-0.0	-0.0	2	
103	48.32	-0.0	-0.0	-0.0	2	
103	102.00	-0.0	-0.0	-0.0	2	
103	0.00	-0.0	-87.5	0.1	3	
103	48.32	-0.0	-55.1	0.0	3	
103	102.00	-0.0	-19.0	-0.1	3	
103	0.00	0.5	-131.2	1.0		1
103	48.32	1.0	-82.6	0.0		1
103	102.00	1.5	-28.6	-1.0		1
103	0.00	0.4	-87.5	0.7		2
103	48.32	0.7	-55.1	0.0		2
103	102.00	1.2	-19.0	-0.7		2
103	0.00	0.4	-43.7	0.7		3
103	48.32	0.7	-27.5	0.0		3
103	102.00	1.2	-9.5	-0.7		3
103	0.00	0.4	-26.2	0.7		4
103	48.32	0.7	-16.5	0.0		4
103	102.00	1.2	-5.7	-0.7		4
104	0.00	0.4	0.0	0.0	1	
104	48.32	0.7	0.0	0.0	1	
104	102.00	1.2	0.0	-0.0	1	
104	0.00	-0.0	-0.0	-0.0	2	
104	48.32	-0.0	-0.0	-0.0	2	
104	102.00	-0.0	-0.0	-0.0	2	
104	0.00	-0.0	-86.9	0.1	3	
104	48.32	-0.0	-55.0	0.0	3	
104	102.00	-0.0	-19.6	-0.1	3	
104	0.00	0.5	-130.3	0.1		1
104	48.32	1.0	-82.5	0.0		1
104	102.00	1.5	-29.4	-0.1		1
104	0.00	0.4	-86.9	0.1		2
104	48.32	0.7	-55.0	0.0		2
104	102.00	1.2	-19.6	-0.1		2
104	0.00	0.4	-43.4	0.1		3
104	48.32	0.7	-27.5	0.0		3
104	102.00	1.2	-9.8	-0.1		3
104	0.00	0.4	-26.1	0.0		4
104	48.32	0.7	-16.5	0.0		4
104	102.00	1.2	-5.9	-0.0		4
105	0.00	0.4	0.0	-0.6	1	
105	48.32	0.7	0.0	-0.0	1	
105	102.00	1.2	0.0	0.6	1	
105	0.00	-0.0	-0.0	-0.0	2	
105	48.32	-0.0	-0.0	-0.0	2	
105	102.00	-0.0	-0.0	-0.0	2	
105	0.00	-0.0	-90.3	0.1	3	
105	48.32	-0.0	-56.4	0.0	3	
105	102.00	-0.0	-18.7	-0.1	3	
105	0.00	0.5	-135.4	-0.7		1
105	48.32	1.0	-84.6	-0.0		1
105	102.00	1.5	-28.1	0.7		1
105	0.00	0.4	-90.3	-0.5		2
105	48.32	0.7	-56.4	-0.0		2
105	102.00	1.2	-18.7	0.5		2
105	0.00	0.4	-45.1	-0.6		3
105	48.32	0.7	-28.2	-0.0		3
105	102.00	1.2	-9.4	0.6		3
105	0.00	0.4	-27.1	-0.6		4
105	48.32	0.7	-16.9	-0.0		4
105	102.00	1.2	-5.6	0.6		4
106	0.00	0.4	0.0	-1.1	1	
106	48.32	0.8	0.0	-0.0	1	
106	102.00	1.2	0.0	1.1	1	
106	0.00	-0.0	-0.0	-0.0	2	
106	48.32	-0.0	-0.0	-0.0	2	
106	102.00	-0.0	-0.0	-0.0	2	
106	0.00	-0.0	-97.9	0.1	3	
106	48.32	-0.0	-59.2	0.0	3	
106	102.00	-0.0	-16.3	-0.1	3	
106	0.00	0.5	-146.8	-1.3		1
106	48.32	1.0	-88.8	-0.1		1
106	102.00	1.5	-24.4	1.3		1
106	0.00	0.4	-97.9	-1.0		2
106	48.32	0.8	-59.2	-0.0		2
106	102.00	1.2	-16.3	1.0		2
106	0.00	0.4	-48.9	-1.0		3
106	48.32	0.8	-29.6	-0.0		3
106	102.00	1.2	-8.1	1.0		3
106	0.00	0.4	-29.4	-1.0		4
106	48.32	0.8	-17.8	-0.0		4
106	102.00	1.2	-4.9	1.0		4
107	0.00	0.5	0.0	-1.2	1	
107	48.32	0.9	0.0	-0.1	1	
107	102.00	1.3	0.0	1.2	1	
107	0.00	-0.0	-0.0	-0.0	2	
107	48.32	-0.0	-0.0	-0.0	2	
107	102.00	-0.0	-0.0	-0.0	2	
107	0.00	-0.0	-110.2	0.1	3	
107	48.32	-0.0	-63.7	0.0	3	
107	102.00	-0.0	-12.0	-0.1	3	
107	0.00	0.6	-165.2	-1.5		1
107	48.32	1.1	-95.5	-0.1		1
107	102.00	1.7	-18.0	1.5		1
107	0.00	0.5	-110.2	-1.2		2
107	48.32	0.9	-63.7	-0.1		2
107	102.00	1.3	-12.0	1.2		2
107	0.00	0.5	-55.1	-1.2		3
107	48.32	0.9	-31.8	-0.1		3
107	102.00	1.3	-6.0	1.2		3
107	0.00	0.5	-33.0	-1.2		4
107	48.32	0.9	-19.1	-0.1		4
107	102.00	1.3	-3.6	1.2		4
108	0.00	-0.2	0.0	-1.3	1	
108	48.32	0.2	0.0	-0.2	1	
108	102.00	0.6	0.0	1.1	1	
108	0.00	-0.0	-0.0	-0.0	2	
108	48.32	-0.0	-0.0	-0.0	2	
108	102.00	-0.0	-0.0	-0.0	2	
108	0.00	0.0	-128.1	0.0	3	
108	48.32	0.0	-69.9	0.0	3	
108	102.00	0.0	-5.3	-0.0	3	
108	0.00	-0.3	-192.2	-1.6		1
108	48.32	0.2	-104.9	-0.2		1
108	102.00	0.8	-7.9	1.4		1
108	0.00	-0.2	-128.1	-1.3		2
108	48.32	0.2	-69.9	-0.2		2
108	102.00	0.6	-5.3	1.1		2
108	0.00	-0.2	-64.1	-1.3		3

108	48.32	0.2	-35.0	-0.2		3
108	102.00	0.6	-2.6	1.1		3
108	0.00	-0.2	-38.4	-1.3		4
108	48.32	0.2	-21.0	-0.2		4
108	102.00	0.6	-1.6	1.1		4
129	0.00	-2.5	0.0	0.4	1	
129	12.79	-2.4	0.0	0.0	1	
129	27.00	-2.3	0.0	-0.4	1	
129	0.00	-0.0	-0.0	-0.0	2	
129	12.79	-0.0	-0.0	-0.0	2	
129	27.00	-0.0	-0.0	-0.0	2	
129	0.00	0.0	-1069.9	-0.3	3	
129	12.79	0.0	-960.0	-0.1	3	
129	27.00	0.0	-838.0	0.2	3	
129	0.00	-3.3	-1604.8	0.0		1
129	12.79	-3.2	-1440.0	-0.1		1
129	27.00	-3.0	-1256.9	-0.2		1
129	0.00	-2.5	-1069.9	0.1		2
129	12.79	-2.4	-960.0	-0.1		2
129	27.00	-2.3	-838.0	-0.2		2
129	0.00	-2.5	-534.9	0.2		3
129	12.79	-2.4	-480.0	-0.0		3
129	27.00	-2.3	-419.0	-0.3		3
129	0.00	-2.5	-320.9	0.3		4
129	12.79	-2.4	-288.0	-0.0		4
129	27.00	-2.3	-251.4	-0.3		4
131	0.00	-2.2	0.0	-0.4	1	
131	48.32	-1.8	0.0	0.1	1	
131	102.00	-1.4	-0.0	0.7	1	
131	0.00	-0.0	-0.0	-0.0	2	
131	48.32	-0.0	-0.0	-0.0	2	
131	102.00	-0.0	-0.0	-0.0	2	
131	0.00	0.0	-831.7	0.2	3	
131	48.32	0.0	-425.7	-0.1	3	
131	102.00	0.0	25.4	-0.4	3	
131	0.00	-2.9	-1247.5	-0.2		1
131	48.32	-2.4	-638.5	0.0		1
131	102.00	-1.8	38.1	0.3		1
131	0.00	-2.2	-831.7	-0.2		2
131	48.32	-1.8	-425.7	0.0		2
131	102.00	-1.4	25.4	0.3		2
131	0.00	-2.2	-415.8	-0.3		3
131	48.32	-1.8	-212.8	0.1		3
131	102.00	-1.4	12.7	0.5		3
131	0.00	-2.2	-249.5	-0.4		4
131	48.32	-1.8	-127.7	0.1		4
131	102.00	-1.4	7.6	0.6		4
132	0.00	-1.4	-0.0	1.6	1	
132	48.32	-1.0	-0.0	-1.3	1	
132	102.00	-0.6	-0.0	-4.6	1	
132	0.00	-0.0	-0.0	-0.0	2	
132	48.32	-0.0	-0.0	-0.0	2	
132	102.00	-0.0	-0.0	-0.0	2	
132	0.00	-0.0	-632.1	0.4	3	
132	48.32	-0.0	-356.9	0.0	3	
132	102.00	-0.0	-51.1	-0.4	3	
132	0.00	-1.8	-948.1	2.7		1
132	48.32	-1.3	-535.3	-1.7		1
132	102.00	-0.8	-76.7	-6.6		1
132	0.00	-1.4	-632.1	2.0		2
132	48.32	-1.0	-356.9	-1.3		2
132	102.00	-0.6	-51.1	-5.0		2
132	0.00	-1.4	-316.1	1.8		3
132	48.32	-1.0	-178.5	-1.3		3
132	102.00	-0.6	-25.6	-4.8		3
132	0.00	-1.4	-189.6	1.7		4
132	48.32	-1.0	-107.1	-1.3		4
132	102.00	-0.6	-15.3	-4.7		4
134	0.00	-1.7	-0.0	0.2	1	
134	12.79	-1.6	-0.0	0.7	1	
134	27.00	-1.5	-0.0	1.2	1	
134	0.00	-0.0	-0.0	-0.0	2	
134	12.79	-0.0	-0.0	-0.0	2	
134	27.00	-0.0	-0.0	-0.0	2	
134	0.00	-0.0	-783.3	-0.8	3	
134	12.79	-0.0	-713.3	-0.2	3	
134	27.00	-0.0	-635.6	0.4	3	
134	0.00	-2.2	-1175.0	-0.9		1
134	12.79	-2.1	-1070.1	0.6		1
134	27.00	-1.9	-953.4	2.2		1
134	0.00	-1.7	-783.4	-0.6		2
134	12.79	-1.6	-713.4	0.5		2
134	27.00	-1.5	-635.6	1.6		2
134	0.00	-1.7	-391.7	-0.2		3
134	12.79	-1.6	-356.7	0.6		3
134	27.00	-1.5	-317.8	1.4		3
134	0.00	-1.7	-235.0	-0.0		4
134	12.79	-1.6	-214.0	0.6		4
134	27.00	-1.5	-190.7	1.3		4
155	0.00	-0.3	0.0	-1.7	1	
155	48.32	0.1	0.0	-0.2	1	
155	102.00	0.5	-0.0	1.5	1	
155	0.00	-0.0	-0.0	-0.0	2	
155	48.32	-0.0	-0.0	-0.0	2	
155	102.00	-0.0	-0.0	-0.0	2	
155	0.00	0.0	-116.0	0.2	3	
155	48.32	0.0	-63.2	0.0	3	
155	102.00	0.0	-4.5	-0.2	3	
155	0.00	-0.3	-174.1	-1.9		1
155	48.32	0.2	-94.8	-0.2		1
155	102.00	0.7	-6.7	1.6		1
155	0.00	-0.3	-116.0	-1.5		2
155	48.32	0.1	-63.2	-0.2		2
155	102.00	0.5	-4.5	1.3		2
155	0.00	-0.3	-58.0	-1.6		3
155	48.32	0.1	-31.6	-0.2		3
155	102.00	0.5	-2.2	1.4		3
155	0.00	-0.3	-34.8	-1.6		4
155	48.32	0.1	-19.0	-0.2		4
155	102.00	0.5	-1.3	1.4		4
156	0.00	0.5	0.0	-1.7	1	
156	48.32	0.9	0.0	-0.1	1	
156	102.00	1.3	-0.0	1.7	1	
156	0.00	-0.0	-0.0	-0.0	2	
156	48.32	-0.0	-0.0	-0.0	2	
156	102.00	-0.0	-0.0	-0.0	2	
156	0.00	-0.0	-99.1	0.2	3	
156	48.32	-0.0	-57.4	0.0	3	

156	102.00	-0.0	-10.9	-0.2	3	
156	0.00	0.6	-148.7	-1.8		1
156	48.32	1.1	-86.0	-0.1		1
156	102.00	1.7	-16.4	1.8		1
156	0.00	0.5	-99.1	-1.4		2
156	48.32	0.9	-57.4	-0.1		2
156	102.00	1.3	-10.9	1.4		2
156	0.00	0.5	-49.6	-1.5		3
156	48.32	0.9	-28.7	-0.1		3
156	102.00	1.3	-5.5	1.6		3
156	0.00	0.5	-29.7	-1.6		4
156	48.32	0.9	-17.2	-0.1		4
156	102.00	1.3	-3.3	1.6		4
157	0.00	0.4	0.0	-1.5	1	
157	48.32	0.8	0.0	-0.1	1	
157	102.00	1.2	0.0	1.5	1	
157	0.00	-0.0	-0.0	-0.0	2	
157	48.32	-0.0	-0.0	-0.0	2	
157	102.00	-0.0	-0.0	-0.0	2	
157	0.00	-0.0	-86.8	0.2	3	
157	48.32	-0.0	-53.1	0.0	3	
157	102.00	-0.0	-15.7	-0.2	3	
157	0.00	0.5	-130.2	-1.6		1
157	48.32	1.0	-79.7	-0.1		1
157	102.00	1.6	-23.6	1.6		1
157	0.00	0.4	-86.8	-1.3		2
157	48.32	0.8	-53.1	-0.1		2
157	102.00	1.2	-15.7	1.3		2
157	0.00	0.4	-43.4	-1.4		3
157	48.32	0.8	-26.6	-0.1		3
157	102.00	1.2	-7.9	1.4		3
157	0.00	0.4	-26.0	-1.4		4
157	48.32	0.8	-15.9	-0.1		4
157	102.00	1.2	-4.7	1.4		4
158	0.00	0.4	0.0	-1.0	1	
158	48.32	0.7	0.0	-0.1	1	
158	102.00	1.2	0.0	1.0	1	
158	0.00	-0.0	-0.0	-0.0	2	
158	48.32	-0.0	-0.0	-0.0	2	
158	102.00	-0.0	-0.0	-0.0	2	
158	0.00	-0.0	-78.2	0.3	3	
158	48.32	-0.0	-50.3	0.0	3	
158	102.00	-0.0	-19.3	-0.3	3	
158	0.00	0.5	-117.3	-0.9		1
158	48.32	1.0	-75.5	-0.0		1
158	102.00	1.5	-29.0	0.9		1
158	0.00	0.4	-78.2	-0.7		2
158	48.32	0.7	-50.3	-0.0		2
158	102.00	1.2	-19.3	0.7		2
158	0.00	0.4	-39.1	-0.9		3
158	48.32	0.7	-25.2	-0.0		3
158	102.00	1.2	-9.7	0.9		3
158	0.00	0.4	-23.5	-0.9		4
158	48.32	0.7	-15.1	-0.0		4
158	102.00	1.2	-5.8	0.9		4
159	0.00	0.4	-0.0	-0.3	1	
159	48.32	0.7	-0.0	-0.0	1	
159	102.00	1.2	0.0	0.3	1	
159	0.00	-0.0	-0.0	-0.0	2	
159	48.32	-0.0	-0.0	-0.0	2	
159	102.00	-0.0	-0.0	-0.0	2	
159	0.00	0.0	-73.0	0.3	3	
159	48.32	0.0	-48.7	0.0	3	
159	102.00	0.0	-21.8	-0.3	3	
159	0.00	0.5	-109.5	0.1		1
159	48.32	1.0	-73.1	0.0		1
159	102.00	1.5	-32.7	-0.1		1
159	0.00	0.4	-73.0	0.0		2
159	48.32	0.7	-48.7	0.0		2
159	102.00	1.2	-21.8	-0.0		2
159	0.00	0.4	-36.5	-0.1		3
159	48.32	0.7	-24.4	-0.0		3
159	102.00	1.2	-10.9	0.1		3
159	0.00	0.4	-21.9	-0.2		4
159	48.32	0.7	-14.6	-0.0		4
159	102.00	1.2	-6.5	0.2		4
160	0.00	0.4	-0.0	0.5	1	
160	48.32	0.7	-0.0	0.0	1	
160	102.00	1.2	0.0	-0.5	1	
160	0.00	-0.0	-0.0	-0.0	2	
160	48.32	-0.0	-0.0	-0.0	2	
160	102.00	-0.0	-0.0	-0.0	2	
160	0.00	0.0	-71.1	0.3	3	
160	48.32	0.0	-48.4	0.0	3	
160	102.00	0.0	-23.1	-0.3	3	
160	0.00	0.5	-106.6	1.1		1
160	48.32	1.0	-72.6	0.1		1
160	102.00	1.5	-34.7	-1.1		1
160	0.00	0.4	-71.1	0.8		2
160	48.32	0.7	-48.4	0.0		2
160	102.00	1.2	-23.1	-0.8		2
160	0.00	0.4	-35.5	0.7		3
160	48.32	0.7	-24.2	0.0		3
160	102.00	1.2	-11.6	-0.7		3
160	0.00	0.4	-21.3	0.6		4
160	48.32	0.7	-14.5	0.0		4
160	102.00	1.2	-6.9	-0.6		4
161	0.00	0.4	-0.0	1.2	1	
161	48.32	0.8	-0.0	0.1	1	
161	102.00	1.2	0.0	-1.2	1	
161	0.00	-0.0	-0.0	-0.0	2	
161	48.32	-0.0	-0.0	-0.0	2	
161	102.00	-0.0	-0.0	-0.0	2	
161	0.00	0.0	-72.7	0.2	3	
161	48.32	0.0	-49.2	0.0	3	
161	102.00	0.0	-23.1	-0.2	3	
161	0.00	0.5	-109.0	1.9		1
161	48.32	1.0	-73.8	0.1		1
161	102.00	1.6	-34.6	-2.0		1
161	0.00	0.4	-72.7	1.5		2
161	48.32	0.8	-49.2	0.1		2
161	102.00	1.2	-23.1	-1.5		2
161	0.00	0.4	-36.3	1.3		3
161	48.32	0.8	-24.6	0.1		3
161	102.00	1.2	-11.5	-1.4		3
161	0.00	0.4	-21.8	1.3		4
161	48.32	0.8	-14.8	0.1		4
161	102.00	1.2	-6.9	-1.3		4

162	0.00	0.4	-0.0	1.8	1
162	48.32	0.8	-0.0	0.1	1
162	102.00	1.2	0.0	-1.7	1
162	0.00	-0.0	-0.0	-0.0	2
162	48.32	-0.0	-0.0	-0.0	2
162	102.00	-0.0	-0.0	-0.0	2
162	0.00	0.0	-78.2	0.2	3
162	48.32	0.0	-51.2	0.0	3
162	102.00	0.0	-21.2	-0.2	3
162	0.00	0.6	-117.3	2.6	1
162	48.32	1.1	-76.8	0.1	1
162	102.00	1.6	-31.7	-2.5	1
162	0.00	0.4	-78.2	1.9	2
162	48.32	0.8	-51.2	0.1	2
162	102.00	1.2	-21.2	-1.9	2
162	0.00	0.4	-39.1	1.8	3
162	48.32	0.8	-25.6	0.1	3
162	102.00	1.2	-10.6	-1.8	3
162	0.00	0.4	-23.5	1.8	4
162	48.32	0.8	-15.4	0.1	4
162	102.00	1.2	-6.3	-1.8	4
163	0.00	-0.7	-0.0	2.2	1
163	48.32	-0.3	-0.0	0.2	1
163	102.00	0.1	-0.0	-2.0	1
163	0.00	-0.0	-0.0	-0.0	2
163	48.32	-0.0	-0.0	-0.0	2
163	102.00	-0.0	-0.0	-0.0	2
163	0.00	-0.0	-88.7	0.1	3
163	48.32	-0.0	-54.6	0.0	3
163	102.00	-0.0	-16.6	-0.1	3
163	0.00	-0.9	-133.0	3.1	1
163	48.32	-0.4	-81.8	0.3	1
163	102.00	0.1	-24.9	-2.8	1
163	0.00	-0.7	-88.7	2.4	2
163	48.32	-0.3	-54.6	0.2	2
163	102.00	0.1	-16.6	-2.1	2
163	0.00	-0.7	-44.4	2.3	3
163	48.32	-0.3	-27.3	0.2	3
163	102.00	0.1	-8.3	-2.1	3
163	0.00	-0.7	-26.6	2.3	4
163	48.32	-0.3	-16.4	0.2	4
163	102.00	0.1	-5.0	-2.0	4

DESCRIZIONE TABELLA SOLLECITAZIONI TRAVI E PILASTRI

Di seguito si riportano le spiegazioni delle sigle usate nella tabella SOLLECITAZIONI TRAVI E PILASTRI.
Per ogni gruppo di elementi ed internamente ad esso, per ogni elemento ad esso appartenente ed in ogni condizione di carico considerata vengono riportate, secondo modalita' diverse da tipo a tipo di elemento, azioni e/o tensioni in punti caratteristici riferiti alla terna locale.

ELEM. numero dell' elemento
n.ro
x ascissa locale misurata dal nodo I al nodo J
N sforzo normale nel p.to x
V2 forza di taglio ' ' ' in direz. 2 locale
V3 forza di taglio ' ' ' ' 3 '
T momento torcente ' ' '
M2 momento flettente ' ' ' intorno asse 2 locale
M3 momento flettente ' ' ' ' 3 '

Per la descrizione delle convenzioni usate per il segno delle azioni interne, si rimanda alla documentazione fornita con il programma.

RISULTATI : SOLLECITAZIONI PILASTRATA 1

ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
1	0.00	-21.8	0.7	0.0	0.0	-0.0	-0.0	1	
1	0.27	-19.1	0.7	0.0	0.0	-0.0	-0.2	1	
1	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
1	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
1	0.00	-0.2	1.0	116.3	13.4	-166.5	0.2	3	
1	0.27	-0.2	1.0	116.3	13.4	-135.1	-0.1	3	
1	0.00	-28.7	2.4	174.5	20.1	-249.7	0.2		1
1	0.27	-25.1	2.4	174.5	20.1	-202.6	-0.5		1
1	0.00	-22.0	1.7	116.3	13.4	-166.5	0.1		2
1	0.27	-19.3	1.7	116.3	13.4	-135.1	-0.3		2
1	0.00	-21.9	1.2	58.2	6.7	-83.3	0.0		3
1	0.27	-19.2	1.2	58.2	6.7	-67.5	-0.3		3
1	0.00	-21.9	1.0	34.9	4.0	-50.0	0.0		4
1	0.27	-19.1	1.0	34.9	4.0	-40.5	-0.3		4
3	0.00	-17.8	-1.3	0.0	0.0	-0.0	-0.3	1	
3	1.02	-7.4	-1.3	0.0	0.0	-0.0	1.0	1	
3	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
3	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
3	0.00	-0.2	-0.2	121.1	16.4	-134.3	-0.1	3	
3	1.02	-0.2	-0.2	121.1	16.4	-10.9	0.1	3	
3	0.00	-23.4	-1.9	181.6	24.6	-201.5	-0.6		1
3	1.02	-9.9	-1.9	181.6	24.6	-16.3	1.4		1
3	0.00	-18.0	-1.5	121.1	16.4	-134.3	-0.4		2
3	1.02	-7.6	-1.5	121.1	16.4	-10.9	1.1		2
3	0.00	-17.9	-1.4	60.5	8.2	-67.2	-0.4		3
3	1.02	-7.5	-1.4	60.5	8.2	-5.4	1.0		3
3	0.00	-17.9	-1.3	36.3	4.9	-40.3	-0.4		4
3	1.02	-7.5	-1.3	36.3	4.9	-3.3	1.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 2

ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
27	0.00	-0.7	-0.0	0.0	0.0	-0.0	-0.0	1	
27	1.02	0.1	-0.0	0.0	0.0	-0.0	0.0	1	
27	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
27	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
27	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
27	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
27	0.00	-0.9	-0.0	0.2	0.0	-0.2	-0.0		1
27	1.02	0.1	-0.0	0.2	0.0	-0.0	0.0		1
27	0.00	-0.7	-0.0	0.1	0.0	-0.1	-0.0		2
27	1.02	0.1	-0.0	0.1	0.0	-0.0	0.0		2
27	0.00	-0.7	-0.0	0.1	0.0	-0.1	-0.0		3
27	1.02	0.1	-0.0	0.1	0.0	-0.0	0.0		3
27	0.00	-0.7	-0.0	0.0	0.0	-0.0	-0.0		4

27	1.02	0.1	-0.0	0.0	0.0	-0.0	0.0		4
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RISULTATI : SOLLECITAZIONI PILASTRATA 3									
=====									
ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
28	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	1	
28	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1	
28	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
28	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
28	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
28	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3	
28	0.00	0.6	-0.0	0.1	0.0	-0.2	-0.0		1
28	1.02	1.6	-0.0	0.1	0.0	-0.1	0.0		1
28	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		2
28	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		2
28	0.00	0.4	-0.0	0.0	0.0	-0.1	-0.0		3
28	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		3
28	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0		4
28	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		4
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RISULTATI : SOLLECITAZIONI PILASTRATA 4									
=====									
ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
29	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	1	
29	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1	
29	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
29	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
29	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
29	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3	
29	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0		1
29	1.02	1.6	-0.0	0.1	0.0	-0.1	0.0		1
29	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		2
29	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		2
29	0.00	0.4	-0.0	0.0	0.0	-0.1	-0.0		3
29	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		3
29	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0		4
29	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		4
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RISULTATI : SOLLECITAZIONI PILASTRATA 5									
=====									
ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
30	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	1	
30	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1	
30	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
30	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
30	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
30	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3	
30	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0		1
30	1.02	1.5	-0.0	0.1	0.0	-0.1	0.0		1
30	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		2
30	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		2
30	0.00	0.4	-0.0	0.0	0.0	-0.1	-0.0		3
30	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		3
30	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0		4
30	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		4
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RISULTATI : SOLLECITAZIONI PILASTRATA 6									
=====									
ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
31	0.00	0.4	0.0	0.0	0.0	-0.0	0.0	1	
31	1.02	1.2	0.0	0.0	0.0	0.0	-0.0	1	
31	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
31	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
31	0.00	0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
31	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3	
31	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0		1
31	1.02	1.5	-0.0	0.1	0.0	-0.1	0.0		1
31	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		2
31	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		2
31	0.00	0.4	-0.0	0.0	0.0	-0.1	0.0		3
31	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		3
31	0.00	0.4	-0.0	0.0	0.0	-0.1	0.0		4
31	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0		4
31	0.00	0.4	0.0	0.0	0.0	-0.0	0.0		4
31	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0		4
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RISULTATI : SOLLECITAZIONI PILASTRATA 7									
=====									
ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
32	0.00	0.4	0.0	-0.0	0.0	0.0	0.0	1	
32	1.02	1.2	0.0	-0.0	0.0	0.0	-0.0	1	
32	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
32	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
32	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
32	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
32	0.00	0.5	0.0	0.1	0.0	-0.2	0.0		1
32	1.02	1.5	0.0	0.1	0.0	-0.0	-0.0		1
32	0.00	0.4	0.0	0.1	0.0	-0.1	0.0		2
32	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0		2
32	0.00	0.4	0.0	0.0	0.0	-0.1	0.0		3
32	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0		3
32	0.00	0.4	0.0	0.0	0.0	-0.0	0.0		4
32	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0		4
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RISULTATI : SOLLECITAZIONI PILASTRATA 8									
=====									
ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
33	0.00	0.4	0.0	-0.0	0.0	0.0	0.0	1	
33	1.02	1.2	0.0	-0.0	0.0	0.0	-0.0	1	
33	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
33	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
33	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
33	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
33	0.00	0.5	0.0	0.2	0.0	-0.2	0.0		1
33	1.02	1.6	0.0	0.2	0.0	-0.0	-0.0		1
33	0.00	0.4	0.0	0.1	0.0	-0.1	0.0		2
33	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0		2
33	0.00	0.4	0.0	0.1	0.0	-0.1	0.0		3

33	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0	3	
33	0.00	0.4	0.0	0.0	0.0	-0.0	0.0	4	
33	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0	4	

RISULTATI : SOLLECITAZIONI PILASTRATA 9

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
34	0.00	0.5	0.0	-0.0	0.0	0.0	0.0	1	
34	1.02	1.3	0.0	-0.0	0.0	-0.0	-0.0	1	
34	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
34	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
34	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0	3	
34	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
34	0.00	0.6	0.0	0.2	0.0	-0.2	0.0		1
34	1.02	1.7	0.0	0.2	0.0	-0.0	-0.0		1
34	0.00	0.5	0.0	0.1	0.0	-0.2	0.0		2
34	1.02	1.3	0.0	0.1	0.0	-0.0	-0.0		2
34	0.00	0.5	0.0	0.1	0.0	-0.1	0.0		3
34	1.02	1.3	0.0	0.1	0.0	-0.0	-0.0		3
34	0.00	0.5	0.0	0.0	0.0	-0.0	0.0		4
34	1.02	1.3	0.0	0.0	0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 10

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
35	0.00	-0.3	0.0	-0.0	0.0	0.0	0.0	1	
35	1.02	0.5	0.0	-0.0	0.0	-0.0	-0.0	1	
35	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
35	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
35	0.00	0.0	-0.0	0.2	0.0	-0.2	-0.0	3	
35	1.02	0.0	-0.0	0.2	0.0	-0.0	0.0	3	
35	0.00	-0.3	0.0	0.3	0.0	-0.3	0.0		1
35	1.02	0.7	0.0	0.3	0.0	-0.0	-0.0		1
35	0.00	-0.3	0.0	0.2	0.0	-0.2	0.0		2
35	1.02	0.5	0.0	0.2	0.0	-0.0	-0.0		2
35	0.00	-0.3	0.0	0.1	0.0	-0.1	0.0		3
35	1.02	0.5	0.0	0.1	0.0	-0.0	-0.0		3
35	0.00	-0.3	0.0	0.1	0.0	-0.1	0.0		4
35	1.02	0.5	0.0	0.1	0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 11

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
6	0.00	-33.0	-0.6	-0.0	0.0	0.0	-0.1	1	
6	0.27	-30.2	-0.6	-0.0	0.0	0.0	0.1	1	
6	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
6	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
6	0.00	0.2	0.4	182.6	6.8	-227.4	0.1	3	
6	0.27	0.2	0.4	182.6	6.8	-178.1	-0.0	3	
6	0.00	-42.6	-0.2	273.8	10.2	-341.1	-0.0		1
6	0.27	-39.1	-0.2	273.8	10.2	-267.2	0.0		1
6	0.00	-32.8	-0.2	182.6	6.8	-227.4	-0.0		2
6	0.27	-30.1	-0.2	182.6	6.8	-178.1	0.0		2
6	0.00	-32.9	-0.4	91.3	3.4	-113.7	-0.0		3
6	0.27	-30.1	-0.4	91.3	3.4	-89.0	0.1		3
6	0.00	-32.9	-0.5	54.8	2.0	-68.2	-0.1		4
6	0.27	-30.2	-0.5	54.8	2.0	-53.4	0.1		4
4	0.00	-28.6	0.2	-0.0	0.0	0.0	0.1	1	
4	1.02	-18.2	0.2	-0.0	0.0	-0.0	-0.1	1	
4	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
4	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
4	0.00	0.1	-0.1	178.6	10.3	-176.8	-0.1	3	
4	1.02	0.1	-0.1	178.6	10.3	5.4	0.1	3	
4	0.00	-37.0	0.1	267.9	15.4	-265.2	0.0		1
4	1.02	-23.5	0.1	267.9	15.4	8.1	-0.1		1
4	0.00	-28.5	0.1	178.6	10.3	-176.8	0.0		2
4	1.02	-18.1	0.1	178.6	10.3	5.4	-0.1		2
4	0.00	-28.6	0.2	89.3	5.1	-88.4	0.1		3
4	1.02	-18.2	0.2	89.3	5.1	2.7	-0.1		3
4	0.00	-28.6	0.2	53.6	3.1	-53.0	0.1		4
4	1.02	-18.2	0.2	53.6	3.1	1.6	-0.1		4

RISULTATI : SOLLECITAZIONI PILASTRATA 12

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
44	0.00	-0.2	-0.0	-0.0	0.0	0.0	-0.0	1	
44	1.02	0.6	-0.0	-0.0	0.0	-0.0	0.0	1	
44	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
44	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
44	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0	3	
44	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0	3	
44	0.00	-0.3	-0.0	0.3	0.0	-0.3	-0.0		1
44	1.02	0.7	-0.0	0.3	0.0	-0.0	0.0		1
44	0.00	-0.2	-0.0	0.2	0.0	-0.2	-0.0		2
44	1.02	0.6	-0.0	0.2	0.0	-0.0	0.0		2
44	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0		3
44	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0		3
44	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0		4
44	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 13

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
43	0.00	0.5	-0.0	-0.0	0.0	0.0	-0.0	1	
43	1.02	1.3	-0.0	-0.0	0.0	0.0	0.0	1	
43	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
43	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
43	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0	3	
43	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
43	0.00	0.6	-0.0	0.2	0.0	-0.3	-0.0		1
43	1.02	1.7	-0.0	0.2	0.0	-0.0	0.0		1
43	0.00	0.5	-0.0	0.1	0.0	-0.2	-0.0		2
43	1.02	1.3	-0.0	0.1	0.0	-0.0	0.0		2
43	0.00	0.5	-0.0	0.1	0.0	-0.1	-0.0		3
43	1.02	1.3	-0.0	0.1	0.0	-0.0	0.0		3
43	0.00	0.5	-0.0	0.0	0.0	-0.1	-0.0		4
43	1.02	1.3	-0.0	0.0	0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 14

ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
42	0.00	0.4	-0.0	-0.0	0.0	0.0	-0.0	1	
42	1.02	1.2	-0.0	-0.0	0.0	0.0	0.0	1	
42	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
42	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
42	0.00	0.0	-0.0	0.1	0.0	-0.2	-0.0	3	
42	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3	
42	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0		1
42	1.02	1.6	-0.0	0.2	0.0	-0.0	0.0		1
42	0.00	0.4	-0.0	0.1	0.0	-0.2	-0.0		2
42	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		2
42	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		3
42	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		3
42	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0		4
42	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 15

ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
41	0.00	0.4	-0.0	-0.0	0.0	0.0	-0.0	1	
41	1.02	1.2	-0.0	-0.0	0.0	0.0	0.0	1	
41	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
41	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
41	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
41	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
41	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0		1
41	1.02	1.5	-0.0	0.2	0.0	-0.0	0.0		1
41	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		2
41	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		2
41	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		3
41	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		3
41	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0		4
41	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 16

ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
40	0.00	0.4	-0.0	0.0	0.0	0.0	-0.0	1	
40	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1	
40	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
40	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
40	0.00	-0.0	-0.0	0.1	0.0	-0.1	-0.0	3	
40	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
40	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0		1
40	1.02	1.5	-0.0	0.2	0.0	-0.0	0.0		1
40	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		2
40	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		2
40	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		3
40	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		3
40	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0		4
40	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 17

ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
39	0.00	0.4	0.0	0.0	0.0	0.0	0.0	1	
39	1.02	1.2	0.0	0.0	0.0	0.0	-0.0	1	
39	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
39	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
39	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0	3	
39	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
39	0.00	0.5	0.0	0.2	0.0	-0.2	0.0		1
39	1.02	1.5	0.0	0.2	0.0	-0.0	-0.0		1
39	0.00	0.4	0.0	0.1	0.0	-0.2	0.0		2
39	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0		2
39	0.00	0.4	0.0	0.1	0.0	-0.1	0.0		3
39	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0		3
39	0.00	0.4	0.0	0.0	0.0	-0.0	0.0		4
39	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 18

ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
38	0.00	0.4	0.0	0.0	0.0	0.0	0.0	1	
38	1.02	1.2	0.0	0.0	0.0	0.0	-0.0	1	
38	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
38	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
38	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0	3	
38	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
38	0.00	0.5	0.0	0.2	0.0	-0.2	0.0		1
38	1.02	1.5	0.0	0.2	0.0	-0.0	-0.0		1
38	0.00	0.4	0.0	0.1	0.0	-0.2	0.0		2
38	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0		2
38	0.00	0.4	0.0	0.1	0.0	-0.1	0.0		3
38	1.02	1.2	0.0	0.1	0.0	-0.0	-0.0		3
38	0.00	0.4	0.0	0.0	0.0	-0.0	0.0		4
38	1.02	1.2	0.0	0.0	0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 19

ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro
37	0.00	0.5	0.0	0.0	0.0	0.0	0.0	1	
37	1.02	1.3	0.0	0.0	0.0	0.0	-0.0	1	
37	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
37	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
37	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0	3	
37	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0	3	
37	0.00	0.6	0.0	0.2	0.0	-0.3	0.0		1
37	1.02	1.7	0.0	0.2	0.0	-0.0	-0.0		1
37	0.00	0.5	0.0	0.2	0.0	-0.2	0.0		2
37	1.02	1.3	0.0	0.2	0.0	-0.0	-0.0		2
37	0.00	0.5	0.0	0.1	0.0	-0.1	0.0		3
37	1.02	1.3	0.0	0.1	0.0	-0.0	-0.0		3
37	0.00	0.5	0.0	0.0	0.0	-0.1	0.0		4

37	1.02	1.3	0.0	0.0	0.0	-0.0	-0.0	4
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RISULTATI : SOLLECITAZIONI PILASTRATA 20

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
36	0.00	-0.2	0.0	0.0	0.0	0.0	0.0	1	
36	1.02	0.6	0.0	0.0	0.0	0.0	-0.0	1	
36	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
36	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
36	0.00	0.0	-0.0	0.2	0.0	-0.2	-0.0	3	
36	1.02	0.0	-0.0	0.2	0.0	-0.0	0.0	3	
36	0.00	-0.3	0.0	0.3	0.0	-0.3	0.0		1
36	1.02	0.8	0.0	0.3	0.0	-0.0	-0.0		1
36	0.00	-0.2	0.0	0.2	0.0	-0.2	0.0		2
36	1.02	0.6	0.0	0.2	0.0	-0.0	-0.0		2
36	0.00	-0.2	0.0	0.1	0.0	-0.1	0.0		3
36	1.02	0.6	0.0	0.1	0.0	-0.0	-0.0		3
36	0.00	-0.2	0.0	0.1	0.0	-0.1	0.0		4
36	1.02	0.6	0.0	0.1	0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 21

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
65	0.00	-32.0	-0.1	0.0	0.0	0.0	-0.0	1	
65	0.27	-29.3	-0.1	0.0	0.0	0.0	0.0	1	
65	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
65	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
65	0.00	0.0	0.1	201.1	1.9	-251.1	0.0	3	
65	0.27	0.0	0.1	201.1	1.9	-196.8	-0.0	3	
65	0.00	-41.6	-0.0	301.7	2.8	-376.7	-0.0		1
65	0.27	-38.0	-0.0	301.7	2.8	-295.2	0.0		1
65	0.00	-32.0	-0.0	201.1	1.9	-251.1	-0.0		2
65	0.27	-29.2	-0.0	201.1	1.9	-196.8	0.0		2
65	0.00	-32.0	-0.1	100.6	0.9	-125.6	-0.0		3
65	0.27	-29.3	-0.1	100.6	0.9	-98.4	0.0		3
65	0.00	-32.0	-0.1	60.3	0.6	-75.3	-0.0		4
65	0.27	-29.3	-0.1	60.3	0.6	-59.0	0.0		4
67	0.00	-27.7	-0.0	0.0	0.0	0.0	0.0	1	
67	1.02	-17.3	-0.0	0.0	0.0	0.0	0.0	1	
67	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
67	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
67	0.00	0.0	-0.0	197.4	2.9	-195.3	-0.0	3	
67	1.02	0.0	-0.0	197.4	2.9	6.1	0.0	3	
67	0.00	-36.0	-0.0	296.1	4.4	-292.9	-0.0		1
67	1.02	-22.5	-0.0	296.1	4.4	9.1	0.0		1
67	0.00	-27.7	-0.0	197.4	2.9	-195.3	-0.0		2
67	1.02	-17.3	-0.0	197.4	2.9	6.1	0.0		2
67	0.00	-27.7	-0.0	98.7	1.5	-97.6	0.0		3
67	1.02	-17.3	-0.0	98.7	1.5	3.0	0.0		3
67	0.00	-27.7	-0.0	59.2	0.9	-58.6	0.0		4
67	1.02	-17.3	-0.0	59.2	0.9	1.8	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 22

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
91	0.00	-0.2	-0.0	0.0	0.0	0.0	-0.0	1	
91	1.02	0.6	-0.0	0.0	0.0	0.0	0.0	1	
91	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
91	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
91	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0	3	
91	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0	3	
91	0.00	-0.3	-0.0	0.3	0.0	-0.3	-0.0		1
91	1.02	0.7	-0.0	0.3	0.0	-0.0	0.0		1
91	0.00	-0.3	-0.0	0.2	0.0	-0.2	-0.0		2
91	1.02	0.5	-0.0	0.2	0.0	-0.0	0.0		2
91	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0		3
91	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0		3
91	0.00	-0.2	-0.0	0.1	0.0	-0.1	-0.0		4
91	1.02	0.6	-0.0	0.1	0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 23

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
92	0.00	0.5	-0.0	0.0	0.0	0.0	-0.0	1	
92	1.02	1.3	-0.0	0.0	0.0	0.0	0.0	1	
92	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
92	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
92	0.00	-0.0	-0.0	0.2	0.0	-0.2	-0.0	3	
92	1.02	-0.0	-0.0	0.2	0.0	-0.0	0.0	3	
92	0.00	0.6	-0.0	0.2	0.0	-0.3	-0.0		1
92	1.02	1.7	-0.0	0.2	0.0	-0.0	0.0		1
92	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0		2
92	1.02	1.3	-0.0	0.2	0.0	-0.0	0.0		2
92	0.00	0.5	-0.0	0.1	0.0	-0.1	-0.0		3
92	1.02	1.3	-0.0	0.1	0.0	-0.0	0.0		3
92	0.00	0.5	-0.0	0.0	0.0	-0.1	-0.0		4
92	1.02	1.3	-0.0	0.0	0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 24

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
93	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	1	
93	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1	
93	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
93	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
93	0.00	0.0	-0.0	0.1	0.0	-0.2	-0.0	3	
93	1.02	0.0	-0.0	0.1	0.0	-0.0	0.0	3	
93	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0		1
93	1.02	1.6	-0.0	0.2	0.0	-0.0	0.0		1
93	0.00	0.4	-0.0	0.1	0.0	-0.2	-0.0		2
93	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		2
93	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		3
93	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		3
93	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0		4
93	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 25

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
94	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0	1	
94	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1	
94	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
94	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
94	0.00	-0.0	-0.0	0.1	0.0	-0.2	-0.0	3	
94	1.02	-0.0	-0.0	0.1	0.0	-0.0	0.0	3	
94	0.00	0.5	-0.0	0.2	0.0	-0.2	-0.0		1
94	1.02	1.5	-0.0	0.2	0.0	-0.1	0.0		1
94	0.00	0.4	-0.0	0.1	0.0	-0.2	-0.0		2
94	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		2
94	0.00	0.4	-0.0	0.1	0.0	-0.1	-0.0		3
94	1.02	1.2	-0.0	0.1	0.0	-0.0	0.0		3
94	0.00	0.4	-0.0	0.0	0.0	-0.0	-0.0		4
94	1.02	1.2	-0.0	0.0	0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 26

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
95	0.00	0.4	-0.0	0.0	0.0	-0.0	0.0	1	
95	1.02	1.2	-0.0	0.0	0.0	0.0	0.0	1	
95	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
95	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
95	0.00	-0.0	-0.0	0.1	-0.0	-0.1	-0.0	3	
95	1.02	-0.0	-0.0	0.1	-0.0	-0.0	-0.0	3	
95	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0		1
95	1.02	1.5	0.0	0.2	-0.0	-0.1	0.0		1
95	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		2
95	1.02	1.2	0.0	0.1	-0.0	-0.0	0.0		2
95	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		3
95	1.02	1.2	0.0	0.1	-0.0	-0.0	0.0		3
95	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0		4
95	1.02	1.2	0.0	0.0	-0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 27

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
96	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	1	
96	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1	
96	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
96	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
96	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0	3	
96	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
96	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0		1
96	1.02	1.5	0.0	0.2	-0.0	-0.1	-0.0		1
96	0.00	0.4	0.0	0.1	-0.0	-0.2	0.0		2
96	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		2
96	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		3
96	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		3
96	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0		4
96	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 28

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
97	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	1	
97	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1	
97	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
97	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
97	0.00	0.0	0.0	0.1	-0.0	-0.2	0.0	3	
97	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
97	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0		1
97	1.02	1.6	0.0	0.2	-0.0	-0.0	-0.0		1
97	0.00	0.4	0.0	0.1	-0.0	-0.2	0.0		2
97	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		2
97	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		3
97	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		3
97	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0		4
97	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 29

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
98	0.00	0.5	0.0	0.0	-0.0	0.0	0.0	1	
98	1.02	1.3	0.0	0.0	-0.0	0.0	-0.0	1	
98	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
98	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
98	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0	3	
98	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0	3	
98	0.00	0.6	0.0	0.2	-0.0	-0.3	0.0		1
98	1.02	1.7	0.0	0.2	-0.0	-0.0	-0.0		1
98	0.00	0.5	0.0	0.2	-0.0	-0.2	0.0		2
98	1.02	1.3	0.0	0.2	-0.0	-0.0	-0.0		2
98	0.00	0.5	0.0	0.1	-0.0	-0.1	0.0		3
98	1.02	1.3	0.0	0.1	-0.0	-0.0	-0.0		3
98	0.00	0.5	0.0	0.0	-0.0	-0.1	0.0		4
98	1.02	1.3	0.0	0.0	-0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 30

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
99	0.00	-0.2	0.0	0.0	-0.0	0.0	0.0	1	
99	1.02	0.6	0.0	0.0	-0.0	0.0	-0.0	1	
99	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
99	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
99	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0	3	
99	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0	3	
99	0.00	-0.3	0.0	0.3	-0.0	-0.3	0.0		1
99	1.02	0.7	0.0	0.3	-0.0	-0.0	-0.0		1
99	0.00	-0.3	0.0	0.2	-0.0	-0.2	0.0		2
99	1.02	0.5	0.0	0.2	-0.0	-0.0	-0.0		2
99	0.00	-0.2	0.0	0.1	-0.0	-0.1	0.0		3
99	1.02	0.6	0.0	0.1	-0.0	-0.0	-0.0		3
99	0.00	-0.2	0.0	0.1	-0.0	-0.1	0.0		4
99	1.02	0.6	0.0	0.1	-0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 31

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
70	0.00	-32.0	0.1	0.0	-0.0	0.0	0.0	1	
70	0.27	-29.3	0.1	0.0	-0.0	0.0	-0.0	1	
70	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
70	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
70	0.00	0.0	-0.1	201.1	-1.9	-251.1	-0.0	3	
70	0.27	0.0	-0.1	201.1	-1.9	-196.8	0.0	3	
70	0.00	-41.6	0.0	301.7	-2.8	-376.7	0.0		1
70	0.27	-38.0	0.0	301.7	-2.8	-295.2	-0.0		1
70	0.00	-32.0	0.0	201.1	-1.9	-251.1	0.0		2
70	0.27	-29.2	0.0	201.1	-1.9	-196.8	-0.0		2
70	0.00	-32.0	0.1	100.6	-0.9	-125.6	0.0		3
70	0.27	-29.3	0.1	100.6	-0.9	-98.4	-0.0		3
70	0.00	-32.0	0.1	60.3	-0.6	-75.3	0.0		4
70	0.27	-29.3	0.1	60.3	-0.6	-59.0	-0.0		4
68	0.00	-27.7	0.0	0.0	-0.0	0.0	-0.0	1	
68	1.02	-17.3	0.0	0.0	-0.0	0.0	-0.0	1	
68	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
68	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
68	0.00	0.0	0.0	197.4	-2.9	-195.3	0.0	3	
68	1.02	0.0	0.0	197.4	-2.9	6.1	-0.0	3	
68	0.00	-36.0	0.0	296.1	-4.4	-292.9	0.0		1
68	1.02	-22.5	0.0	296.1	-4.4	9.1	-0.0		1
68	0.00	-27.7	0.0	197.4	-2.9	-195.3	0.0		2
68	1.02	-17.3	0.0	197.4	-2.9	6.1	-0.0		2
68	0.00	-27.7	0.0	98.7	-1.5	-97.6	-0.0		3
68	1.02	-17.3	0.0	98.7	-1.5	3.0	-0.0		3
68	0.00	-27.7	0.0	59.2	-0.9	-58.6	-0.0		4
68	1.02	-17.3	0.0	59.2	-0.9	1.8	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 32

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
108	0.00	-0.2	-0.0	0.0	-0.0	0.0	-0.0	1	
108	1.02	0.6	-0.0	0.0	-0.0	0.0	0.0	1	
108	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
108	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
108	0.00	0.0	0.0	0.2	-0.0	-0.2	0.0	3	
108	1.02	0.0	0.0	0.2	-0.0	-0.0	-0.0	3	
108	0.00	-0.3	-0.0	0.3	-0.0	-0.3	-0.0		1
108	1.02	0.8	-0.0	0.3	-0.0	-0.0	0.0		1
108	0.00	-0.2	-0.0	0.2	-0.0	-0.2	-0.0		2
108	1.02	0.6	-0.0	0.2	-0.0	-0.0	0.0		2
108	0.00	-0.2	-0.0	0.1	-0.0	-0.1	-0.0		3
108	1.02	0.6	-0.0	0.1	-0.0	-0.0	0.0		3
108	0.00	-0.2	-0.0	0.1	-0.0	-0.1	-0.0		4
108	1.02	0.6	-0.0	0.1	-0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 33

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
107	0.00	0.5	-0.0	0.0	-0.0	0.0	-0.0	1	
107	1.02	1.3	-0.0	0.0	-0.0	0.0	0.0	1	
107	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
107	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
107	0.00	-0.0	0.0	0.2	-0.0	-0.2	0.0	3	
107	1.02	-0.0	0.0	0.2	-0.0	-0.0	-0.0	3	
107	0.00	0.6	-0.0	0.2	-0.0	-0.3	-0.0		1
107	1.02	1.7	-0.0	0.2	-0.0	-0.0	0.0		1
107	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0		2
107	1.02	1.3	-0.0	0.2	-0.0	-0.0	0.0		2
107	0.00	0.5	-0.0	0.1	-0.0	-0.1	-0.0		3
107	1.02	1.3	-0.0	0.1	-0.0	-0.0	0.0		3
107	0.00	0.5	-0.0	0.0	-0.0	-0.1	-0.0		4
107	1.02	1.3	-0.0	0.0	-0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 34

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
106	0.00	0.4	-0.0	0.0	-0.0	0.0	-0.0	1	
106	1.02	1.2	-0.0	0.0	-0.0	0.0	0.0	1	
106	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
106	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
106	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0	3	
106	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
106	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0		1
106	1.02	1.5	-0.0	0.2	-0.0	-0.0	0.0		1
106	0.00	0.4	-0.0	0.1	-0.0	-0.2	-0.0		2
106	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0		2
106	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0		3
106	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0		3
106	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0		4
106	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 35

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
105	0.00	0.4	-0.0	0.0	-0.0	0.0	-0.0	1	
105	1.02	1.2	-0.0	0.0	-0.0	0.0	0.0	1	
105	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
105	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
105	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0	3	
105	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
105	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0		1
105	1.02	1.5	-0.0	0.2	-0.0	-0.0	0.0		1
105	0.00	0.4	-0.0	0.1	-0.0	-0.2	-0.0		2
105	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0		2
105	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0		3
105	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0		3
105	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0		4
105	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 36

ELEM.	ascissa	N	V2	V3	T	M2	M3	CDC	COMB.
n.ro	(m)	(Kg)	(Kg)	(Kg)	(Kg*m)	(Kg*m)	(Kg*m)	n.ro	n.ro

RISULTATI : SOLLECITAZIONI PILASTRATA 37

RISULTATI : SOLLECITAZIONI PILASTRATA 38

RISULTATI : SOLLECITAZIONI PILASTRATA 39

RISULTATI : SOLLECITAZIONI PILASTRATA 40

RISULTATI : SOLLECITAZIONI PILASTRATA 41

[illegible]

131	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
131	0.00	0.1	0.1	178.6	-10.3	-176.8	0.1	3	
131	1.02	0.1	0.1	178.6	-10.3	5.4	-0.1	3	
131	0.00	-37.0	-0.1	267.9	-15.4	-265.2	-0.0		1
131	1.02	-23.5	-0.1	267.9	-15.4	8.1	0.1		1
131	0.00	-28.5	-0.1	178.6	-10.3	-176.8	-0.0		2
131	1.02	-18.1	-0.1	178.6	-10.3	5.4	0.1		2
131	0.00	-28.6	-0.2	89.3	-5.1	-88.4	-0.1		3
131	1.02	-18.2	-0.2	89.3	-5.1	2.7	0.1		3
131	0.00	-28.6	-0.2	53.6	-3.1	-53.0	-0.1		4
131	1.02	-18.2	-0.2	53.6	-3.1	1.6	0.1		4

RISULTATI : SOLLECITAZIONI PILASTRATA 42

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
155	0.00	-0.3	-0.0	-0.0	-0.0	0.0	-0.0	1	
155	1.02	0.5	-0.0	-0.0	-0.0	-0.0	0.0	1	
155	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
155	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
155	0.00	0.0	0.0	0.2	-0.0	-0.2	0.0	3	
155	1.02	0.0	0.0	0.2	-0.0	-0.0	-0.0	3	
155	0.00	-0.3	-0.0	0.3	-0.0	-0.3	-0.0		1
155	1.02	0.7	-0.0	0.3	-0.0	-0.0	0.0		1
155	0.00	-0.3	-0.0	0.2	-0.0	-0.2	-0.0		2
155	1.02	0.5	-0.0	0.2	-0.0	-0.0	0.0		2
155	0.00	-0.3	-0.0	0.1	-0.0	-0.1	-0.0		3
155	1.02	0.5	-0.0	0.1	-0.0	-0.0	0.0		3
155	0.00	-0.3	-0.0	0.1	-0.0	-0.1	-0.0		4
155	1.02	0.5	-0.0	0.1	-0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 43

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
156	0.00	0.5	-0.0	-0.0	-0.0	0.0	-0.0	1	
156	1.02	1.3	-0.0	-0.0	-0.0	-0.0	0.0	1	
156	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
156	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
156	0.00	-0.0	0.0	0.1	-0.0	-0.2	0.0	3	
156	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
156	0.00	0.6	-0.0	0.2	-0.0	-0.2	-0.0		1
156	1.02	1.7	-0.0	0.2	-0.0	-0.0	0.0		1
156	0.00	0.5	-0.0	0.1	-0.0	-0.2	-0.0		2
156	1.02	1.3	-0.0	0.1	-0.0	-0.0	0.0		2
156	0.00	0.5	-0.0	0.1	-0.0	-0.1	-0.0		3
156	1.02	1.3	-0.0	0.1	-0.0	-0.0	0.0		3
156	0.00	0.5	-0.0	0.0	-0.0	-0.0	-0.0		4
156	1.02	1.3	-0.0	0.0	-0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 44

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
157	0.00	0.4	-0.0	-0.0	-0.0	0.0	-0.0	1	
157	1.02	1.2	-0.0	-0.0	-0.0	0.0	0.0	1	
157	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
157	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
157	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0	3	
157	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
157	0.00	0.5	-0.0	0.2	-0.0	-0.2	-0.0		1
157	1.02	1.6	-0.0	0.2	-0.0	-0.0	0.0		1
157	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0		2
157	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0		2
157	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0		3
157	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0		3
157	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0		4
157	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 45

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
158	0.00	0.4	-0.0	-0.0	-0.0	0.0	-0.0	1	
158	1.02	1.2	-0.0	-0.0	-0.0	0.0	0.0	1	
158	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
158	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
158	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0	3	
158	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
158	0.00	0.5	-0.0	0.1	-0.0	-0.2	-0.0		1
158	1.02	1.5	-0.0	0.1	-0.0	-0.0	0.0		1
158	0.00	0.4	-0.0	0.1	-0.0	-0.1	-0.0		2
158	1.02	1.2	-0.0	0.1	-0.0	-0.0	0.0		2
158	0.00	0.4	-0.0	0.0	-0.0	-0.1	-0.0		3
158	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		3
158	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0		4
158	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 46

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
159	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0	1	
159	1.02	1.2	-0.0	0.0	-0.0	0.0	0.0	1	
159	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
159	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
159	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0	3	
159	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
159	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0		1
159	1.02	1.5	0.0	0.1	-0.0	-0.1	-0.0		1
159	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		2
159	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		2
159	0.00	0.4	-0.0	0.0	-0.0	-0.1	-0.0		3
159	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		3
159	0.00	0.4	-0.0	0.0	-0.0	-0.0	-0.0		4
159	1.02	1.2	-0.0	0.0	-0.0	-0.0	0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 47

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
160	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	1	

160	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1	
160	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
160	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
160	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0	3	
160	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
160	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0		1
160	1.02	1.5	0.0	0.1	-0.0	-0.1	-0.0		1
160	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		2
160	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		2
160	0.00	0.4	0.0	0.0	-0.0	-0.1	0.0		3
160	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		3
160	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0		4
160	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 48

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
161	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	1	
161	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1	
161	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
161	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
161	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0	3	
161	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
161	0.00	0.5	0.0	0.1	-0.0	-0.2	0.0		1
161	1.02	1.6	0.0	0.1	-0.0	-0.1	-0.0		1
161	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		2
161	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		2
161	0.00	0.4	0.0	0.0	-0.0	-0.1	0.0		3
161	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		3
161	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0		4
161	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 49

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
162	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0	1	
162	1.02	1.2	0.0	0.0	-0.0	0.0	-0.0	1	
162	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
162	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
162	0.00	0.0	0.0	0.1	-0.0	-0.1	0.0	3	
162	1.02	0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
162	0.00	0.6	0.0	0.1	-0.0	-0.2	0.0		1
162	1.02	1.6	0.0	0.1	-0.0	-0.1	-0.0		1
162	0.00	0.4	0.0	0.1	-0.0	-0.1	0.0		2
162	1.02	1.2	0.0	0.1	-0.0	-0.0	-0.0		2
162	0.00	0.4	0.0	0.0	-0.0	-0.1	0.0		3
162	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		3
162	0.00	0.4	0.0	0.0	-0.0	-0.0	0.0		4
162	1.02	1.2	0.0	0.0	-0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 50

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
163	0.00	-0.7	0.0	0.0	-0.0	-0.0	0.0	1	
163	1.02	0.1	0.0	0.0	-0.0	-0.0	-0.0	1	
163	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
163	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
163	0.00	-0.0	0.0	0.1	-0.0	-0.1	0.0	3	
163	1.02	-0.0	0.0	0.1	-0.0	-0.0	-0.0	3	
163	0.00	-0.9	0.0	0.2	-0.0	-0.2	0.0		1
163	1.02	0.1	0.0	0.2	-0.0	-0.0	-0.0		1
163	0.00	-0.7	0.0	0.1	-0.0	-0.1	0.0		2
163	1.02	0.1	0.0	0.1	-0.0	-0.0	-0.0		2
163	0.00	-0.7	0.0	0.1	-0.0	-0.1	0.0		3
163	1.02	0.1	0.0	0.1	-0.0	-0.0	-0.0		3
163	0.00	-0.7	0.0	0.0	-0.0	-0.0	0.0		4
163	1.02	0.1	0.0	0.0	-0.0	-0.0	-0.0		4

RISULTATI : SOLLECITAZIONI PILASTRATA 51

ELEM. n.ro	ascissa (m)	N (Kg)	V2 (Kg)	V3 (Kg)	T (Kg*m)	M2 (Kg*m)	M3 (Kg*m)	CDC n.ro	COMB. n.ro
134	0.00	-21.8	-0.7	0.0	-0.0	-0.0	0.0	1	
134	0.27	-19.1	-0.7	0.0	-0.0	-0.0	0.2	1	
134	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
134	0.27	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
134	0.00	-0.2	-1.0	116.3	-13.4	-166.5	-0.2	3	
134	0.27	-0.2	-1.0	116.3	-13.4	-135.1	0.1	3	
134	0.00	-28.7	-2.4	174.5	-20.1	-249.7	-0.2		1
134	0.27	-25.1	-2.4	174.5	-20.1	-202.6	0.5		1
134	0.00	-22.0	-1.7	116.3	-13.4	-166.5	-0.1		2
134	0.27	-19.3	-1.7	116.3	-13.4	-135.1	0.3		2
134	0.00	-21.9	-1.2	58.2	-6.7	-83.3	-0.0		3
134	0.27	-19.2	-1.2	58.2	-6.7	-67.5	0.3		3
134	0.00	-21.9	-1.0	34.9	-4.0	-50.0	-0.0		4
134	0.27	-19.1	-1.0	34.9	-4.0	-40.5	0.3		4
132	0.00	-17.8	1.3	0.0	-0.0	-0.0	0.3	1	
132	1.02	-7.4	1.3	0.0	-0.0	-0.0	-1.0	1	
132	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
132	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0	2	
132	0.00	-0.2	0.2	121.1	-16.4	-134.3	0.1	3	
132	1.02	-0.2	0.2	121.1	-16.4	-10.9	-0.1	3	
132	0.00	-23.4	1.9	181.6	-24.6	-201.5	0.6		1
132	1.02	-9.9	1.9	181.6	-24.6	-16.3	-1.4		1
132	0.00	-18.0	1.5	121.1	-16.4	-134.3	0.4		2
132	1.02	-7.6	1.5	121.1	-16.4	-10.9	-1.1		2
132	0.00	-17.9	1.4	60.5	-8.2	-67.2	0.4		3
132	1.02	-7.5	1.4	60.5	-8.2	-5.4	-1.0		3
132	0.00	-17.9	1.3	36.3	-4.9	-40.3	0.4		4
132	1.02	-7.5	1.3	36.3	-4.9	-3.3	-1.0		4

DESCRIZIONE TABELLA REAZIONI VINCOLARI

Di seguito si riportano le spiegazioni delle sigle usate nella tabella REAZIONI VINCOLARI.

Relativamente ad ogni caso di carico, vengono elencate, per ogni nodo vincolato, i valori delle componenti delle reazioni vincolari (forze e momenti) riferite alla terna globale:

NODO numero del nodo vincolato
n.ro
Fx componente della reazione-forza in direzione X
Fy , , , Y

Nota: per componente del momento in una direzione, si intende la componente del vettore asse-momento in quella direzione.
La componente F_x della forza e' positiva se concorde con l'asse X ; analogamente per F_y, F_z .
La componente M_x del momento e' positiva se concorde con l'asse X ; analogamente per M_y, M_z .

NODO n.ro	CDC n.ro	Fx (Kg)	Fy (Kg)	Fz (Kg)	Mx (Kg*m)	My (Kg*m)	Mz (Kg*m)
3	1	0.0	-0.7	22.2	-0.0	0.9	0.0
8	1	-0.0	0.6	33.4	-0.1	1.3	-0.0
48	1	0.0	0.1	32.4	-0.0	1.3	-0.0
52	1	0.0	-0.1	32.4	0.0	1.3	0.0
92	1	-0.0	-0.6	33.4	0.1	1.3	0.0
96	1	0.0	0.7	22.2	0.0	0.9	-0.0
3	2	0.0	0.0	0.0	0.0	0.0	0.0
8	2	0.0	0.0	0.0	0.0	0.0	0.0
48	2	0.0	0.0	0.0	0.0	0.0	0.0
52	2	0.0	0.0	0.0	0.0	0.0	0.0
92	2	0.0	0.0	0.0	0.0	0.0	0.0
96	2	0.0	0.0	0.0	0.0	0.0	0.0
3	3	116.3	-1.0	0.2	0.2	166.5	-13.4
8	3	182.6	-0.4	-0.2	0.1	227.4	-6.8
48	3	201.1	-0.1	-0.0	0.0	251.1	-1.9
52	3	201.1	0.1	-0.0	-0.0	251.1	1.9
92	3	182.6	0.4	-0.2	-0.1	227.4	6.8
96	3	116.3	1.0	0.2	-0.2	166.5	13.4

NODO n.ro	COMB. n.ro	Fx (Kg)	Fy (Kg)	Fz (Kg)	Mx (Kg*m)	My (Kg*m)	Mz (Kg*m)
3	1	174.5	-2.4	29.2	0.2	250.9	-20.0
8	1	273.8	0.2	43.2	-0.0	342.8	-10.2
48	1	301.7	0.0	42.1	-0.0	378.3	-2.8
52	1	301.7	-0.0	42.1	0.0	378.3	2.8
92	1	273.8	-0.2	43.2	0.0	342.8	10.2
96	1	174.5	2.4	29.2	-0.2	250.9	20.0
3	2	116.3	-1.7	22.4	0.1	167.4	-13.3
8	2	182.6	0.2	33.2	-0.0	228.7	-6.8
48	2	201.1	0.0	32.4	-0.0	252.4	-1.9
52	2	201.1	-0.0	32.4	0.0	252.4	1.9
92	2	182.6	-0.2	33.2	0.0	228.7	6.8
96	2	116.3	1.7	22.4	-0.1	167.4	13.3
3	3	58.2	-1.2	22.3	0.0	84.1	-6.7
8	3	91.3	0.4	33.3	-0.0	115.0	-3.4
48	3	100.6	0.1	32.4	-0.0	126.8	-0.9
52	3	100.6	-0.1	32.4	0.0	126.8	0.9
92	3	91.3	-0.4	33.3	0.0	115.0	3.4
96	3	58.2	1.2	22.3	-0.0	84.1	6.7
3	4	34.9	-1.0	22.3	0.0	50.8	-4.0
8	4	54.8	0.5	33.3	-0.1	69.5	-2.1
48	4	60.3	0.1	32.4	-0.0	76.6	-0.6
52	4	60.3	-0.1	32.4	0.0	76.6	0.6
92	4	54.8	-0.5	33.3	0.1	69.5	2.1
96	4	34.9	1.0	22.3	-0.0	50.8	4.0

Di seguito si riportano le spiegazioni delle sigle usate nella tabella SOLLECITAZIONI TRAVI E PILASTRI.

Per ogni gruppo di elementi ed internamente ad esso, per ogni elemento ad esso appartenente ed in ogni condizione di carico considerata vengono riportate, secondo modalita' diverse da tipo a tipo di elemento, azioni e/o tensioni in punti caratteristici riferiti alla terna locale.

Per la descrizione delle convenzioni usate per il segno delle azioni interne, si rimanda alla documentazione fornita con il programma.

ELEM. n.ro	ascissa (m)	N (Kg) min/max	V2 (Kg) min/max	V3 (Kg) min/max	T (Kg*m) min/max	M2 (Kg*m) min/max	M3 (Kg*m) min/max
2	0.00	-0.0 174.5	-0.0 28.7	-0.0 2.4	-0.0 0.2	-20.1 -0.0	-249.7 -0.0
2	0.04	-0.0 174.5	-0.0 29.2	-0.0 2.4	-0.0 0.2	-20.0 0.0	-250.9 -0.0
5	0.00	-0.0 273.8	-0.2 42.6	-0.6 0.4	-0.1 0.1	-10.2 -0.0	-341.1 0.0
5	0.04	-0.0 273.8	-0.2 43.2	-0.6 0.4	-0.1 0.1	-10.2 -0.0	-342.8 -0.0
7	0.00	-0.0 4.3	-1.6 -0.0	-0.0 7.1	-1.1 -0.0	-4.4 0.0	-0.1 -0.0
7	0.10	-0.0 4.3	-1.1 -0.0	-0.0 7.1	-1.1 -0.0	-3.7 0.0	-0.0 0.0
8	0.00	-0.0	-0.2	-0.0	-0.9	-3.8	-0.0

		4.4	-0.0	7.3	-0.0	0.0	0.0
8	0.10	-0.0	-0.0	-0.0	-0.9	-3.0	-0.0
		4.4	0.3	7.3	-0.0	0.0	0.0
9	0.00	-0.0	-0.3	-0.0	-0.7	-3.1	-0.0
		4.4	-0.0	7.4	-0.0	0.0	0.0
9	0.10	-0.0	-0.0	-0.0	-0.7	-2.3	-0.0
		4.4	0.2	7.4	-0.0	0.0	0.0
10	0.00	-0.0	-0.3	-0.0	-0.5	-2.4	-0.0
		4.4	-0.0	7.5	-0.0	0.0	0.0
10	0.10	-0.0	-0.0	-0.0	-0.5	-1.6	-0.0
		4.4	0.2	7.5	-0.0	0.0	0.0
11	0.00	-0.0	-0.3	-0.0	-0.3	-1.6	-0.0
		4.4	-0.0	7.7	-0.0	0.0	0.0
11	0.10	-0.0	-0.0	-0.0	-0.3	-0.9	-0.0
		4.4	0.2	7.7	-0.0	0.0	0.0
12	0.00	-0.0	-0.2	-0.0	-0.2	-0.9	-0.0
		4.4	-0.0	7.8	-0.0	0.0	0.0
12	0.10	-0.0	-0.0	-0.0	-0.2	-0.1	-0.0
		4.4	0.3	7.8	-0.0	-0.0	0.0
13	0.00	-0.0	-0.2	-0.0	-0.0	-0.2	-0.0
		4.4	-0.0	7.9	0.0	-0.0	0.0
13	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		4.4	0.3	7.9	0.0	0.6	0.0
14	0.00	-0.0	-0.2	-0.0	-0.0	-0.0	-0.0
		4.4	-0.0	8.1	0.3	0.6	0.0
14	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		4.4	0.3	8.1	0.3	1.4	0.0
15	0.00	-0.0	-0.3	-0.0	-0.0	-0.0	-0.0
		4.4	-0.0	8.3	0.5	1.4	0.0
15	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		4.4	0.2	8.3	0.5	2.2	0.0
16	0.00	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		4.4	0.5	8.6	0.8	2.2	0.0
16	0.10	-0.0	-0.0	-0.0	-0.0	-0.0	-0.1
		4.4	1.1	8.6	0.8	3.0	0.0
17	0.00	-1.9	-9.9	-181.6	-16.3	-0.0	-1.4
		-0.0	-0.0	-0.0	-0.0	24.6	-0.0
17	0.10	-1.9	-8.9	-151.6	-16.3	-0.0	-0.5
		-0.0	-0.0	-0.0	-0.0	7.9	-0.0
18	0.00	-2.0	-8.8	-151.8	-16.3	-0.0	-0.5
		-0.0	-0.0	-0.0	-0.0	7.9	-0.0
18	0.10	-2.0	-7.8	-121.8	-16.3	-5.7	-0.1
		-0.0	-0.0	-0.0	-0.0	0.0	0.4
19	0.00	-2.0	-6.1	-121.9	-16.4	-5.7	-0.1
		-0.0	-0.0	-0.0	-0.0	0.0	0.4
19	0.10	-2.0	-5.1	-91.9	-16.4	-16.4	-0.0
		-0.0	-0.0	-0.0	-0.0	0.0	0.9
20	0.00	-2.0	-3.6	-92.0	-16.5	-16.4	-0.0
		-0.0	-0.0	-0.0	-0.0	0.0	0.9
20	0.10	-2.0	-2.5	-62.0	-16.5	-24.1	-0.0
		-0.0	-0.0	-0.0	-0.0	-0.0	1.2
21	0.00	-2.0	-1.0	-62.1	-16.5	-24.0	-0.0
		-0.0	-0.0	-0.0	-0.0	-0.0	1.2
21	0.10	-2.0	-0.2	-32.1	-16.5	-28.7	-0.0
		-0.0	0.2	-0.0	-0.0	-0.0	1.3
22	0.00	-2.0	-0.2	-32.3	-16.6	-28.7	-0.0
		-0.0	1.5	-0.0	-0.0	-0.0	1.3
22	0.10	-2.0	-0.2	-2.3	-16.6	-30.4	-0.0
		-0.0	2.5	-0.0	-0.0	-0.0	1.1
23	0.00	-2.0	-0.2	-2.4	-16.6	-30.4	-0.0
		-0.0	4.0	-0.0	-0.0	-0.0	1.1
23	0.10	-2.0	-0.2	-0.0	-16.6	-29.1	-0.0
		-0.0	5.0	27.6	-0.0	-0.0	0.6
24	0.00	-2.0	-0.2	-0.0	-16.7	-29.1	-0.0
		-0.0	6.6	27.4	-0.0	-0.0	0.6
24	0.10	-2.0	-0.2	-0.0	-16.7	-24.9	-0.1
		-0.0	7.6	57.4	-0.0	-0.0	0.1
25	0.00	-2.0	-0.2	-0.0	-16.7	-24.9	-0.1
		-0.0	9.3	57.2	-0.0	-0.0	0.1
25	0.10	-2.0	-0.2	-0.0	-16.7	-17.6	-1.1
		-0.0	10.3	87.2	-0.0	-0.0	0.1
26	0.00	-2.0	-0.1	-0.0	-16.7	-17.6	-1.0
		-0.0	11.0	86.9	-0.0	-0.0	0.1
26	0.10	-2.0	-0.1	-0.0	-16.7	-7.4	-2.2
		-0.0	12.0	116.9	-0.0	-0.0	0.1
45	0.00	-1.9	-0.0	-0.0	-8.9	-7.0	-0.9
		-0.0	10.2	117.1	-0.0	-0.0	0.0
45	0.10	-1.9	-0.0	-0.0	-8.9	-0.0	-2.0
		-0.0	11.2	147.1	-0.0	6.2	0.0
46	0.00	-1.9	-0.0	-0.0	-8.9	-17.3	-0.1
		-0.0	8.4	87.4	-0.0	-0.0	0.0
46	0.10	-1.9	-0.0	-0.0	-8.9	-7.0	-0.9
		-0.0	9.4	117.4	-0.0	-0.0	0.0
47	0.00	-1.9	-0.0	-0.0	-8.9	-24.5	-0.0
		-0.0	5.7	57.6	-0.0	-0.0	0.6
47	0.10	-1.9	-0.0	-0.0	-8.9	-17.3	-0.1
		-0.0	6.7	87.6	-0.0	-0.0	0.0
48	0.00	-1.9	-0.0	-0.0	-8.8	-28.8	-0.0
		-0.0	3.1	27.8	-0.0	-0.0	0.9
48	0.10	-1.9	-0.0	-0.0	-8.8	-24.5	-0.0
		-0.0	4.1	57.8	-0.0	-0.0	0.6
49	0.00	-1.9	-0.0	-2.0	-8.8	-30.1	-0.0
		-0.0	0.6	0.0	-0.0	-0.0	1.1
49	0.10	-1.9	-0.0	-0.0	-8.8	-28.8	-0.0
		-0.0	1.6	28.0	-0.0	-0.0	0.9

50	0.00	-1.9 -0.0	-1.9 -0.0	-31.8 0.0	-8.7 -0.0	-28.5 -0.0	-0.0 0.9
50	0.10	-1.9 -0.0	-0.9 -0.0	-1.8 0.0	-8.7 -0.0	-30.2 -0.0	-0.0 1.1
51	0.00	-1.9 -0.0	-4.4 -0.0	-61.6 0.0	-8.7 -0.0	-23.8 -0.0	-0.0 0.5
51	0.10	-1.9 -0.0	-3.4 -0.0	-31.6 0.0	-8.7 -0.0	-28.5 -0.0	-0.0 0.9
52	0.00	-1.9 -0.0	-7.0 -0.0	-91.5 0.0	-8.6 -0.0	-16.2 -0.0	-0.1 0.0
52	0.10	-1.9 -0.0	-6.0 -0.0	-61.5 0.0	-8.6 -0.0	-23.9 -0.0	-0.0 0.5
53	0.00	-1.9 -0.0	-9.7 -0.0	-121.2 0.0	-8.6 -0.0	-5.6 -0.0	-1.0 -0.0
53	0.10	-1.9 -0.0	-8.7 -0.0	-91.2 0.0	-8.6 -0.0	-16.2 -0.0	-0.1 0.0
54	0.00	-1.8 -0.0	-11.5 0.0	-151.0 0.0	-8.6 -0.0	-0.0 8.0	-2.1 -0.0
54	0.10	-1.8 -0.0	-10.5 0.0	-121.0 0.0	-8.6 -0.0	-5.6 -0.0	-1.0 -0.0
55	0.00	-0.0 4.1	-0.0 0.5	-0.0 4.6	-0.0 1.1	-0.0 0.8	-0.0 0.0
55	0.10	-0.0 4.1	-0.0 1.0	-0.0 4.6	-0.0 1.1	-0.0 1.3	-0.1 0.0
56	0.00	-0.0 4.1	-0.3 -0.0	-0.0 4.3	-0.0 0.8	-0.0 0.4	-0.0 0.0
56	0.10	-0.0 4.1	-0.0 0.2	-0.0 4.3	-0.0 0.8	-0.0 0.8	-0.0 0.0
57	0.00	-0.0 4.1	-0.2 -0.0	-0.0 4.0	-0.0 0.5	-0.0 0.0	-0.0 0.0
57	0.10	-0.0 4.1	-0.0 0.3	-0.0 4.0	-0.0 0.5	-0.0 0.4	-0.0 0.0
58	0.00	-0.0 4.1	-0.2 -0.0	-0.0 3.8	-0.0 0.2	-0.4 -0.0	-0.0 0.0
58	0.10	-0.0 4.1	-0.0 0.3	-0.0 3.8	-0.0 0.2	-0.0 0.0	-0.0 0.0
59	0.00	-0.0 4.1	-0.2 -0.0	-0.0 3.7	-0.0 0.0	-0.7 -0.0	-0.0 0.0
59	0.10	-0.0 4.1	-0.0 0.3	-0.0 3.7	-0.0 0.0	-0.3 -0.0	-0.0 0.0
60	0.00	-0.0 4.1	-0.3 -0.0	-0.0 3.5	-0.2 -0.0	-1.0 -0.0	-0.0 0.0
60	0.10	-0.0 4.1	-0.0 0.2	-0.0 3.5	-0.2 -0.0	-0.7 -0.0	-0.0 0.0
61	0.00	-0.0 4.1	-0.3 -0.0	-0.0 3.3	-0.4 -0.0	-1.4 -0.0	-0.0 -0.0
61	0.10	-0.0 4.1	-0.0 0.2	-0.0 3.3	-0.4 -0.0	-1.0 -0.0	-0.0 0.0
62	0.00	-0.0 4.1	-0.3 -0.0	-0.0 3.1	-0.7 -0.0	-1.7 -0.0	-0.0 0.0
62	0.10	-0.0 4.1	-0.0 0.2	-0.0 3.1	-0.7 -0.0	-1.3 -0.0	-0.0 0.0
63	0.00	-0.0 4.1	-0.2 -0.0	-0.0 2.9	-0.9 -0.0	-1.9 -0.0	-0.0 0.0
63	0.10	-0.0 4.1	-0.0 0.3	-0.0 2.9	-0.9 -0.0	-1.6 -0.0	-0.0 0.0
64	0.00	-0.0 4.1	-1.0 -0.0	-0.0 2.7	-1.2 0.0	-2.2 -0.0	-0.1 -0.0
64	0.10	-0.0 4.1	-0.5 -0.0	-0.0 2.7	-1.2 0.0	-1.9 -0.0	-0.0 0.0
66	0.00	-0.0 301.7	-0.0 41.6	-0.1 0.1	-0.0 0.0	-2.8 -0.0	-376.7 0.0
66	0.04	-0.0 301.7	-0.0 42.1	-0.1 0.1	-0.0 0.0	-2.8 -0.0	-378.3 -0.0
69	0.00	-0.0 301.7	-0.0 41.6	-0.1 0.1	-0.0 0.0	-0.0 2.8	-376.7 0.0
69	0.04	-0.0 301.7	-0.0 42.1	-0.1 0.1	-0.0 0.0	-0.0 2.8	-378.3 -0.0
71	0.00	-0.0 4.1	-1.0 -0.0	-1.0 -0.0	-1.2 -0.0	-0.3 -0.0	-0.1 -0.0
71	0.10	-0.0 4.1	-0.5 -0.0	-1.0 -0.0	-1.2 -0.0	-0.4 -0.0	-0.0 0.0
72	0.00	-0.0 4.1	-0.2 -0.0	-0.7 -0.0	-0.9 -0.0	-0.4 -0.0	-0.0 0.0
72	0.10	-0.0 4.1	-0.0 0.3	-0.7 -0.0	-0.9 -0.0	-0.5 -0.0	-0.0 0.0
73	0.00	-0.0 4.1	-0.3 0.0	-0.5 -0.0	-0.6 -0.0	-0.5 -0.0	-0.0 0.0
73	0.10	-0.0 4.1	-0.0 0.2	-0.5 -0.0	-0.6 -0.0	-0.5 -0.0	-0.0 0.0
74	0.00	-0.0 4.1	-0.3 -0.0	-0.3 -0.0	-0.3 -0.0	-0.5 -0.0	-0.0 0.0
74	0.10	-0.0 4.1	-0.0 0.2	-0.3 -0.0	-0.3 -0.0	-0.6 -0.0	-0.0 0.0
75	0.00	-0.0 4.1	-0.3 -0.0	-0.1 -0.0	-0.1 -0.0	-0.6 -0.0	-0.0 0.0
75	0.10	-0.0 4.1	-0.0 0.2	-0.1 -0.0	-0.1 -0.0	-0.6 -0.0	-0.0 0.0
76	0.00	-0.0 4.1	-0.2 0.0	-0.0 0.1	-0.0 0.1	-0.6 -0.0	-0.0 0.0
76	0.10	-0.0 4.1	-0.0 0.3	-0.0 0.1	-0.0 0.1	-0.6 -0.0	-0.0 0.0
77	0.00	-0.0 4.1	-0.2 0.0	-0.0 0.3	-0.0 0.3	-0.6 -0.0	-0.0 0.0

77	0.10	-0.0 4.1	-0.0 0.3	-0.0 0.3	-0.0 0.3	-0.5 -0.0	-0.0 0.0
78	0.00	-0.0 4.1	-0.2 -0.0	-0.0 0.5	-0.0 0.6	-0.5 -0.0	-0.0 0.0
78	0.10	-0.0 4.1	-0.0 0.3	-0.0 0.5	-0.0 0.6	-0.5 -0.0	-0.0 0.0
79	0.00	-0.0 4.1	-0.3 0.0	-0.0 0.7	-0.0 0.9	-0.5 -0.0	-0.0 0.0
79	0.10	-0.0 4.1	-0.0 0.2	-0.0 0.7	-0.0 0.9	-0.4 -0.0	-0.0 0.0
80	0.00	-0.0 4.1	-0.0 0.5	-0.0 1.0	-0.0 1.2	-0.4 -0.0	-0.0 0.0
80	0.10	-0.0 4.1	-0.0 1.0	-0.0 1.0	-0.0 1.2	-0.3 -0.0	-0.1 -0.0
81	0.00	-1.9 -0.0	-11.3 0.0	-149.0 0.0	-0.0 0.2	-0.0 10.6	-2.0 0.0
81	0.10	-1.9 -0.0	-10.3 0.0	-119.0 0.0	-0.0 0.2	-2.8 -0.0	-1.0 0.0
82	0.00	-1.9 -0.0	-9.6 0.0	-119.3 0.0	-0.0 0.2	-2.8 -0.0	-1.0 0.0
82	0.10	-1.9 -0.0	-8.5 0.0	-89.3 0.0	-0.0 0.2	-13.2 -0.0	-0.1 0.0
83	0.00	-1.9 -0.0	-6.9 -0.0	-89.5 0.0	-0.0 0.1	-13.2 -0.0	-0.1 0.0
83	0.10	-1.9 -0.0	-5.8 -0.0	-59.5 0.0	-0.0 0.1	-20.7 -0.0	-0.0 0.6
84	0.00	-1.9 -0.0	-4.3 0.0	-59.7 0.0	-0.0 0.1	-20.7 -0.0	-0.0 0.6
84	0.10	-1.9 -0.0	-3.3 0.0	-29.7 0.0	-0.0 0.1	-25.1 -0.0	-0.0 1.0
85	0.00	-1.9 -0.0	-1.8 0.0	-29.9 0.0	-0.0 0.0	-25.1 -0.0	-0.0 1.0
85	0.10	-1.9 -0.0	-0.8 0.0	-0.0 0.1	-0.0 0.0	-26.6 -0.0	-0.0 1.1
86	0.00	-1.9 -0.0	-0.0 0.8	-0.1 -0.0	-0.0 0.0	-26.6 -0.0	-0.0 1.1
86	0.10	-1.9 -0.0	-0.0 1.8	-0.0 29.9	-0.0 0.0	-25.1 -0.0	-0.0 1.0
87	0.00	-1.9 -0.0	-0.0 3.3	-0.0 29.7	-0.1 0.0	-25.1 -0.0	-0.0 1.0
87	0.10	-1.9 -0.0	-0.0 4.3	-0.0 59.7	-0.1 0.0	-20.7 -0.0	-0.0 0.6
88	0.00	-1.9 -0.0	-0.0 5.8	-0.0 59.5	-0.1 0.0	-20.7 -0.0	-0.0 0.6
88	0.10	-1.9 -0.0	-0.0 6.9	-0.0 89.5	-0.1 0.0	-13.2 -0.0	-0.1 0.0
89	0.00	-1.9 -0.0	-0.0 8.5	-0.0 89.3	-0.2 0.0	-13.2 -0.0	-0.1 0.0
89	0.10	-1.9 -0.0	-0.0 9.6	-0.0 119.3	-0.2 0.0	-2.8 -0.0	-1.0 0.0
90	0.00	-1.9 -0.0	-0.0 10.3	-0.0 119.0	-0.2 0.0	-2.8 -0.0	-1.0 0.0
90	0.10	-1.9 -0.0	-0.0 11.3	-0.0 149.0	-0.2 0.0	-0.0 10.6	-2.0 0.0
109	0.00	-1.8 -0.0	-0.0 10.5	-0.0 121.0	-0.0 8.6	-5.6 -0.0	-1.0 -0.0
109	0.10	-1.8 -0.0	-0.0 11.5	-0.0 151.0	-0.0 8.6	-0.0 8.0	-2.1 -0.0
110	0.00	-1.9 -0.0	-0.0 8.7	-0.0 91.2	-0.0 8.6	-16.2 -0.0	-0.1 0.0
110	0.10	-1.9 -0.0	-0.0 9.7	-0.0 121.2	-0.0 8.6	-5.6 -0.0	-1.0 -0.0
111	0.00	-1.9 -0.0	-0.0 6.0	-0.0 61.5	-0.0 8.6	-23.9 -0.0	-0.0 0.5
111	0.10	-1.9 -0.0	-0.0 7.0	-0.0 91.5	-0.0 8.6	-16.2 -0.0	-0.1 0.0
112	0.00	-1.9 -0.0	-0.0 3.4	-0.0 31.6	-0.0 8.7	-28.5 -0.0	-0.0 0.9
112	0.10	-1.9 -0.0	-0.0 4.4	-0.0 61.6	-0.0 8.7	-23.8 -0.0	-0.0 0.5
113	0.00	-1.9 -0.0	-0.0 0.9	-0.0 1.8	-0.0 8.7	-30.2 -0.0	-0.0 1.1
113	0.10	-1.9 -0.0	-0.0 1.9	-0.0 31.8	-0.0 8.7	-28.5 -0.0	-0.0 0.9
114	0.00	-1.9 -0.0	-1.6 0.0	-28.0 -0.0	-0.0 8.8	-28.8 -0.0	-0.0 0.9
114	0.10	-1.9 -0.0	-0.6 0.0	-0.0 2.0	-0.0 8.8	-30.1 -0.0	-0.0 1.1
115	0.00	-1.9 -0.0	-4.1 0.0	-57.8 -0.0	-0.0 8.8	-24.5 -0.0	-0.0 0.6
115	0.10	-1.9 -0.0	-3.1 0.0	-27.8 -0.0	-0.0 8.8	-28.8 -0.0	-0.0 0.9
116	0.00	-1.9 -0.0	-6.7 0.0	-87.6 -0.0	-0.0 8.9	-17.3 -0.0	-0.1 0.0
116	0.10	-1.9 -0.0	-5.7 0.0	-57.6 -0.0	-0.0 8.9	-24.5 -0.0	-0.0 0.6
117	0.00	-1.9 -0.0	-9.4 0.0	-117.4 -0.0	-0.0 8.9	-7.0 -0.0	-0.9 0.0
117	0.10	-1.9 -0.0	-8.4 0.0	-87.4 -0.0	-0.0 8.9	-17.3 -0.0	-0.1 0.0
118	0.00	-1.9 -0.0	-11.2 0.0	-147.1 -0.0	-0.0 8.9	-0.0 6.2	-2.0 0.0
118	0.10	-1.9 -0.0	-10.2 0.0	-117.1 -0.0	-0.0 8.9	-7.0 -0.0	-0.9 0.0

119	0.00	-0.0	-0.0	-2.7	-0.0	-1.9	-0.0
		4.1	0.5	-0.0	1.2	-0.0	0.0
119	0.10	-0.0	-0.0	-2.7	-0.0	-2.2	-0.1
		4.1	1.0	-0.0	1.2	-0.0	-0.0
120	0.00	-0.0	-0.3	-2.9	-0.0	-1.6	-0.0
		4.1	0.0	-0.0	0.9	-0.0	0.0
120	0.10	-0.0	-0.0	-2.9	-0.0	-1.9	-0.0
		4.1	0.2	-0.0	0.9	-0.0	0.0
121	0.00	-0.0	-0.2	-3.1	-0.0	-1.3	-0.0
		4.1	0.0	-0.0	0.7	-0.0	0.0
121	0.10	-0.0	-0.0	-3.1	-0.0	-1.7	-0.0
		4.1	0.3	-0.0	0.7	-0.0	0.0
122	0.00	-0.0	-0.2	-3.3	-0.0	-1.0	-0.0
		4.1	0.0	-0.0	0.4	-0.0	0.0
122	0.10	-0.0	-0.0	-3.3	-0.0	-1.4	-0.0
		4.1	0.3	-0.0	0.4	-0.0	-0.0
123	0.00	-0.0	-0.2	-3.5	-0.0	-0.7	-0.0
		4.1	0.0	-0.0	0.2	-0.0	0.0
123	0.10	-0.0	-0.0	-3.5	-0.0	-1.0	-0.0
		4.1	0.3	-0.0	0.2	-0.0	0.0
124	0.00	-0.0	-0.3	-3.7	-0.0	-0.3	-0.0
		4.1	0.0	-0.0	0.0	-0.0	0.0
124	0.10	-0.0	-0.0	-3.7	-0.0	-0.7	-0.0
		4.1	0.2	-0.0	0.0	-0.0	0.0
125	0.00	-0.0	-0.3	-3.8	-0.2	-0.0	-0.0
		4.1	0.0	-0.0	0.0	0.0	0.0
125	0.10	-0.0	-0.0	-3.8	-0.2	-0.4	-0.0
		4.1	0.2	-0.0	0.0	-0.0	0.0
126	0.00	-0.0	-0.3	-4.0	-0.5	-0.0	-0.0
		4.1	0.0	-0.0	0.0	0.4	0.0
126	0.10	-0.0	-0.0	-4.0	-0.5	-0.0	-0.0
		4.1	0.2	-0.0	0.0	0.0	0.0
127	0.00	-0.0	-0.2	-4.3	-0.8	-0.0	-0.0
		4.1	0.0	-0.0	0.0	0.8	0.0
127	0.10	-0.0	-0.0	-4.3	-0.8	-0.0	-0.0
		4.1	0.3	-0.0	0.0	0.4	0.0
128	0.00	-0.0	-1.0	-4.6	-1.1	-0.0	-0.1
		4.1	0.0	-0.0	0.0	1.3	0.0
128	0.10	-0.0	-0.5	-4.6	-1.1	-0.0	-0.0
		4.1	0.0	-0.0	0.0	0.8	0.0
130	0.00	-0.0	-0.2	-0.4	-0.1	-0.0	-341.1
		273.8	42.6	0.6	0.1	10.2	0.0
130	0.04	-0.0	-0.2	-0.4	-0.1	-0.0	-342.8
		273.8	43.2	0.6	0.1	10.2	-0.0
133	0.00	-0.0	-0.0	-2.4	-0.2	-0.0	-249.7
		174.5	28.7	-0.0	0.0	20.1	-0.0
133	0.04	-0.0	-0.0	-2.4	-0.2	-0.0	-250.9
		174.5	29.2	-0.0	0.0	20.0	-0.0
135	0.00	-0.0	-1.1	-8.6	-0.8	-0.0	-0.1
		4.4	0.0	0.0	0.0	3.0	0.0
135	0.10	-0.0	-0.5	-8.6	-0.8	-0.0	-0.0
		4.4	0.0	0.0	0.0	2.2	0.0
136	0.00	-0.0	-0.2	-8.3	-0.5	-0.0	-0.0
		4.4	0.0	0.0	0.0	2.2	0.0
136	0.10	-0.0	-0.0	-8.3	-0.5	-0.0	-0.0
		4.4	0.3	0.0	0.0	1.4	0.0
137	0.00	-0.0	-0.3	-8.1	-0.3	-0.0	-0.0
		4.4	0.0	0.0	0.0	1.4	0.0
137	0.10	-0.0	-0.0	-8.1	-0.3	-0.0	-0.0
		4.4	0.2	0.0	0.0	0.6	0.0
138	0.00	-0.0	-0.3	-7.9	-0.0	-0.0	-0.0
		4.4	0.0	0.0	0.0	0.6	0.0
138	0.10	-0.0	-0.0	-7.9	-0.0	-0.2	-0.0
		4.4	0.2	0.0	0.0	-0.0	0.0
139	0.00	-0.0	-0.3	-7.8	-0.0	-0.1	-0.0
		4.4	0.0	0.0	0.2	-0.0	0.0
139	0.10	-0.0	-0.0	-7.8	-0.0	-0.9	-0.0
		4.4	0.2	0.0	0.2	0.0	0.0
140	0.00	-0.0	-0.2	-7.7	-0.0	-0.9	-0.0
		4.4	0.0	0.0	0.3	0.0	0.0
140	0.10	-0.0	-0.0	-7.7	-0.0	-1.6	-0.0
		4.4	0.3	0.0	0.3	0.0	0.0
141	0.00	-0.0	-0.2	-7.5	-0.0	-1.6	-0.0
		4.4	0.0	0.0	0.5	0.0	0.0
141	0.10	-0.0	-0.0	-7.5	-0.0	-2.4	-0.0
		4.4	0.3	0.0	0.5	0.0	0.0
142	0.00	-0.0	-0.2	-7.4	-0.0	-2.3	-0.0
		4.4	0.0	0.0	0.7	0.0	0.0
142	0.10	-0.0	-0.0	-7.4	-0.0	-3.1	-0.0
		4.4	0.3	0.0	0.7	0.0	0.0
143	0.00	-0.0	-0.3	-7.3	-0.0	-3.0	-0.0
		4.4	0.0	0.0	0.9	0.0	0.0
143	0.10	-0.0	-0.0	-7.3	-0.0	-3.8	-0.0
		4.4	0.2	0.0	0.9	0.0	0.0
144	0.00	-0.0	-0.0	-7.1	-0.0	-3.7	-0.0
		4.3	1.1	0.0	1.1	0.0	0.0
144	0.10	-0.0	-0.0	-7.1	-0.0	-4.4	-0.1
		4.3	1.6	0.0	1.1	0.0	-0.0
145	0.00	-2.0	-12.0	-116.9	-0.0	-7.4	-2.2
		-0.0	0.1	0.0	16.7	-0.0	0.1
145	0.10	-2.0	-11.0	-86.9	-0.0	-17.6	-1.0
		-0.0	0.1	0.0	16.7	-0.0	0.1
146	0.00	-2.0	-10.3	-87.2	-0.0	-17.6	-1.1
		-0.0	0.2	0.0	16.7	-0.0	0.1
146	0.10	-2.0	-9.3	-57.2	-0.0	-24.9	-0.1

		-0.0	0.2	0.0	16.7	-0.0	0.1
147	0.00	-2.0	-7.6	-57.4	-0.0	-24.9	-0.1
		-0.0	0.2	0.0	16.7	-0.0	0.1
147	0.10	-2.0	-6.6	-27.4	-0.0	-29.1	-0.0
		-0.0	0.2	0.0	16.7	-0.0	0.6
148	0.00	-2.0	-5.0	-27.6	-0.0	-29.1	-0.0
		-0.0	0.2	0.0	16.6	-0.0	0.6
148	0.10	-2.0	-4.0	-0.0	-0.0	-30.4	-0.0
		-0.0	0.2	2.4	16.6	-0.0	1.1
149	0.00	-2.0	-2.5	-0.0	-0.0	-30.4	-0.0
		-0.0	0.2	2.3	16.6	-0.0	1.1
149	0.10	-2.0	-1.5	-0.0	-0.0	-28.7	-0.0
		-0.0	0.2	32.3	16.6	-0.0	1.3
150	0.00	-2.0	-0.2	-0.0	-0.0	-28.7	-0.0
		-0.0	0.2	32.1	16.5	-0.0	1.3
150	0.10	-2.0	-0.0	-0.0	-0.0	-24.0	-0.0
		-0.0	1.0	62.1	16.5	-0.0	1.2
151	0.00	-2.0	-0.0	-0.0	-0.0	-24.1	-0.0
		-0.0	2.5	62.0	16.5	-0.0	1.2
151	0.10	-2.0	-0.0	-0.0	-0.0	-16.4	-0.0
		-0.0	3.6	92.0	16.5	0.0	0.9
152	0.00	-2.0	-0.0	-0.0	-0.0	-16.4	-0.0
		-0.0	5.1	91.9	16.4	0.0	0.9
152	0.10	-2.0	-0.0	-0.0	-0.0	-5.7	-0.1
		-0.0	6.1	121.9	16.4	0.0	0.4
153	0.00	-2.0	-0.0	-0.0	-0.0	-5.7	-0.1
		-0.0	7.8	121.8	16.3	0.0	0.4
153	0.10	-2.0	-0.0	-0.0	-0.0	-0.0	-0.5
		-0.0	8.8	151.8	16.3	7.9	-0.0
154	0.00	-1.9	-0.0	-0.0	-0.0	-0.0	-0.5
		-0.0	8.9	151.6	16.3	7.9	-0.0
154	0.10	-1.9	-0.0	-0.0	-0.0	-0.0	-1.4
		-0.0	9.9	181.6	16.3	24.6	-0.0

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RISULTATI : SOLLECITAZIONI INVILUPPO PILASTRI

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ELEM. n.ro	ascissa (m)	N (Kg) min/max	V2 (Kg) min/max	V3 (Kg) min/max	T (Kg*m) min/max	M2 (Kg*m) min/max	M3 (Kg*m) min/max
1	0.00	-28.7	-0.0	-0.0	-0.0	-249.7	-0.0
		-0.0	2.4	174.5	20.1	-0.0	0.2
1	0.27	-25.1	-0.0	-0.0	-0.0	-202.6	-0.5
		-0.0	2.4	174.5	20.1	-0.0	-0.0
3	0.00	-23.4	-1.9	-0.0	-0.0	-201.5	-0.6
		-0.0	-0.0	181.6	24.6	-0.0	-0.0
3	1.02	-9.9	-1.9	-0.0	-0.0	-16.3	-0.0
		-0.0	-0.0	181.6	24.6	-0.0	1.4
4	0.00	-37.0	-0.1	-0.0	-0.0	-265.2	-0.1
		0.1	0.2	267.9	15.4	0.0	0.1
4	1.02	-23.5	-0.1	-0.0	-0.0	-0.0	-0.1
		0.1	0.2	267.9	15.4	8.1	0.1
6	0.00	-42.6	-0.6	-0.0	-0.0	-341.1	-0.1
		0.2	0.4	273.8	10.2	0.0	0.1
6	0.27	-39.1	-0.6	-0.0	-0.0	-267.2	-0.0
		0.2	0.4	273.8	10.2	0.0	0.1
27	0.00	-0.9	-0.0	-0.0	-0.0	-0.2	-0.0
		-0.0	-0.0	0.2	0.0	-0.0	-0.0
27	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		0.1	-0.0	0.2	0.0	-0.0	0.0
28	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.6	-0.0	0.1	0.0	-0.0	-0.0
28	1.02	-0.0	-0.0	-0.0	-0.0	-0.1	-0.0
		1.6	-0.0	0.1	0.0	0.0	0.0
29	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	-0.0	0.1	0.0	-0.0	-0.0
29	1.02	-0.0	-0.0	-0.0	-0.0	-0.1	-0.0
		1.6	-0.0	0.1	0.0	0.0	0.0
30	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	-0.0	0.1	0.0	-0.0	-0.0
30	1.02	-0.0	-0.0	-0.0	-0.0	-0.1	-0.0
		1.5	-0.0	0.1	0.0	0.0	0.0
31	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	0.0	0.1	0.0	-0.0	0.0
31	1.02	-0.0	-0.0	-0.0	-0.0	-0.1	-0.0
		1.5	0.0	0.1	0.0	0.0	0.0
32	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	0.0	0.1	0.0	0.0	0.0
32	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.5	0.0	0.1	0.0	0.0	0.0
33	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	0.0	0.2	0.0	0.0	0.0
33	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.6	0.0	0.2	0.0	0.0	0.0
34	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.6	0.0	0.2	0.0	0.0	0.0
34	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.7	0.0	0.2	0.0	-0.0	0.0
35	0.00	-0.3	-0.0	-0.0	-0.0	-0.3	-0.0
		0.0	0.0	0.3	0.0	0.0	0.0
35	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		0.7	0.0	0.3	0.0	-0.0	0.0
36	0.00	-0.3	-0.0	-0.0	-0.0	-0.3	-0.0
		0.0	0.0	0.3	0.0	0.0	0.0
36	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		0.8	0.0	0.3	0.0	0.0	0.0

37	0.00	-0.0	-0.0	-0.0	-0.0	-0.3	-0.0
		0.6	0.0	0.2	0.0	0.0	0.0
37	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.7	0.0	0.2	0.0	0.0	0.0
38	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	0.0	0.2	0.0	0.0	0.0
38	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.5	0.0	0.2	0.0	0.0	0.0
39	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	0.0	0.2	0.0	0.0	0.0
39	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.5	0.0	0.2	0.0	0.0	0.0
40	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	-0.0	0.2	0.0	0.0	-0.0
40	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.5	-0.0	0.2	0.0	0.0	0.0
41	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	-0.0	0.2	0.0	0.0	-0.0
41	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.5	-0.0	0.2	0.0	0.0	0.0
42	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	-0.0	0.2	0.0	0.0	-0.0
42	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.6	-0.0	0.2	0.0	0.0	0.0
43	0.00	-0.0	-0.0	-0.0	-0.0	-0.3	-0.0
		0.6	-0.0	0.2	0.0	0.0	-0.0
43	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.7	-0.0	0.2	0.0	0.0	0.0
44	0.00	-0.3	-0.0	-0.0	-0.0	-0.3	-0.0
		-0.0	-0.0	0.3	0.0	0.0	-0.0
44	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		0.7	-0.0	0.3	0.0	-0.0	0.0
65	0.00	-41.6	-0.1	-0.0	-0.0	-376.7	-0.0
		0.0	0.1	301.7	2.8	0.0	0.0
65	0.27	-38.0	-0.1	-0.0	-0.0	-295.2	-0.0
		0.0	0.1	301.7	2.8	0.0	0.0
67	0.00	-36.0	-0.0	-0.0	-0.0	-292.9	-0.0
		0.0	-0.0	296.1	4.4	0.0	0.0
67	1.02	-22.5	-0.0	-0.0	-0.0	-0.0	-0.0
		0.0	-0.0	296.1	4.4	9.1	0.0
68	0.00	-36.0	-0.0	-0.0	-4.4	-292.9	-0.0
		0.0	0.0	296.1	-0.0	0.0	0.0
68	1.02	-22.5	-0.0	-0.0	-4.4	-0.0	-0.0
		0.0	0.0	296.1	-0.0	9.1	-0.0
70	0.00	-41.6	-0.1	-0.0	-2.8	-376.7	-0.0
		0.0	0.1	301.7	-0.0	0.0	0.0
70	0.27	-38.0	-0.1	-0.0	-2.8	-295.2	-0.0
		0.0	0.1	301.7	-0.0	0.0	0.0
91	0.00	-0.3	-0.0	-0.0	-0.0	-0.3	-0.0
		-0.0	-0.0	0.3	0.0	0.0	-0.0
91	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		0.7	-0.0	0.3	0.0	0.0	0.0
92	0.00	-0.0	-0.0	-0.0	-0.0	-0.3	-0.0
		0.6	-0.0	0.2	0.0	0.0	-0.0
92	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.7	-0.0	0.2	0.0	0.0	0.0
93	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	-0.0	0.2	0.0	-0.0	-0.0
93	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.6	-0.0	0.2	0.0	0.0	0.0
94	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	-0.0	0.2	0.0	-0.0	-0.0
94	1.02	-0.0	-0.0	-0.0	-0.0	-0.1	-0.0
		1.5	-0.0	0.2	0.0	0.0	0.0
95	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	-0.0	0.2	0.0	-0.0	0.0
95	1.02	-0.0	-0.0	-0.0	-0.0	-0.1	-0.0
		1.5	-0.0	0.2	0.0	0.0	0.0
96	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	0.0	0.2	-0.0	-0.0	0.0
96	1.02	-0.0	-0.0	-0.0	-0.0	-0.1	-0.0
		1.5	0.0	0.2	-0.0	0.0	-0.0
97	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	0.0	0.2	-0.0	-0.0	0.0
97	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.6	0.0	0.2	-0.0	0.0	-0.0
98	0.00	-0.0	-0.0	-0.0	-0.0	-0.3	-0.0
		0.6	0.0	0.2	-0.0	0.0	0.0
98	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.7	0.0	0.2	-0.0	0.0	-0.0
99	0.00	-0.3	-0.0	-0.0	-0.0	-0.3	-0.0
		-0.0	0.0	0.3	-0.0	0.0	0.0
99	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		0.7	0.0	0.3	-0.0	0.0	-0.0
100	0.00	-0.3	-0.0	-0.0	-0.0	-0.3	-0.0
		-0.0	0.0	0.3	-0.0	0.0	0.0
100	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		0.7	0.0	0.3	-0.0	-0.0	-0.0
101	0.00	-0.0	-0.0	-0.0	-0.0	-0.3	-0.0
		0.6	0.0	0.2	-0.0	0.0	0.0
101	1.02	-0.0	-0.0	-0.0	-0.0	-0.0	-0.0
		1.7	0.0	0.2	-0.0	0.0	-0.0
102	0.00	-0.0	-0.0	-0.0	-0.0	-0.2	-0.0
		0.5	0.0	0.2	-0.0	0.0	0.0

ELEM. n.ro	numero dell' elemento trave
x	ascissa locale misurata dal nodo I al nodo J
N	sforzo normale nel p.to x
V2	forza di taglio ' ' ' in direz. 2 locale
V3	forza di taglio ' ' ' ' ' 3 '
T	momento torcente ' ' ' '
M2	momento flettente ' ' ' intorno asse 2 loc.
M3	momento flettente ' ' ' ' ' 3 '
SEZIONE	dimensioni della sezione trasversale della trave (per rettangolari, circolari, T, L, per le altre tipologie si riporta solo il tipo: es. T 60/30x50, o sez.polig. etc. Coeff.sicurezza = rapporto tra azioni ultime ed azioni di calcolo N,M
C.sic.	
Vrdu2	taglio max. ammissibile per la verifica bielle di conglomerato
Vrdu3	taglio max. ammissibile per la verifica armatura trasversale d'anima
Trdu	mom. torcente max. ammissibile per verifica bielle di conglomerato
sc max	tensione max (in senso algebrico) nel c/c (poiche' le tensioni di compressione sono

=====													
ELEM.	tipo sezione	tipo	L	Peso	Arid/A	Classe prof.			Beta	Beta	snel.	curva	X
n.ro		acc.	(m)	(Kg)		N	M2	M3	fles. 1-2 1-3	tors. 1-2 1-3	1-2 1-3	1-2 1-3	1-2 1-3
1	RC 6x6/4.8x4.8	S235	0.27	2.7	1.0	1	1	1	1.0	1.0	12.2	a	1.00
2	RC 6x6/4.8x4.8	S235	0.04	0.4	1.0	1	1	1	1.0	1.0	12.2	a	1.00
3	RC 6x6/4.8x4.8	S235	1.02	10.4	1.0	1	1	1	1.0	1.0	1.8	a	1.00
4	RC 6x6/4.8x4.8	S235	1.02	10.4	1.0	1	1	1	1.0	1.0	1.8	a	1.00
5	RC 6x6/4.8x4.8	S235	0.04	0.4	1.0	1	1	1	1.0	1.0	46.0	a	0.93
6	RC 6x6/4.8x4.8	S235	0.27	2.7	1.0	1	1	1	1.0	1.0	46.0	a	0.93
7	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	46.0	a	0.93
8	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	1.8	a	1.00
9	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	1.8	a	1.00
10	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	12.2	a	1.00
11	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	12.2	a	1.00
12	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
13	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	6.9	c	1.00
14	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
15	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	6.9	c	1.00
16	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
17	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	6.9	c	1.00
18	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
19	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	4.5	a	1.00
20	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
21	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	4.5	a	1.00
22	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
23	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	4.5	a	1.00
24	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
25	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	4.5	a	1.00
26	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
27	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	4.5	a	1.00
28	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
29	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
30	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
31	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
32	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
33	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
34	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
35	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
36	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
37	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
38	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
39	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
40	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
41	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
42	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
43	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
44	RETT. b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
45	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
46	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
47	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	4.5	a	1.00
48	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
49	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	4.5	a	1.00
50	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
51	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	4.5	a	1.00
52	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
53	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	4.5	a	1.00
54	RC 6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
55	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	4.5	a	1.00
56	RETT. b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91

[illegible]

116	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	4.5	a	1.00
										1.0		5.3	a	1.00
										1.0		4.5	a	1.00
117	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
118	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
119	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
120	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
121	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
122	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
123	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
124	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
125	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
126	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
127	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
128	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
129	RC	6x6/4.8x4.8	S235	0.27	2.7	1.0	1	1	1	1.0	1.0	12.2	a	1.00
										1.0		12.2	a	1.00
130	RC	6x6/4.8x4.8	S235	0.04	0.4	1.0	1	1	1	1.0	1.0	1.8	a	1.00
										1.0		1.8	a	1.00
131	RC	6x6/4.8x4.8	S235	1.02	10.4	1.0	1	1	1	1.0	1.0	46.0	a	0.93
										1.0		46.0	a	0.93
132	RC	6x6/4.8x4.8	S235	1.02	10.4	1.0	1	1	1	1.0	1.0	46.0	a	0.93
										1.0		46.0	a	0.93
133	RC	6x6/4.8x4.8	S235	0.04	0.4	1.0	1	1	1	1.0	1.0	1.8	a	1.00
										1.0		1.8	a	1.00
134	RC	6x6/4.8x4.8	S235	0.27	2.7	1.0	1	1	1	1.0	1.0	12.2	a	1.00
										1.0		12.2	a	1.00
135	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
136	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
137	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
138	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
139	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
140	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
141	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
142	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
143	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
144	RETT.	b=5. h=1.	S235	0.10	0.4	1.0	1	1	1	1.0	1.0	34.6	c	0.91
										1.0		6.9	c	1.00
145	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
146	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
147	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
148	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
149	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
150	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
151	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
152	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
153	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
154	RC	6x5/5x4	S235	0.10	0.8	1.0	1	1	1	1.0	1.0	5.3	a	1.00
										1.0		4.5	a	1.00
155	RETT.	b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
										1.0		353.3	c	0.06
156	RETT.	b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
										1.0		353.3	c	0.06
157	RETT.	b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
										1.0		353.3	c	0.06
158	RETT.	b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
										1.0		353.3	c	0.06
159	RETT.	b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
										1.0		353.3	c	0.06
160	RETT.	b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
										1.0		353.3	c	0.06
161	RETT.	b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
										1.0		353.3	c	0.06
162	RETT.	b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
										1.0		353.3	c	0.06
163	RETT.	b=1. h=1.	S235	1.02	0.8	1.0	1	1	1	1.0	1.0	353.3	c	0.06
										1.0		353.3	c	0.06

DESCRIZIONE TABELLA VALORI EFFICACI SEZIONI IN CLASSE 4

Di seguito si riportano le spiegazioni delle sigle usate nelle tabelle VALORI EFFICACI SEZIONI IN CLASSE 4.

Le sezioni sono riferite al sistema di riferimento 'locale', nel piano trasversale di travi, pilastri ed aste (assi locali 2, 3). Nelle tabelle sono usate sigle il cui significato e' illustrato nella documentazione fornita con il programma.

Aree ed inerzie sono nel rif. locale:

Aeff_comp area efficace a compressione
Aeff_traz area efficace a trazione
W2pos modulo resistenza efficace per momento M2+
W2neg modulo resistenza efficace per momento M2 -
W3pos modulo resistenza efficace per momento M3+
W3neg modulo resistenza efficace per momento M3 -

DESCRIZIONE TABELLA VERIFICA ASTE, TRAVI, PILASTRI IN ACCIAIO

Di seguito si riportano le spiegazioni delle sigle usate nella tabella VERIFICA ASTE, TRAVI, PILASTRI IN ACCIAIO

ELEM. n.ro numero dell' elemento asta, trave o pilastro
 CDC n.ro n.ro del caso di carico
 COMB n.ro n.ro della combinazione di carico
 Sigma snerv. tensione di snervamento in Kg/cm2
 C_sfrut res. coeff.di sfruttamento a resistenza max: OK se <= 1.
 C_sfrut stab. coeff.di sfruttamento max a stabilita': OK se <= 1.
 Tipo ver. tipo di verifica a stabilita', con i seguenti
 stab. significati :
 0 nessuna verifica di stabilita' necessaria
 1 aste compresse (NTC 4.2.4, EC3 5.5.1)
 2 presso-flessione (NTC 4.2.4, EC3 5.5.4)
 3 presso-flessione + svergolamento (NTC 4.2.4, EC3 5.5.4)
 4 instabilita' flessio-torsionale (NTC 4.2.4, EC3 5.5.2)
 M2eq_pf momento equivalente per presso-flessione relativo
 alla flessione nel piano definito dagli assi 1-3
 (=0. se l' elemento non e' compresso e/o inflesso)
 M3eq_pf momento equivalente per presso-flessione relativo
 alla flessione nel piano definito dagli assi 1-2
 (=0. se l' elemento non e' compresso e/o inflesso)
 Meq_sverg momento equivalente per lo svergolamento nel piano
 di flessione 1-2
 (= 0. se non e' presente il momento M3)
 nv elemento non verificato ad una delle seguenti
 condizioni : resistenza, stabilita'

ELEM. n.ro	CDC n.ro	COMB n.ro	C_sfrut res.	C_sfrut stab.	Tipo ver. stab.	M2eq_pf (Kg*m)	M3eq_pf (Kg*m)	Meq_sverg (Kg*m)
1		1	0.42	0.00	0	0.0	0.0	0.0
2		1	0.46	0.00	0	0.0	0.0	0.0
3		1	0.34	0.00	0	0.0	0.0	0.0
4		1	0.44	0.00	0	0.0	0.0	0.0
5		1	0.60	0.00	0	0.0	0.0	0.0
6		1	0.57	0.00	0	0.0	0.0	0.0
7		1	0.04	0.00	0	0.0	0.0	0.0
8		1	0.03	0.00	0	0.0	0.0	0.0
9		1	0.02	0.00	0	0.0	0.0	0.0
10		1	0.02	0.00	0	0.0	0.0	0.0
11		1	0.01	0.00	0	0.0	0.0	0.0
12		1	0.01	0.00	0	0.0	0.0	0.0
13		1	0.00	0.00	0	0.0	0.0	0.0
14		1	0.01	0.00	0	0.0	0.0	0.0
15		1	0.02	0.00	0	0.0	0.0	0.0
16		1	0.02	0.00	0	0.0	0.0	0.0
17		1	0.06	0.00	0	0.0	0.0	0.0
18		1	0.02	0.00	0	0.0	0.0	0.0
19		1	0.04	0.00	0	0.0	0.0	0.0
20		1	0.06	0.00	0	0.0	0.0	0.0
21		1	0.07	0.00	0	0.0	0.0	0.0
22		1	0.07	0.00	0	0.0	0.0	0.0
23		1	0.07	0.00	0	0.0	0.0	0.0
24		1	0.07	0.00	0	0.0	0.0	0.0
25		1	0.05	0.00	0	0.0	0.0	0.0
26		1	0.04	0.00	0	0.0	0.0	0.0
27		1	0.04	0.00	0	0.0	0.0	0.0
28		1	0.04	0.00	0	0.0	0.0	0.0
29		1	0.03	0.00	0	0.0	0.0	0.0
30		1	0.03	0.00	0	0.0	0.0	0.0
31		1	0.03	0.00	0	0.0	0.0	0.0
32		1	0.03	0.00	0	0.0	0.0	0.0
33		1	0.04	0.00	0	0.0	0.0	0.0
34		1	0.04	0.00	0	0.0	0.0	0.0
35		1	0.05	0.00	0	0.0	0.0	0.0
36		1	0.06	0.00	0	0.0	0.0	0.0
37		1	0.05	0.00	0	0.0	0.0	0.0
38		1	0.04	0.00	0	0.0	0.0	0.0
39		1	0.04	0.00	0	0.0	0.0	0.0
40		1	0.04	0.00	0	0.0	0.0	0.0
41		1	0.04	0.00	0	0.0	0.0	0.0
42		1	0.04	0.00	0	0.0	0.0	0.0
43		1	0.05	0.00	0	0.0	0.0	0.0
44		1	0.05	0.00	0	0.0	0.0	0.0
45		1	0.02	0.00	0	0.0	0.0	0.0
46		1	0.04	0.00	0	0.0	0.0	0.0
47		1	0.06	0.00	0	0.0	0.0	0.0
48		1	0.07	0.00	0	0.0	0.0	0.0
49		1	0.07	0.00	0	0.0	0.0	0.0
50		1	0.07	0.00	0	0.0	0.0	0.0
51		1	0.06	0.00	0	0.0	0.0	0.0
52		1	0.05	0.00	0	0.0	0.0	0.0
53		1	0.03	0.00	0	0.0	0.0	0.0
54		1	0.02	0.00	0	0.0	0.0	0.0
55		1	0.01	0.00	0	0.0	0.0	0.0
56		1	0.01	0.00	0	0.0	0.0	0.0
57		1	0.00	0.00	0	0.0	0.0	0.0
58		1	0.00	0.00	0	0.0	0.0	0.0
59		1	0.01	0.00	0	0.0	0.0	0.0
60		1	0.01	0.00	0	0.0	0.0	0.0
61		1	0.01	0.00	0	0.0	0.0	0.0
62		1	0.01	0.00	0	0.0	0.0	0.0
63		1	0.01	0.00	0	0.0	0.0	0.0
64		1	0.02	0.00	0	0.0	0.0	0.0
65		1	0.63	0.00	0	0.0	0.0	0.0
66		1	0.64	0.00	0	0.0	0.0	0.0
67		1	0.49	0.00	0	0.0	0.0	0.0
68		1	0.49	0.00	0	0.0	0.0	0.0
69		1	0.64	0.00	0	0.0	0.0	0.0
70		1	0.63	0.00	0	0.0	0.0	0.0
71		1	0.00	0.00	0	0.0	0.0	0.0
72		1	0.00	0.00	0	0.0	0.0	0.0
73		1	0.00	0.00	0	0.0	0.0	0.0
74		1	0.00	0.00	0	0.0	0.0	0.0
75		1	0.00	0.00	0	0.0	0.0	0.0
76		1	0.00	0.00	0	0.0	0.0	0.0
77		1	0.00	0.00	0	0.0	0.0	0.0
78		1	0.00	0.00	0	0.0	0.0	0.0
79		1	0.00	0.00	0	0.0	0.0	0.0
80		1	0.00	0.00	0	0.0	0.0	0.0
81		1	0.03	0.00	0	0.0	0.0	0.0
82		1	0.03	0.00	0	0.0	0.0	0.0
83		1	0.05	0.00	0	0.0	0.0	0.0
84		1	0.06	0.00	0	0.0	0.0	0.0
85		1	0.06	0.00	0	0.0	0.0	0.0
86		1	0.06	0.00	0	0.0	0.0	0.0

87	1	0.06	0.00	0	0.0	0.0	0.0
88	1	0.05	0.00	0	0.0	0.0	0.0
89	1	0.03	0.00	0	0.0	0.0	0.0
90	1	0.03	0.00	0	0.0	0.0	0.0
91	1	0.06	0.00	0	0.0	0.0	0.0
92	1	0.05	0.00	0	0.0	0.0	0.0
93	1	0.04	0.00	0	0.0	0.0	0.0
94	1	0.04	0.00	0	0.0	0.0	0.0
95	1	0.04	0.00	0	0.0	0.0	0.0
96	1	0.04	0.00	0	0.0	0.0	0.0
97	1	0.04	0.00	0	0.0	0.0	0.0
98	1	0.05	0.00	0	0.0	0.0	0.0
99	1	0.06	0.00	0	0.0	0.0	0.0
100	1	0.05	0.00	0	0.0	0.0	0.0
101	1	0.05	0.00	0	0.0	0.0	0.0
102	1	0.04	0.00	0	0.0	0.0	0.0
103	1	0.04	0.00	0	0.0	0.0	0.0
104	1	0.04	0.00	0	0.0	0.0	0.0
105	1	0.04	0.00	0	0.0	0.0	0.0
106	1	0.04	0.00	0	0.0	0.0	0.0
107	1	0.05	0.00	0	0.0	0.0	0.0
108	1	0.06	0.00	0	0.0	0.0	0.0
109	1	0.02	0.00	0	0.0	0.0	0.0
110	1	0.04	0.00	0	0.0	0.0	0.0
111	1	0.05	0.00	0	0.0	0.0	0.0
112	1	0.06	0.00	0	0.0	0.0	0.0
113	1	0.07	0.00	0	0.0	0.0	0.0
114	1	0.07	0.00	0	0.0	0.0	0.0
115	1	0.07	0.00	0	0.0	0.0	0.0
116	1	0.05	0.00	0	0.0	0.0	0.0
117	1	0.04	0.00	0	0.0	0.0	0.0
118	1	0.02	0.00	0	0.0	0.0	0.0
119	1	0.02	0.00	0	0.0	0.0	0.0
120	1	0.01	0.00	0	0.0	0.0	0.0
121	1	0.01	0.00	0	0.0	0.0	0.0
122	1	0.01	0.00	0	0.0	0.0	0.0
123	1	0.01	0.00	0	0.0	0.0	0.0
124	1	0.01	0.00	0	0.0	0.0	0.0
125	1	0.00	0.00	0	0.0	0.0	0.0
126	1	0.00	0.00	0	0.0	0.0	0.0
127	1	0.01	0.00	0	0.0	0.0	0.0
128	1	0.01	0.00	0	0.0	0.0	0.0
129	1	0.57	0.00	0	0.0	0.0	0.0
130	1	0.60	0.00	0	0.0	0.0	0.0
131	1	0.44	0.00	0	0.0	0.0	0.0
132	1	0.34	0.00	0	0.0	0.0	0.0
133	1	0.46	0.00	0	0.0	0.0	0.0
134	1	0.42	0.00	0	0.0	0.0	0.0
135	1	0.02	0.00	0	0.0	0.0	0.0
136	1	0.02	0.00	0	0.0	0.0	0.0
137	1	0.01	0.00	0	0.0	0.0	0.0
138	1	0.00	0.00	0	0.0	0.0	0.0
139	1	0.01	0.00	0	0.0	0.0	0.0
140	1	0.01	0.00	0	0.0	0.0	0.0
141	1	0.02	0.00	0	0.0	0.0	0.0
142	1	0.02	0.00	0	0.0	0.0	0.0
143	1	0.03	0.00	0	0.0	0.0	0.0
144	1	0.04	0.00	0	0.0	0.0	0.0
145	1	0.04	0.00	0	0.0	0.0	0.0
146	1	0.05	0.00	0	0.0	0.0	0.0
147	1	0.06	0.00	0	0.0	0.0	0.0
148	1	0.07	0.00	0	0.0	0.0	0.0
149	1	0.07	0.00	0	0.0	0.0	0.0
150	1	0.07	0.00	0	0.0	0.0	0.0
151	1	0.06	0.00	0	0.0	0.0	0.0
152	1	0.04	0.00	0	0.0	0.0	0.0
153	1	0.02	0.00	0	0.0	0.0	0.0
154	1	0.06	0.00	0	0.0	0.0	0.0
155	1	0.05	0.00	0	0.0	0.0	0.0
156	1	0.04	0.00	0	0.0	0.0	0.0
157	1	0.04	0.00	0	0.0	0.0	0.0
158	1	0.03	0.00	0	0.0	0.0	0.0
159	1	0.03	0.00	0	0.0	0.0	0.0
160	1	0.03	0.00	0	0.0	0.0	0.0
161	1	0.03	0.00	0	0.0	0.0	0.0
162	1	0.04	0.00	0	0.0	0.0	0.0
163	1	0.04	0.00	0	0.0	0.0	0.0

=====

DATI: CASI DI CARICO

=====

CASO DESCRIZIONE & TIPOLOGIA
n.ro

1 c.d.c. 1 peso proprio [peso proprio]
2 c.d.c. 2: permanente [permanente]
3 c.d.c. 3: sovraccarico [sovraccarico]

=====

DATI : COMBINAZIONI

=====

COMB. DESCRIZIONE
n.ro

1 1*1.3 + 2*1.3 + 3*1.5
2 1*1 + 2*1 + 3*1
3 1*1 + 2*1 + 3*0.5
4 1*1 + 2*1 + 3*0.3

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SOMMATORIA TOTALE DEI CARICHI APPLICATI (PER OGNI CASO DI CARICO)

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CASO CARICO n.ro	FX (Kg)	FY (Kg)	Forizz (Kg)	FZ (=Fvert.) (Kg)
1	0.0	0.0	0.0	-176.1
2	0.0	0.0	0.0	0.0
3	-1000.0	0.0	1000.0	0.0

ALLEGATO B

CALCOLO STATICO MURO IN C.A.

INFORMAZIONI GENERALI

Comune	Comune di ancona
Provincia	Provincia di ancona
Oggetto	MURO DI SOSTEGNO A MENSOLA
Parte d'opera	
Normativa di riferimento	D.M. 17/01/2018
Analisi sismica	Nessuna

MATERIALI

Materiali															
N	Tipo	Descrizione	Sigla	Peso Specifico	Coeff. Dil. Termica	Modulo elastico		Rk	γ	ridFmk	n	ft	fc	τ R	N Act
				[N/m³]	[1/°C]	E	G	Rk		[%]		[N/mm²]	[N/mm²]	[N/mm²]	
1	CA	Cls C28/35-B450C	C28/35	25000	0.000010	32588	13578	35.0	1.50	85	15	1.32	3.40	0.38	Acciaio B450C
2	AcT	Acciaio B450C		B450C	78500	0.000010	210000	80769	450.0	1.15	0	1	0.00	0.00	

LEGENDA Materiali

N	Numero identificativo del materiale.
Tipo	Tipologia del materiale: [CA] = Calcestruzzo armato - [AcT] = Acciaio in tondini - [AcP] = Acciaio in profilati - [M] = Muratura - [AcA] = Acciaio armonico per trefoli - [Mlt] = Malta per tiranti - [PGab] = Pietrame per Gabbioni.
Sigla	Sigla del materiale.
Coeff. Dil. Termica	Coefficiente di dilatazione termica.
E	Modulo elastico normale.
G	Modulo elastico tangenziale.
Rk	Resistenza caratteristica del materiale. Il valore riportato è "Rck" per il calcestruzzo, "f _{yk} " per l'acciaio, "f _{mk} " per la muratura ed "f _k " nel caso di altro materiale.
γ	Coefficiente di sicurezza allo Stato Limite Ultimo del materiale. Il valore riportato è " γ_c " per il calcestruzzo, " γ_f " per l'acciaio, " γ_m " per la muratura e " γ_g " in caso di altro materiale.
ridFmk	Percentuale di riduzione di Rcfmk.
n	Coefficiente di omogeneizzazione.
ft	Il valore riportato e' la "Resistenza di calcolo a trazione" per il calcestruzzo armato, la "Resistenza caratteristica a trazione" per la muratura.
fc	Il valore riportato e' la "Resistenza a rottura per flessione" per il calcestruzzo armato, la "Resistenza caratteristica a compressione orizzontale" per la muratura.
τR	Il valore riportato e' la "Resistenza tangenziale di calcolo" per il calcestruzzo armato, la "Resistenza caratteristica a taglio in assenza di compressione - f _{vk0} " per la muratura.
N Act	Identificativo, nella tabella materiali, dell'acciaio utilizzato.

TERRENI

Terreni													
N	Descrizione	Tv	γ	γ_{saturo}	ϕ	Cu	C'	Ed	Costante di sottofondo			E _{cu}	A _{S-B}
			[N/m³]	[N/m³]	[°]	[N/mm²]	[N/mm²]	[N/mm²]	X	Y	Z	[N/mm²]	
1	Sabbia compatta (asciutta)	Medio Minimo	18000 18000	22000 22000	37 37	0.000 0.000	0.000 0.000	80 80	30 30	30 30	90 90	-	-

LEGENDA Terreni

N	Numero identificativo del terreno.
Descrizione	Descrizione del terreno.
Tv	Indica i valori minimi e medi dei parametri del terreno.
γ	Peso per unità di volume [N/m³].
γ_{saturo}	Peso per unità di volume saturo [N/m³].
ϕ	Angolo di attrito [°ssdc].
Cu	Coesione [N/mm²].
C'	Coesione Efficace [N/mm²].
Ed	Modulo edometrico [N/mm²].
Costante di sottofondo	Valori della costante di sottofondo del terreno nelle direzioni degli assi del riferimento globale X, Y, e Z.
E_{cu}	Modulo elastico in condizioni non drenate [N/mm²].
A_{S-B}	Parametro A si Skempton-Bjerrum per pressioni interstiziali.

CONDIZIONI DI CARICO

Condizioni di carico							
N	Condizioni Carico Utente			Tipologia Carico Accidentale			
	Descrizione	AgS	Alt	Descrizione	$\psi 0$	$\psi 1$	$\psi 2$

N	Condizioni Carico Utente			Condizioni di carico			
	Descrizione	AgS	Alt	Tipologia Carico Accidentale			
				Descrizione	ψ 0	ψ 1	ψ 2
1	Carico permanente	SI	NO	Carico permanente	1.0	1.0	1.0

LEGENDA Condizioni di carico

N	Numero identificativo della condizione di carico.
AgS	Indica se la condizione di carico considerata è Agente con il Sisma.
Alt	Indica se la condizione di carico è Alternata (cioè considerata due volte con segno opposto) o meno.
ψ 0	Coefficiente riduttivo dei carichi allo SLU e SLE (Carichi rari).
ψ 1	Coefficiente riduttivo dei carichi allo SLE (Carichi frequenti).
ψ 2	Coefficiente riduttivo dei carichi allo SLE (Carichi frequenti e quasi permanenti).

SLE: COMBINAZIONE DI AZIONI QUASI PERMANENTE - COEFFICIENTI

SLE: Combinazione di azioni Quasi permanente - Coefficienti	
CC 01	
COMB.	Carico permanente (Carico permanente)
01	1.00

LEGENDA SLE: Combinazione di azioni Quasi permanente - Coefficienti

COMB.	Numero identificativo della Combinazione di Carico.
CC	Condizione di carico considerata.
	CC 01= Carico permanente (Carico permanente)

SLE: COMBINAZIONE DI AZIONI FREQUENTE - COEFFICIENTI

SLE: Combinazione di azioni Frequente - Coefficienti	
CC 01	
COMB.	Carico permanente (Carico permanente)
01	1.00

LEGENDA SLE: Combinazione di azioni Frequente - Coefficienti

COMB.	Numero identificativo della Combinazione di Carico.
CC	Condizione di carico considerata.
	CC 01= Carico permanente (Carico permanente)

SLE: COMBINAZIONE DI AZIONI RARA - COEFFICIENTI

SLE: Combinazione di azioni Rara - Coefficienti	
CC 01	
COMB.	Carico permanente (Carico permanente)
01	1.00

LEGENDA SLE: Combinazione di azioni Rara - Coefficienti

COMB.	Numero identificativo della Combinazione di Carico.
CC	Condizione di carico considerata.
	CC 01= Carico permanente (Carico permanente)

SLU: COMBINAZIONI DI CARICO IN ASSENZA DI SISMA - COEFFICIENTI

SLU: Combinazioni di carico in assenza di sisma - Coefficienti	
CC 01	
COMB.	Carico permanente (Carico permanente)
Approccio 1, Combinazione 2 - Verifica di stabilità globale (A2+M2+R2)	

SLU: Combinazioni di carico in assenza di sisma - Coefficienti

CC 01	
COMB.	Carico permanente (Carico permanente)
01	1
02	1
Approccio 2 - Rimanenti verifiche (A1+M1+R3)	
01	1.3
02	1

LEGENDA SLU: Combinazioni di carico in assenza di sisma - Coefficienti

COMB. Numero identificativo della Combinazione di Carico.

CC Condizione di carico considerata.

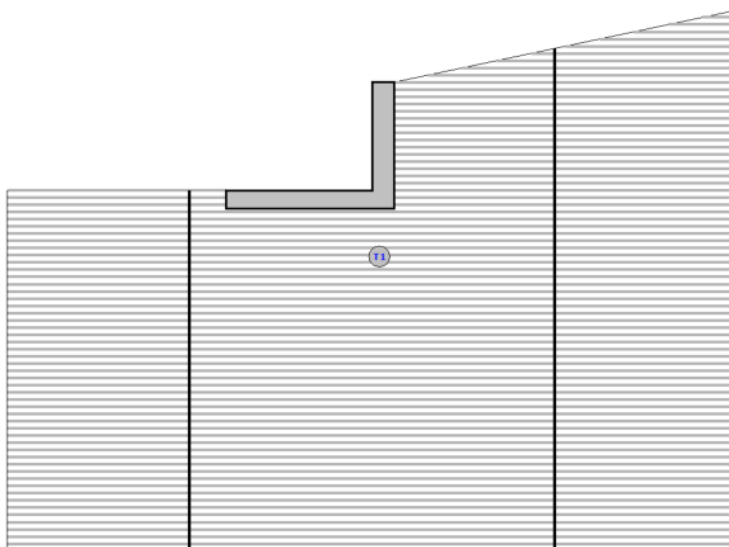
CC 01= Carico permanente (Carico permanente)

GEOMETRIA

Sezione...

Geometria

SEZIONE... - STRATI



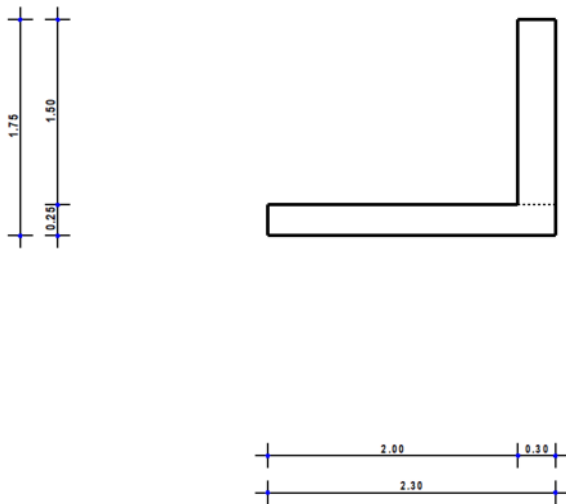
Strato	Descrizione	γ	γ_{sat}	ϕ	Cu	C'
T1	Sabbia compatta (asciutta)	18000	22000	37.0°	0.00	0.00

GEOMETRIA

Sezione...

Geometria

SEZIONE... - SEZIONE



CARATTERISTICHE MECCANICHE DEGLI STRATI

Caratteristiche meccaniche degli strati												
N	Caratt. Geotecnica	Addens. Strato	Var. Mod. Edom.	NSPT	IGU	Alfa	IRS	Res. Tang.	IGU	IRS	Kp	PrsMenar d
								[N/mm²]	[N/mm²]			[N/mm²]
Sezione...												
1	Sabbia media	Sciolto	Nulla	24	1.2		1.5	0.120	0.175		1.20	1.20

LEGENDA Caratteristiche meccaniche degli strati

N	Numero identificativo dello strato.
Caratt. Geotecnica	Caratterizzazione geotecnica per micropali.
Addens. Strato	Addensamento dello strato
Var. Mod. Edom.	Variazione del Modulo Edometrico.
NSPT	Numero di colpi dello Standard Penetration Test
Alfa	Coefficiente maggiorativo diametro perforazione per micropali.
Res. Tang.	Resistenza tangenziale tra zona iniettata e terreno per micropali.
Kp	Coefficiente di calcolo resistenza alla punta per micropali.
PrsMenard	Pressione limite terreno determinata col pressiometro Menard.

SPINTE SUL PARAMENTO ALLO SLU

SPINTE SUL PARAMENTO ALLO SLU - Approccio 2, Combinazione (A1+M1+R3)						
Stato limite	Sisma	Fx [N]	Fz [N]	Angolo [gradi]	PtApp [m]	
Sezione...						
SLU	NO	6,186	2,857	58	X: 0.30; Z: 0.50	
SLU	NO	4,759	2,198	58	X: 0.30; Z: 0.50	

LEGENDA Spinte sul paramento allo SLU

Stato limite	Tipo di Stato Limite.
Sisma	Sisma agente nella Combinazione.
Fx	Spinta Orizzontale [N].
Fz	Spinta Verticale [N].
Angolo	Angolo della retta delimitante il cuneo di Spinta [gradi].
PtApp	Punto di applicazione della Spinta [m].

SPINTE SUL CUNEO ALLO SLU

SPINTE SUL CUNEO ALLO SLU - Approccio 2, Combinazione (A1+M1+R3)						
Stato limite	Sisma	Fx [N]	Fz [N]	Angolo [gradi]	PtApp [m]	
Sezione...						
SLU	NO	8,420	3,889	58	X: 0.30; Z: 0.33	
SLU	NO	6,477	2,991	58	X: 0.30; Z: 0.33	

LEGENDA Spinte sul cuneo allo SLU

Stato limite	Tipo di Stato Limite.
Sisma	Sisma agente nella Combinazione.
Fx	Spinta Orizzontale [N].
Fz	Spinta Verticale [N].
Angolo	Angolo della retta delimitante il cuneo di Spinta [gradi].
PtApp	Punto di applicazione della Spinta [m].

SPINTE SUL PARAMENTO ALLO SLE

SPINTE SUL PARAMENTO ALLO SLE						
Combinazione	Sisma	Fx [N]	Fz [N]	Angolo [gradi]	PtApp [m]	
Sezione...						
RARA	NO	4,759	2,198	58	X: 0.30; Z: 0.50	
FREQUENTE	NO	4,759	2,198	58	X: 0.30; Z: 0.50	
QUASI PERMANENTE	NO	4,759	2,198	58	X: 0.30; Z: 0.50	

LEGENDA Spinte sul paramento allo SLE

Combinazione	Combinazione di Carico allo SLE.
Sisma	Sisma agente nella Combinazione.
Fx	Spinta Orizzontale [N].
Fz	Spinta Verticale [N].
Angolo	Angolo della retta delimitante il cuneo di Spinta [gradi].
PtApp	Punto di applicazione della Spinta [m].

SPINTE SUL CUNEO ALLO SLE

SPINTE SUL CUNEO ALLO SLE						
Combinazione	Sisma	Fx [N]	Fz [N]	Angolo [gradi]	PtApp [m]	
Sezione...						
RARA	NO	6,477	2,991	58	X: 0.30; Z: 0.33	
FREQUENTE	NO	6,477	2,991	58	X: 0.30; Z: 0.33	
QUASI PERMANENTE	NO	6,477	2,991	58	X: 0.30; Z: 0.33	

LEGENDA Spinte sul cuneo allo SLE

Combinazione	Combinazione di Carico allo SLE.
Sisma	Sisma agente nella Combinazione.
Fx	Spinta Orizzontale [N].
Fz	Spinta Verticale [N].
Angolo	Angolo della retta delimitante il cuneo di Spinta [gradi].
PtApp	Punto di applicazione della Spinta [m].

SOLLECITAZIONI SUL PARAMENTO

SOLLECITAZIONI SUL PARAMENTO						
Approccio	Stato limite	Sisma	N	My	Tx	
			[N]	[Nm]	[N]	
Sezione...						
Sez. calcolo n.1 - Dis: 0.04						
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	17074	-2413.00	-6187.00	
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	13132	-1856.00	-4759.00	
-	SLE: Combinazione RARA	NO	13132	-1856.00	-4759.00	
-	SLE: Combinazione FREQUENTE	NO	13132	-1856.00	-4759.00	
-	SLE: Combinazione QUASI PERMANENTE	NO	13132	-1856.00	-4759.00	
Sez. calcolo n.2 - Dis: 0.21						
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	14590	-1619.00	-4546.00	
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	11222	-1245.00	-3496.00	
-	SLE: Combinazione RARA	NO	11222	-1245.00	-3496.00	
-	SLE: Combinazione FREQUENTE	NO	11222	-1245.00	-3496.00	
-	SLE: Combinazione QUASI PERMANENTE	NO	11222	-1245.00	-3496.00	
Sez. calcolo n.3 - Dis: 0.39						
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	12223	-1017.00	-3157.00	
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	9401	-782.00	-2428.00	
-	SLE: Combinazione RARA	NO	9401	-782.00	-2428.00	
-	SLE: Combinazione FREQUENTE	NO	9401	-782.00	-2428.00	
-	SLE: Combinazione QUASI PERMANENTE	NO	9401	-782.00	-2428.00	
Sez. calcolo n.4 - Dis: 0.57						
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	10220	-555.00	-2557.00	
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	7860	-426.00	-1967.00	
-	SLE: Combinazione RARA	NO	7860	-426.00	-1967.00	
-	SLE: Combinazione FREQUENTE	NO	7860	-426.00	-1967.00	
-	SLE: Combinazione QUASI PERMANENTE	NO	7860	-426.00	-1967.00	
Sez. calcolo n.5 - Dis: 0.75						
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	8027	-284.00	-1547.00	
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	6174	-218.00	-1190.00	
-	SLE: Combinazione RARA	NO	6174	-218.00	-1190.00	
-	SLE: Combinazione FREQUENTE	NO	6174	-218.00	-1190.00	
-	SLE: Combinazione QUASI PERMANENTE	NO	6174	-218.00	-1190.00	
Sez. calcolo n.6 - Dis: 0.92						
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	5952	-119.00	-790.00	
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	4578	-91.00	-607.00	
-	SLE: Combinazione RARA	NO	4578	-91.00	-607.00	
-	SLE: Combinazione FREQUENTE	NO	4578	-91.00	-607.00	
-	SLE: Combinazione QUASI PERMANENTE	NO	4578	-91.00	-607.00	
Sez. calcolo n.7 - Dis: 1.10						
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	4095	-23.00	-506.00	
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	3149	-18.00	-388.00	
-	SLE: Combinazione RARA	NO	3149	-18.00	-388.00	
-	SLE: Combinazione FREQUENTE	NO	3149	-18.00	-388.00	
-	SLE: Combinazione QUASI PERMANENTE	NO	3149	-18.00	-388.00	
Sez. calcolo n.8 - Dis: 1.28						

SOLLECITAZIONI SUL PARAMENTO					
Approccio	Stato limite	Sisma	N [N]	My [Nm]	Tx [N]
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	2194	-2.00	-127.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	1687	-1.00	-97.00
-	SLE: Combinazione RARA	NO	1687	-1.00	-97.00
-	SLE: Combinazione FREQUENTE	NO	1687	-1.00	-97.00
-	SLE: Combinazione QUASI PERMANENTE	NO	1687	-1.00	-97.00
Sez. calcolo n.9 - Dis: 1.45					
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	410	0.00	0.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	315	0.00	0.00
-	SLE: Combinazione RARA	NO	315	0.00	0.00
-	SLE: Combinazione FREQUENTE	NO	315	0.00	0.00
-	SLE: Combinazione QUASI PERMANENTE	NO	315	0.00	0.00

LEGENDA Sollecitazioni sul Paramento

Approccio	Tipo di Approccio seguito.
Stato limite	Tipo di Stato Limite.
Sisma	Sisma agente nella Combinazione.
N	Sforzo Normale [N].
My	Vettore Momento ortogonale al piano dell'elemento [Nm].
Tx	Taglio orizzontale nel piano dell'elemento [N].

SOLLECITAZIONI SULLA FONDAZIONE

SOLLECITAZIONI SULLA FONDAZIONE					
Approccio	Stato limite	Sisma	N [N]	My [Nm]	Tx [N]
Sezione...					
Sez. calcolo n.10 - Dis: 0.00(Valle)					
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	7.00	312.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	5.00	240.00
-	SLE: Combinazione RARA	NO	0	5.00	240.00
-	SLE: Combinazione FREQUENTE	NO	0	5.00	240.00
-	SLE: Combinazione QUASI PERMANENTE	NO	0	5.00	240.00
Sez. calcolo n.11 - Dis: 0.24(Valle)					
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	255.00	1635.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	196.00	1257.00
-	SLE: Combinazione RARA	NO	0	196.00	1257.00
-	SLE: Combinazione FREQUENTE	NO	0	196.00	1257.00
-	SLE: Combinazione QUASI PERMANENTE	NO	0	196.00	1257.00
Sez. calcolo n.12 - Dis: 0.48(Valle)					
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	728.00	2183.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	560.00	1679.00
-	SLE: Combinazione RARA	NO	0	560.00	1679.00
-	SLE: Combinazione FREQUENTE	NO	0	560.00	1679.00
-	SLE: Combinazione QUASI PERMANENTE	NO	0	560.00	1679.00
Sez. calcolo n.13 - Dis: 0.72(Valle)					
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	1239.00	1957.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	953.00	1505.00
-	SLE: Combinazione RARA	NO	0	953.00	1505.00
-	SLE: Combinazione FREQUENTE	NO	0	953.00	1505.00
-	SLE: Combinazione QUASI PERMANENTE	NO	0	953.00	1505.00
Sez. calcolo n.14 - Dis: 0.96(Valle)					

SOLLECITAZIONI SULLA FONDAZIONE					
Approccio	Stato limite	Sisma	N [N]	My [Nm]	Tx [N]
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	1604.00	957.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	1233.00	736.00
-	SLE: Combinazione RARA	NO	0	1233.00	736.00
-	SLE: Combinazione FREQUENTE	NO	0	1233.00	736.00
-	SLE: Combinazione QUASI PERMANENTE	NO	0	1233.00	736.00
Sez. calcolo n.15 - Dis: 1.20(Valle)					
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	1636.00	-819.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	1258.00	-629.00
-	SLE: Combinazione RARA	NO	0	1258.00	-629.00
-	SLE: Combinazione FREQUENTE	NO	0	1258.00	-629.00
-	SLE: Combinazione QUASI PERMANENTE	NO	0	1258.00	-629.00
Sez. calcolo n.16 - Dis: 1.44(Valle)					
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	1150.00	-3368.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	884.00	-2590.00
-	SLE: Combinazione RARA	NO	0	884.00	-2590.00
-	SLE: Combinazione FREQUENTE	NO	0	884.00	-2590.00
-	SLE: Combinazione QUASI PERMANENTE	NO	0	884.00	-2590.00
Sez. calcolo n.17 - Dis: 1.68(Valle)					
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	-40.00	-6692.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	-30.00	-5147.00
-	SLE: Combinazione RARA	NO	0	-30.00	-5147.00
-	SLE: Combinazione FREQUENTE	NO	0	-30.00	-5147.00
-	SLE: Combinazione QUASI PERMANENTE	NO	0	-30.00	-5147.00
Sez. calcolo n.18 - Dis: 1.92(Valle)					
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	-2118.00	-10791.00
Approccio 2, Combinazione (A1+M1+R3)	SLU	NO	0	-1629.00	-8299.00
-	SLE: Combinazione RARA	NO	0	-1629.00	-8299.00
-	SLE: Combinazione FREQUENTE	NO	0	-1629.00	-8299.00
-	SLE: Combinazione QUASI PERMANENTE	NO	0	-1629.00	-8299.00

LEGENDA Sollecitazioni sulla fondazione

Approccio	Tipo di Approccio seguito.
Stato limite	Tipo di Stato Limite.
Sisma	Sisma agente nella Combinazione.
N	Sforzo Normale [N].
My	Vettore Momento ortogonale al piano dell'elemento [Nm].
Tx	Taglio orizzontale nel piano dell'elemento [N].

TENSIONI SUL TERRENO

TENSIONI SUL TERRENO - Approccio 2, Combinazione (A1+M1+R3)					
Stato Limite	Sisma	Pt[i] [m]	Pr[i] [N/mm²]	Pt[f] [m]	Pr[f] [N/mm²]
Sezione...					
SLU	NO	X: -2.00; Y: -0.25	0.000	X: 0.30; Y: -0.25	0.031
SLU	NO	X: -2.00; Y: -0.25	0.000	X: 0.30; Y: -0.25	0.024

LEGENDA Tensioni sul terreno

Stato limite	Stato limite di riferimento.
Sisma	Sisma agente nella Combinazione.
Pt[i]/Pt[f]	Coordinate del punto iniziale e finale del tratto di terreno di fondazione su cui sono esercitate le tensioni sul terreno [m].
Pr[i]/Pr[f]	Pressione iniziale e finale in corrispondenza dei relativi punti [N/mm²].

VERIFICHE DI STABILITA'

VERIFICHE DI STABILITA'

Bishop					Fellenius				
CS	FrzRblt	FrzRes	Centro	Raggio	CS	FrzRblt	FrzRes	Centro	Raggio
	[N]	[N]	[m]	[m]		[N]	[N]	[m]	[m]
Sezione...									
Verifica 1									
Approccio 1, Combinazione 2 Stato Limite Ultimo senza sisma									
1.77	55,213	97,787	X: 0.30; Y: 4.00	4.83	1.74	55,213	96,151	X: 0.30; Y: 4.00	4.83
3.73	193,262	721,649	X: 0.30; Y: 4.00	8.83	3.33	193,262	642,620	X: 0.30; Y: 4.00	8.83
1.49	46,221	68,935	X: -0.20; Y: 4.00	4.62	1.51	46,221	69,662	X: -0.20; Y: 4.00	4.62
3.72	177,063	658,883	X: -0.20; Y: 4.00	8.62	3.32	177,063	587,111	X: -0.20; Y: 4.00	8.62
1.29	35,785	46,060	X: -0.70; Y: 4.00	4.44	1.33	35,785	47,689	X: -0.70; Y: 4.00	4.44
3.75	162,199	607,800	X: -0.70; Y: 4.00	8.44	3.34	162,199	541,697	X: -0.70; Y: 4.00	8.44
1.30	32,076	41,602	X: -1.20; Y: 4.00	4.51	1.33	32,076	42,694	X: -1.20; Y: 4.00	4.51
3.93	154,547	606,858	X: -1.20; Y: 4.00	8.51	3.49	154,547	539,582	X: -1.20; Y: 4.00	8.51
1.51	31,046	46,750	X: -1.70; Y: 4.00	4.70	1.49	31,046	46,268	X: -1.70; Y: 4.00	4.70
4.18	151,786	634,855	X: -1.70; Y: 4.00	8.70	3.71	151,786	562,597	X: -1.70; Y: 4.00	8.70
1.92	29,744	57,247	X: -2.20; Y: 4.00	4.93	1.84	29,744	54,616	X: -2.20; Y: 4.00	4.93
4.50	149,775	673,305	X: -2.20; Y: 4.00	8.93	3.97	149,775	594,716	X: -2.20; Y: 4.00	8.93
2.54	28,996	73,701	X: -2.70; Y: 4.00	5.20	2.37	28,996	68,676	X: -2.70; Y: 4.00	5.20
4.91	146,903	722,001	X: -2.70; Y: 4.00	9.20	4.33	146,903	635,825	X: -2.70; Y: 4.00	9.20
3.59	26,613	95,519	X: -3.20; Y: 4.00	5.51	3.30	26,613	87,935	X: -3.20; Y: 4.00	5.51
5.29	147,900	782,448	X: -3.20; Y: 4.00	9.51	4.65	147,900	687,044	X: -3.20; Y: 4.00	9.51
4.76	25,957	123,673	X: -3.70; Y: 4.00	5.84	4.35	25,957	113,034	X: -3.70; Y: 4.00	5.84
5.83	145,877	850,511	X: -3.70; Y: 4.00	9.84	5.11	145,877	745,081	X: -3.70; Y: 4.00	9.84
6.43	24,473	157,385	X: -4.20; Y: 4.00	6.19	5.85	24,473	143,105	X: -4.20; Y: 4.00	6.19
6.47	143,295	927,453	X: -4.20; Y: 4.00	10.19	5.66	143,295	810,879	X: -4.20; Y: 4.00	10.19
1.76	57,252	100,768	X: 0.30; Y: 4.50	5.28	1.74	57,252	99,727	X: 0.30; Y: 4.50	5.28
3.66	201,695	738,420	X: 0.30; Y: 4.50	9.28	3.28	201,695	661,122	X: 0.30; Y: 4.50	9.28
1.52	47,386	71,997	X: -0.20; Y: 4.50	5.08	1.54	47,386	72,936	X: -0.20; Y: 4.50	5.08
3.65	185,891	678,375	X: -0.20; Y: 4.50	9.08	3.27	185,891	607,841	X: -0.20; Y: 4.50	9.08
1.33	37,782	50,124	X: -0.70; Y: 4.50	4.92	1.38	37,782	51,955	X: -0.70; Y: 4.50	4.92
3.65	173,029	631,352	X: -0.70; Y: 4.50	8.92	3.27	173,029	565,703	X: -0.70; Y: 4.50	8.92
1.33	33,796	44,891	X: -1.20; Y: 4.50	4.98	1.37	33,796	46,235	X: -1.20; Y: 4.50	4.98
3.81	165,238	629,318	X: -1.20; Y: 4.50	8.98	3.41	165,238	562,681	X: -1.20; Y: 4.50	8.98
1.49	32,768	48,856	X: -1.70; Y: 4.50	5.15	1.49	32,768	48,874	X: -1.70; Y: 4.50	5.15
4.02	162,454	653,720	X: -1.70; Y: 4.50	9.15	3.59	162,454	582,614	X: -1.70; Y: 4.50	9.15
1.84	31,524	58,032	X: -2.20; Y: 4.50	5.37	1.78	31,524	56,123	X: -2.20; Y: 4.50	5.37
4.38	156,804	687,010	X: -2.20; Y: 4.50	9.37	3.89	156,804	610,404	X: -2.20; Y: 4.50	9.37
2.39	30,226	72,355	X: -2.70; Y: 4.50	5.62	2.26	30,226	68,201	X: -2.70; Y: 4.50	5.62
4.74	154,503	731,597	X: -2.70; Y: 4.50	9.62	4.19	154,503	648,031	X: -2.70; Y: 4.50	9.62
3.15	29,424	92,564	X: -3.20; Y: 4.50	5.90	2.92	29,424	85,944	X: -3.20; Y: 4.50	5.90
5.09	154,764	787,476	X: -3.20; Y: 4.50	9.90	4.49	154,764	695,484	X: -3.20; Y: 4.50	9.90
4.34	27,212	118,186	X: -3.70; Y: 4.50	6.21	4.00	27,212	108,930	X: -3.70; Y: 4.50	6.21
5.60	152,083	851,102	X: -3.70; Y: 4.50	10.21	4.93	152,083	749,889	X: -3.70; Y: 4.50	10.21
5.66	26,544	150,200	X: -4.20; Y: 4.50	6.54	5.19	26,544	137,709	X: -4.20; Y: 4.50	6.54
6.17	149,801	923,525	X: -4.20; Y: 4.50	10.54	5.42	149,801	811,937	X: -4.20; Y: 4.50	10.54
1.72	60,030	103,543	X: 0.30; Y: 5.00	5.73	1.72	60,030	103,357	X: 0.30; Y: 5.00	5.73
3.59	210,569	756,074	X: 0.30; Y: 5.00	9.73	3.23	210,569	680,414	X: 0.30; Y: 5.00	9.73
1.54	49,225	75,846	X: -0.20; Y: 5.00	5.55	1.57	49,225	77,061	X: -0.20; Y: 5.00	5.55
3.56	196,649	700,115	X: -0.20; Y: 5.00	9.55	3.21	196,649	630,427	X: -0.20; Y: 5.00	9.55
1.37	39,500	54,175	X: -0.70; Y: 5.00	5.41	1.42	39,500	56,120	X: -0.70; Y: 5.00	5.41
3.60	181,597	653,175	X: -0.70; Y: 5.00	9.41	3.24	181,597	588,325	X: -0.70; Y: 5.00	9.41
1.36	35,146	47,952	X: -1.20; Y: 5.00	5.46	1.41	35,146	49,445	X: -1.20; Y: 5.00	5.46
3.75	173,484	649,955	X: -1.20; Y: 5.00	9.46	3.37	173,484	584,225	X: -1.20; Y: 5.00	9.46
1.50	33,966	50,886	X: -1.70; Y: 5.00	5.62	1.51	33,966	51,245	X: -1.70; Y: 5.00	5.62
3.96	169,597	671,765	X: -1.70; Y: 5.00	9.62	3.55	169,597	601,967	X: -1.70; Y: 5.00	9.62
1.79	32,725	58,725	X: -2.20; Y: 5.00	5.81	1.75	32,725	57,357	X: -2.20; Y: 5.00	5.81
4.22	166,652	703,205	X: -2.20; Y: 5.00	9.81	3.77	166,652	628,168	X: -2.20; Y: 5.00	9.81
2.26	31,825	72,041	X: -2.70; Y: 5.00	6.05	2.16	31,825	68,665	X: -2.70; Y: 5.00	6.05
4.56	163,355	744,305	X: -2.70; Y: 5.00	10.05	4.06	163,355	662,890	X: -2.70; Y: 5.00	10.05
2.95	30,568	90,134	X: -3.20; Y: 5.00	6.31	2.76	30,568	84,458	X: -3.20; Y: 5.00	6.31
4.94	161,013	794,668	X: -3.20; Y: 5.00	10.31	4.38	161,013	705,745	X: -3.20; Y: 5.00	10.31
3.84	29,754	114,109	X: -3.70; Y: 5.00	6.60	3.56	29,754	105,874	X: -3.70; Y: 5.00	6.60
5.38	158,670	854,119	X: -3.70; Y: 5.00	10.60	4.77	158,670	756,605	X: -3.70; Y: 5.00	10.60
5.18	27,694	143,559	X: -4.20; Y: 5.00	6.91	4.79	27,694	132,563	X: -4.20; Y: 5.00	6.91
5.92	155,822	922,396	X: -4.20; Y: 5.00	10.91	5.23	155,822	815,294	X: -4.20; Y: 5.00	10.91
1.74	61,252	106,568	X: 0.30; Y: 5.50	6.19	1.74	61,252	106,678	X: 0.30; Y: 5.50	6.19
3.51	221,386	776,143	X: 0.30; Y: 5.50	10.19	3.17	221,386	701,711	X: 0.30; Y: 5.50	10.19
1.56	50,947	79,680	X: -0.20; Y: 5.50	6.03	1.59	50,947	81,116	X: -0.20; Y: 5.50	6.03
3.51	205,132	720,456	X: -0.20; Y: 5.50	10.03	3.18	205,132	651,883	X: -0.20; Y: 5.50	10.03
1.41	41,152	58,157	X: -0.70; Y: 5.50	5.90	1.46	41,152	60,193	X: -0.70; Y: 5.50	5.90
3.57	189,272	675,041	X: -0.70; Y: 5.50	9.90	3.23	189,272	610,870	X: -0.70; Y: 5.50	9.90
1.40	36,826	51,430	X: -1.20; Y: 5.50	5.94	1.44	36,826	53,101	X: -1.20; Y: 5.50	5.94
3.71	180,877	670,775	X: -1.20; Y: 5.50	9.94	3.35	180,877	605,841	X: -1.20; Y: 5.50	9.94
1.51	35,494	53,458	X: -1.70; Y: 5.50	6.09	1.53	35,494	54,148	X: -1.70; Y: 5.50	6.09
3.89	177,330	690,145	X: -1.70; Y: 5.50	10.09	3.51	177,330	621,558	X: -1.70; Y: 5.50	10.09
1.76	34,271	60,207	X: -2.20; Y: 5.50	6.27	1.73	34,271	59,355	X: -2.20; Y: 5.50	6.27
4.15	173,359	718,847	X: -2.20; Y: 5.50	10.27	3.72	173,359	645,455	X: -2.20; Y: 5.50	10.27
2.18	32,949	71,800	X: -2.70; Y: 5.50	6.49	2.10	32,949	69,045	X: -2.70; Y: 5.50	6.49
4.44	170,348	756,643	X: -2.70; Y: 5.50	10.49	3.98	170,348	677,372	X: -2.70; Y: 5.50	10.49
2.77	32,022	88,742	X: -3.20; Y: 5.50	6.73	2.62	32,022	83,897	X: -3.20; Y: 5.50	6.73
4.81	167,050	803,545	X: -3.20; Y: 5.50	10.73	4.29	167,050	717,366	X: -3.20; Y: 5.50	10.73
3.59	30,821	110,598	X: -3.70; Y: 5.50	7.00	3.35	30,821	103,385	X: -3.70; Y: 5.50	7.00

VERIFICHE DI STABILITA'

Bishop					Fellenius				
CS	FrzRblt	FrzRes	Centro	Raggio	CS	FrzRblt	FrzRes	Centro	Raggio
	[N]	[N]	[m]	[m]		[N]	[N]	[m]	[m]
5.22	164,607	859,223	X: -3.70; Y: 5.50	11.00	4.65	164,607	765,073	X: -3.70; Y: 5.50	11.00
4.61	30,015	138,360	X: -4.20; Y: 5.50	7.30	4.28	30,015	128,465	X: -4.20; Y: 5.50	7.30
5.70	162,157	923,551	X: -4.20; Y: 5.50	11.30	5.06	162,157	820,412	X: -4.20; Y: 5.50	11.30
1.75	62,942	110,166	X: 0.30; Y: 6.00	6.66	1.76	62,942	110,581	X: 0.30; Y: 6.00	6.66
3.46	229,803	794,977	X: 0.30; Y: 6.00	10.66	3.14	229,803	721,979	X: 0.30; Y: 6.00	10.66
1.59	52,561	83,518	X: -0.20; Y: 6.00	6.50	1.62	52,561	85,129	X: -0.20; Y: 6.00	6.50
3.48	212,897	741,038	X: -0.20; Y: 6.00	10.50	3.16	212,897	673,424	X: -0.20; Y: 6.00	10.50
1.45	42,509	61,831	X: -0.70; Y: 6.00	6.38	1.50	42,509	63,903	X: -0.70; Y: 6.00	6.38
3.50	199,143	697,746	X: -0.70; Y: 6.00	10.38	3.18	199,143	634,200	X: -0.70; Y: 6.00	10.38
1.39	39,302	54,538	X: -1.20; Y: 6.00	6.43	1.44	39,302	56,615	X: -1.20; Y: 6.00	6.43
3.63	190,554	692,642	X: -1.20; Y: 6.00	10.43	3.30	190,554	628,418	X: -1.20; Y: 6.00	10.43
1.52	36,927	56,091	X: -1.70; Y: 6.00	6.56	1.54	36,927	57,047	X: -1.70; Y: 6.00	6.56
3.85	184,285	708,905	X: -1.70; Y: 6.00	10.56	3.48	184,285	641,406	X: -1.70; Y: 6.00	10.56
1.74	35,615	61,854	X: -2.20; Y: 6.00	6.73	1.72	35,615	61,422	X: -2.20; Y: 6.00	6.73
4.07	180,584	735,026	X: -2.20; Y: 6.00	10.73	3.67	180,584	663,129	X: -2.20; Y: 6.00	10.73
2.10	34,358	72,302	X: -2.70; Y: 6.00	6.93	2.04	34,358	70,121	X: -2.70; Y: 6.00	6.93
4.36	176,658	770,025	X: -2.70; Y: 6.00	10.93	3.92	176,658	692,704	X: -2.70; Y: 6.00	10.93
2.65	33,080	87,551	X: -3.20; Y: 6.00	7.16	2.52	33,080	83,395	X: -3.20; Y: 6.00	7.16
4.69	173,628	813,679	X: -3.20; Y: 6.00	11.16	4.20	173,628	729,932	X: -3.20; Y: 6.00	11.16
3.36	32,154	108,135	X: -3.70; Y: 6.00	7.42	3.17	32,154	101,816	X: -3.70; Y: 6.00	7.42
5.08	170,340	866,002	X: -3.70; Y: 6.00	11.42	4.55	170,340	774,881	X: -3.70; Y: 6.00	11.42
4.31	31,015	133,769	X: -4.20; Y: 6.00	7.70	4.03	31,015	124,983	X: -4.20; Y: 6.00	7.70
5.52	167,821	926,720	X: -4.20; Y: 6.00	11.70	4.93	167,821	827,213	X: -4.20; Y: 6.00	11.70
1.76	64,541	113,757	X: 0.30; Y: 6.50	7.13	1.77	64,541	114,481	X: 0.30; Y: 6.50	7.13
3.43	237,640	814,218	X: 0.30; Y: 6.50	11.13	3.12	237,640	742,470	X: 0.30; Y: 6.50	11.13
1.62	53,847	87,192	X: -0.20; Y: 6.50	6.99	1.65	53,847	88,896	X: -0.20; Y: 6.50	6.99
3.45	221,067	761,619	X: -0.20; Y: 6.50	10.99	3.14	221,067	694,976	X: -0.20; Y: 6.50	10.99
1.49	44,187	65,856	X: -0.70; Y: 6.50	6.87	1.54	44,187	68,018	X: -0.70; Y: 6.50	6.87
3.48	206,632	719,486	X: -0.70; Y: 6.50	10.87	3.18	206,632	656,596	X: -0.70; Y: 6.50	10.87
1.42	40,619	57,842	X: -1.20; Y: 6.50	6.91	1.48	40,619	59,998	X: -1.20; Y: 6.50	6.91
3.61	197,750	713,501	X: -1.20; Y: 6.50	10.91	3.29	197,750	650,021	X: -1.20; Y: 6.50	10.91
1.54	38,163	58,646	X: -1.70; Y: 6.50	7.04	1.57	38,163	59,800	X: -1.70; Y: 6.50	7.04
3.80	191,760	727,770	X: -1.70; Y: 6.50	11.04	3.45	191,760	661,307	X: -1.70; Y: 6.50	11.04
1.73	36,726	63,474	X: -2.20; Y: 6.50	7.20	1.73	36,726	63,378	X: -2.20; Y: 6.50	7.20
4.02	187,166	751,738	X: -2.20; Y: 6.50	11.20	3.64	187,166	681,200	X: -2.20; Y: 6.50	11.20
2.06	35,417	72,804	X: -2.70; Y: 6.50	7.39	2.01	35,417	71,084	X: -2.70; Y: 6.50	7.39
4.27	183,428	784,095	X: -2.70; Y: 6.50	11.39	3.86	183,428	708,532	X: -2.70; Y: 6.50	11.39
2.53	34,357	87,092	X: -3.20; Y: 6.50	7.60	2.43	34,357	83,557	X: -3.20; Y: 6.50	7.60
4.59	179,583	824,939	X: -3.20; Y: 6.50	11.60	4.14	179,583	743,417	X: -3.20; Y: 6.50	11.60
3.20	33,153	105,982	X: -3.70; Y: 6.50	7.85	3.03	33,153	100,415	X: -3.70; Y: 6.50	7.85
4.95	176,557	874,080	X: -3.70; Y: 6.50	11.85	4.45	176,557	785,655	X: -3.70; Y: 6.50	11.85
4.04	32,247	130,240	X: -4.20; Y: 6.50	8.11	3.80	32,247	122,418	X: -4.20; Y: 6.50	8.11
5.38	173,288	931,544	X: -4.20; Y: 6.50	12.11	4.82	173,288	835,325	X: -4.20; Y: 6.50	12.11
1.78	65,892	117,258	X: 0.30; Y: 7.00	7.61	1.79	65,892	118,191	X: 0.30; Y: 7.00	7.61
3.40	245,270	833,712	X: 0.30; Y: 7.00	11.61	3.11	245,270	763,105	X: 0.30; Y: 7.00	11.61
1.65	55,427	91,184	X: -0.20; Y: 7.00	7.47	1.68	55,427	93,015	X: -0.20; Y: 7.00	7.47
3.41	229,999	783,198	X: -0.20; Y: 7.00	11.47	3.12	229,999	717,339	X: -0.20; Y: 7.00	11.47
1.52	45,818	69,828	X: -0.70; Y: 7.00	7.37	1.57	45,818	72,069	X: -0.70; Y: 7.00	7.37
3.45	214,598	740,965	X: -0.70; Y: 7.00	11.37	3.16	214,598	678,781	X: -0.70; Y: 7.00	11.37
1.46	42,160	61,425	X: -1.20; Y: 7.00	7.40	1.51	42,160	63,692	X: -1.20; Y: 7.00	7.40
3.57	205,467	734,175	X: -1.20; Y: 7.00	11.40	3.27	205,467	671,461	X: -1.20; Y: 7.00	11.40
1.55	39,582	61,507	X: -1.70; Y: 7.00	7.52	1.59	39,582	62,862	X: -1.70; Y: 7.00	7.52
3.74	199,747	747,638	X: -1.70; Y: 7.00	11.52	3.41	199,747	682,060	X: -1.70; Y: 7.00	11.52
1.72	38,032	65,530	X: -2.20; Y: 7.00	7.67	1.73	38,032	65,724	X: -2.20; Y: 7.00	7.67
3.96	194,160	768,722	X: -2.20; Y: 7.00	11.67	3.60	194,160	699,445	X: -2.20; Y: 7.00	11.67
2.02	36,666	73,887	X: -2.70; Y: 7.00	7.85	1.98	36,666	72,603	X: -2.70; Y: 7.00	7.85
4.21	189,659	798,814	X: -2.70; Y: 7.00	11.85	3.82	189,659	724,861	X: -2.70; Y: 7.00	11.85
2.45	35,375	86,759	X: -3.20; Y: 7.00	8.05	2.37	35,375	83,746	X: -3.20; Y: 7.00	8.05
4.50	185,946	836,995	X: -3.20; Y: 7.00	12.05	4.07	185,946	757,479	X: -3.20; Y: 7.00	12.05
3.05	34,325	104,559	X: -3.70; Y: 7.00	8.28	2.90	34,325	99,665	X: -3.70; Y: 7.00	8.28
4.85	182,195	883,341	X: -3.70; Y: 7.00	12.28	4.38	182,195	797,395	X: -3.70; Y: 7.00	12.28
3.83	33,190	127,106	X: -4.20; Y: 7.00	8.53	3.62	33,190	120,108	X: -4.20; Y: 7.00	8.53
5.23	179,188	937,694	X: -4.20; Y: 7.00	12.53	4.71	179,188	844,412	X: -4.20; Y: 7.00	12.53
1.79	67,493	121,115	X: 0.30; Y: 7.50	8.08	1.81	67,493	122,261	X: 0.30; Y: 7.50	8.08
3.35	254,563	854,022	X: 0.30; Y: 7.50	12.08	3.08	254,563	784,526	X: 0.30; Y: 7.50	12.08
1.67	56,971	95,155	X: -0.20; Y: 7.50	7.96	1.70	56,971	97,098	X: -0.20; Y: 7.50	7.96
3.38	237,895	803,846	X: -0.20; Y: 7.50	11.96	3.11	237,895	738,879	X: -0.20; Y: 7.50	11.96
1.53	47,964	73,296	X: -0.70; Y: 7.50	7.86	1.58	47,964	75,819	X: -0.70; Y: 7.50	7.86
3.44	221,845	762,375	X: -0.70; Y: 7.50	11.86	3.16	221,845	700,804	X: -0.70; Y: 7.50	11.86
1.49	43,659	64,985	X: -1.20; Y: 7.50	7.89	1.54	43,659	67,345	X: -1.20; Y: 7.50	7.89
3.55	212,432	754,845	X: -1.20; Y: 7.50	11.89	3.26	212,432	692,806	X: -1.20; Y: 7.50	11.89
1.57	40,814	64,230	X: -1.70; Y: 7.50	8.00	1.61	40,814	65,731	X: -1.70; Y: 7.50	8.00
3.70	206,968	766,714	X: -1.70; Y: 7.50	12.00	3.39	206,968	702,067	X: -1.70; Y: 7.50	12.00
1.72	39,144	67,471	X: -2.20; Y: 7.50	8.14	1.74	39,144	67,925	X: -2.20; Y: 7.50	8.14
3.92	200,636	786,015	X: -2.20; Y: 7.50	12.14	3.58	200,636	717,899	X: -2.20; Y: 7.50	12.14
1.99	37,833	75,114	X: -2.70; Y: 7.50	8.31	1.96	37,833	74,204	X: -2.70; Y: 7.50	8.31
4.16	195,763	814,002	X: -2.70; Y: 7.50	12.31	3.79	195,763	741,526	X: -2.70; Y: 7.50	12.31
2.38	36,547	86,970	X: -3.20; Y: 7.50	8.50	2.31	36,547	84,441	X: -3.20; Y: 7.50	8.50
4.43	191,854	849,793	X: -3.20; Y: 7.50	12.50	4.02	191,854	772,122	X: -3.20; Y: 7.50	12.50
2.93	35,288	103,372	X: -3.70; Y: 7.50	8.72	2.81	35,288	99,055	X: -3.70; Y: 7.50	8.72
4.76	187,754	893,532	X: -3.70; Y: 7.50	12.72	4.31	187,754	809,844	X: -3.70; Y: 7.50	12.72
3.64	34,273	124,718	X: -4.20; Y: 7.50	8.96	3.46	34,273	118,449	X: -4.20; Y: 7.50	8.96
5.12	184,543	945,058	X: -4.20; Y: 7.50	12.96	4.63	184,543	854,494	X: -4.20; Y: 7.50	12.96

VERIFICHE DI STABILITA'

Bishop					Fellenius				
CS	FrzRbIt	FrzRes	Centro	Raggio	CS	FrzRbIt	FrzRes	Centro	Raggio
	[N]	[N]	[m]	[m]		[N]	[N]	[m]	[m]
1.81	68,810	124,788	X: 0.30; Y: 8.00	8.56	1.83	68,810	126,077	X: 0.30; Y: 8.00	8.56
3.34	261,976	873,807	X: 0.30; Y: 8.00	12.56	3.07	261,976	805,332	X: 0.30; Y: 8.00	12.56
1.70	58,372	98,987	X: -0.20; Y: 8.00	8.44	1.73	58,372	101,012	X: -0.20; Y: 8.00	8.44
3.36	245,268	824,505	X: -0.20; Y: 8.00	12.44	3.10	245,268	760,332	X: -0.20; Y: 8.00	12.44
1.56	49,573	77,325	X: -0.70; Y: 8.00	8.35	1.61	49,573	79,916	X: -0.70; Y: 8.00	8.35
3.40	230,335	784,085	X: -0.70; Y: 8.00	12.35	3.14	230,335	723,143	X: -0.70; Y: 8.00	12.35
1.52	45,009	68,423	X: -1.20; Y: 8.00	8.39	1.57	45,009	70,845	X: -1.20; Y: 8.00	8.39
3.52	220,720	775,888	X: -1.20; Y: 8.00	12.39	3.24	220,720	714,526	X: -1.20; Y: 8.00	12.39
1.56	42,895	67,014	X: -1.70; Y: 8.00	8.49	1.60	42,895	68,843	X: -1.70; Y: 8.00	8.49
3.68	213,624	785,873	X: -1.70; Y: 8.00	12.49	3.38	213,624	722,077	X: -1.70; Y: 8.00	12.49
1.73	40,436	69,778	X: -2.20; Y: 8.00	8.62	1.74	40,436	70,475	X: -2.20; Y: 8.00	8.62
3.87	207,752	804,050	X: -2.20; Y: 8.00	12.62	3.55	207,752	736,974	X: -2.20; Y: 8.00	12.62
1.97	38,882	76,408	X: -2.70; Y: 8.00	8.78	1.95	38,882	75,813	X: -2.70; Y: 8.00	8.78
4.10	202,345	829,482	X: -2.70; Y: 8.00	12.78	3.75	202,345	758,377	X: -2.70; Y: 8.00	12.78
2.33	37,504	87,271	X: -3.20; Y: 8.00	8.96	2.27	37,504	85,150	X: -3.20; Y: 8.00	8.96
4.37	197,591	863,166	X: -3.20; Y: 8.00	12.96	3.98	197,591	787,191	X: -3.20; Y: 8.00	12.96
2.82	36,371	102,717	X: -3.70; Y: 8.00	9.17	2.72	36,371	98,925	X: -3.70; Y: 8.00	9.17
4.67	193,766	904,434	X: -3.70; Y: 8.00	13.17	4.25	193,766	822,792	X: -3.70; Y: 8.00	13.17
3.49	35,186	122,652	X: -4.20; Y: 8.00	9.40	3.33	35,186	117,016	X: -4.20; Y: 8.00	9.40
5.02	189,803	953,413	X: -4.20; Y: 8.00	13.40	4.56	189,803	865,330	X: -4.20; Y: 8.00	13.40
1.83	70,414	128,815	X: 0.30; Y: 8.50	9.05	1.85	70,414	130,273	X: 0.30; Y: 8.50	9.05
3.31	269,792	893,559	X: 0.30; Y: 8.50	13.05	3.06	269,792	826,138	X: 0.30; Y: 8.50	13.05
1.72	59,960	103,038	X: -0.20; Y: 8.50	8.93	1.75	59,960	105,166	X: -0.20; Y: 8.50	8.93
3.35	252,448	845,112	X: -0.20; Y: 8.50	12.93	3.10	252,448	781,680	X: -0.20; Y: 8.50	12.93
1.59	51,152	81,312	X: -0.70; Y: 8.50	8.85	1.64	51,152	83,966	X: -0.70; Y: 8.50	8.85
3.39	237,438	805,215	X: -0.70; Y: 8.50	12.85	3.14	237,438	744,863	X: -0.70; Y: 8.50	12.85
1.55	46,449	72,074	X: -1.20; Y: 8.50	8.88	1.61	46,449	74,562	X: -1.20; Y: 8.50	8.88
3.50	227,547	796,356	X: -1.20; Y: 8.50	12.88	3.23	227,547	735,632	X: -1.20; Y: 8.50	12.88
1.58	44,238	70,063	X: -1.70; Y: 8.50	8.98	1.63	44,238	72,025	X: -1.70; Y: 8.50	8.98
3.65	220,609	804,960	X: -1.70; Y: 8.50	12.98	3.36	220,609	741,999	X: -1.70; Y: 8.50	12.98
1.73	41,683	72,140	X: -2.20; Y: 8.50	9.10	1.75	41,683	73,048	X: -2.20; Y: 8.50	9.10
3.83	214,526	821,592	X: -2.20; Y: 8.50	13.10	3.52	214,526	755,555	X: -2.20; Y: 8.50	13.10
1.95	40,036	77,978	X: -2.70; Y: 8.50	9.25	1.94	40,036	77,696	X: -2.70; Y: 8.50	9.25
4.06	208,330	845,321	X: -2.70; Y: 8.50	13.25	3.72	208,330	775,482	X: -2.70; Y: 8.50	13.25
2.28	38,597	87,985	X: -3.20; Y: 8.50	9.42	2.23	38,597	86,249	X: -3.20; Y: 8.50	9.42
4.30	203,783	876,933	X: -3.20; Y: 8.50	13.42	3.94	203,783	802,517	X: -3.20; Y: 8.50	13.42
2.74	37,311	102,247	X: -3.70; Y: 8.50	9.62	2.65	37,311	98,914	X: -3.70; Y: 8.50	9.62
4.60	199,216	916,040	X: -3.70; Y: 8.50	13.62	4.20	199,216	836,301	X: -3.70; Y: 8.50	13.62
3.35	36,062	120,973	X: -4.20; Y: 8.50	9.84	3.21	36,062	115,896	X: -4.20; Y: 8.50	9.84
4.92	195,487	962,545	X: -4.20; Y: 8.50	13.84	4.48	195,487	876,714	X: -4.20; Y: 8.50	13.84

Verifica 2

Approccio 1, Combinazione 2 Stato Limite Ultimo senza sisma

1.77	55,213	97,787	X: 0.30; Y: 4.00	4.83	1.74	55,213	96,151	X: 0.30; Y: 4.00	4.83
3.73	193,262	721,649	X: 0.30; Y: 4.00	8.83	3.33	193,262	642,620	X: 0.30; Y: 4.00	8.83
1.49	46,221	68,935	X: -0.20; Y: 4.00	4.62	1.51	46,221	69,662	X: -0.20; Y: 4.00	4.62
3.72	177,063	658,883	X: -0.20; Y: 4.00	8.62	3.32	177,063	587,111	X: -0.20; Y: 4.00	8.62
1.29	35,785	46,060	X: -0.70; Y: 4.00	4.44	1.33	35,785	47,689	X: -0.70; Y: 4.00	4.44
3.75	162,199	607,800	X: -0.70; Y: 4.00	8.44	3.34	162,199	541,697	X: -0.70; Y: 4.00	8.44
1.30	32,076	41,602	X: -1.20; Y: 4.00	4.51	1.33	32,076	42,694	X: -1.20; Y: 4.00	4.51
3.93	154,547	606,858	X: -1.20; Y: 4.00	8.51	3.49	154,547	539,582	X: -1.20; Y: 4.00	8.51
1.51	31,046	46,750	X: -1.70; Y: 4.00	4.70	1.49	31,046	46,268	X: -1.70; Y: 4.00	4.70
4.18	151,786	634,855	X: -1.70; Y: 4.00	8.70	3.71	151,786	562,597	X: -1.70; Y: 4.00	8.70
1.92	29,744	57,247	X: -2.20; Y: 4.00	4.93	1.84	29,744	54,616	X: -2.20; Y: 4.00	4.93
4.50	149,775	673,305	X: -2.20; Y: 4.00	8.93	3.97	149,775	594,716	X: -2.20; Y: 4.00	8.93
2.54	28,996	73,701	X: -2.70; Y: 4.00	5.20	2.37	28,996	68,676	X: -2.70; Y: 4.00	5.20
4.91	146,903	722,001	X: -2.70; Y: 4.00	9.20	4.33	146,903	635,825	X: -2.70; Y: 4.00	9.20
3.59	26,613	95,519	X: -3.20; Y: 4.00	5.51	3.30	26,613	87,935	X: -3.20; Y: 4.00	5.51
5.29	147,900	782,448	X: -3.20; Y: 4.00	9.51	4.65	147,900	687,044	X: -3.20; Y: 4.00	9.51
4.76	25,957	123,673	X: -3.70; Y: 4.00	5.84	4.35	25,957	113,034	X: -3.70; Y: 4.00	5.84
5.83	145,877	850,511	X: -3.70; Y: 4.00	9.84	5.11	145,877	745,081	X: -3.70; Y: 4.00	9.84
6.43	24,473	157,385	X: -4.20; Y: 4.00	6.19	5.85	24,473	143,105	X: -4.20; Y: 4.00	6.19
6.47	143,295	927,453	X: -4.20; Y: 4.00	10.19	5.66	143,295	810,879	X: -4.20; Y: 4.00	10.19
1.76	57,252	100,768	X: 0.30; Y: 4.50	5.28	1.74	57,252	99,727	X: 0.30; Y: 4.50	5.28
3.66	201,695	738,420	X: 0.30; Y: 4.50	9.28	3.28	201,695	661,122	X: 0.30; Y: 4.50	9.28
1.52	47,386	71,997	X: -0.20; Y: 4.50	5.08	1.54	47,386	72,936	X: -0.20; Y: 4.50	5.08
3.65	185,891	678,375	X: -0.20; Y: 4.50	9.08	3.27	185,891	607,841	X: -0.20; Y: 4.50	9.08
1.33	37,782	50,124	X: -0.70; Y: 4.50	4.92	1.38	37,782	51,955	X: -0.70; Y: 4.50	4.92
3.65	173,029	631,352	X: -0.70; Y: 4.50	8.92	3.27	173,029	565,703	X: -0.70; Y: 4.50	8.92
1.33	33,796	44,891	X: -1.20; Y: 4.50	4.98	1.37	33,796	46,235	X: -1.20; Y: 4.50	4.98
3.81	165,238	629,318	X: -1.20; Y: 4.50	8.98	3.41	165,238	562,681	X: -1.20; Y: 4.50	8.98
1.49	32,768	48,856	X: -1.70; Y: 4.50	5.15	1.49	32,768	48,874	X: -1.70; Y: 4.50	5.15
4.02	162,454	653,720	X: -1.70; Y: 4.50	9.15	3.59	162,454	582,614	X: -1.70; Y: 4.50	9.15
1.84	31,524	58,032	X: -2.20; Y: 4.50	5.37	1.78	31,524	56,123	X: -2.20; Y: 4.50	5.37
4.38	156,804	687,010	X: -2.20; Y: 4.50	9.37	3.89	156,804	610,404	X: -2.20; Y: 4.50	9.37
2.39	30,226	72,355	X: -2.70; Y: 4.50	5.62	2.26	30,226	68,201	X: -2.70; Y: 4.50	5.62
4.74	154,503	731,597	X: -2.70; Y: 4.50	9.62	4.19	154,503	648,031	X: -2.70; Y: 4.50	9.62
3.15	29,424	92,564	X: -3.20; Y: 4.50	5.90	2.92	29,424	85,944	X: -3.20; Y: 4.50	5.90
5.09	154,764	787,476	X: -3.20; Y: 4.50	9.90	4.49	154,764	695,484	X: -3.20; Y: 4.50	9.90
4.34	27,212	118,186	X: -3.70; Y: 4.50	6.21	4.00	27,212	108,930	X: -3.70; Y: 4.50	6.21
5.60	152,083	851,102	X: -3.70; Y: 4.50	10.21	4.93	152,083	749,889	X: -3.70; Y: 4.50	10.21
5.66	26,544	150,200	X: -4.20; Y: 4.50	6.54	5.19	26,544	137,709	X: -4.20; Y: 4.50	6.54
6.17	149,801	923,525	X: -4.20; Y: 4.50	10.54	5.42	149,801	811,937	X: -4.20; Y: 4.50	10.54
1.72	60,030	103,543	X: 0.30; Y: 5.00	5.73	1.72	60,030	103,357	X: 0.30; Y: 5.00	5.73

VERIFICHE DI STABILITA'

Bishop					Fellenius				
CS	FrzRblt	FrzRes	Centro	Raggio	CS	FrzRblt	FrzRes	Centro	Raggio
	[N]	[N]	[m]	[m]		[N]	[N]	[m]	[m]
3.59	210,569	756,074	X: 0.30; Y: 5.00	9.73	3.23	210,569	680,414	X: 0.30; Y: 5.00	9.73
1.54	49,225	75,846	X: -0.20; Y: 5.00	5.55	1.57	49,225	77,061	X: -0.20; Y: 5.00	5.55
3.56	196,649	700,115	X: -0.20; Y: 5.00	9.55	3.21	196,649	630,427	X: -0.20; Y: 5.00	9.55
1.37	39,500	54,175	X: -0.70; Y: 5.00	5.41	1.42	39,500	56,120	X: -0.70; Y: 5.00	5.41
3.60	181,597	653,175	X: -0.70; Y: 5.00	9.41	3.24	181,597	588,325	X: -0.70; Y: 5.00	9.41
1.36	35,146	47,952	X: -1.20; Y: 5.00	5.46	1.41	35,146	49,445	X: -1.20; Y: 5.00	5.46
3.75	173,484	649,955	X: -1.20; Y: 5.00	9.46	3.37	173,484	584,225	X: -1.20; Y: 5.00	9.46
1.50	33,966	50,886	X: -1.70; Y: 5.00	5.62	1.51	33,966	51,245	X: -1.70; Y: 5.00	5.62
3.96	169,597	671,765	X: -1.70; Y: 5.00	9.62	3.55	169,597	601,967	X: -1.70; Y: 5.00	9.62
1.79	32,725	58,725	X: -2.20; Y: 5.00	5.81	1.75	32,725	57,357	X: -2.20; Y: 5.00	5.81
4.22	166,652	703,205	X: -2.20; Y: 5.00	9.81	3.77	166,652	628,168	X: -2.20; Y: 5.00	9.81
2.26	31,825	72,041	X: -2.70; Y: 5.00	6.05	2.16	31,825	68,665	X: -2.70; Y: 5.00	6.05
4.56	163,355	744,305	X: -2.70; Y: 5.00	10.05	4.06	163,355	662,890	X: -2.70; Y: 5.00	10.05
2.95	30,568	90,134	X: -3.20; Y: 5.00	6.31	2.76	30,568	84,458	X: -3.20; Y: 5.00	6.31
4.94	161,013	794,668	X: -3.20; Y: 5.00	10.31	4.38	161,013	705,745	X: -3.20; Y: 5.00	10.31
3.84	29,754	114,109	X: -3.70; Y: 5.00	6.60	3.56	29,754	105,874	X: -3.70; Y: 5.00	6.60
5.38	158,670	854,119	X: -3.70; Y: 5.00	10.60	4.77	158,670	756,605	X: -3.70; Y: 5.00	10.60
5.18	27,694	143,559	X: -4.20; Y: 5.00	6.91	4.79	27,694	132,563	X: -4.20; Y: 5.00	6.91
5.92	155,822	922,396	X: -4.20; Y: 5.00	10.91	5.23	155,822	815,294	X: -4.20; Y: 5.00	10.91
1.74	61,252	106,568	X: 0.30; Y: 5.50	6.19	1.74	61,252	106,678	X: 0.30; Y: 5.50	6.19
3.51	221,386	776,143	X: 0.30; Y: 5.50	10.19	3.17	221,386	701,711	X: 0.30; Y: 5.50	10.19
1.56	50,947	79,680	X: -0.20; Y: 5.50	6.03	1.59	50,947	81,116	X: -0.20; Y: 5.50	6.03
3.51	205,132	720,456	X: -0.20; Y: 5.50	10.03	3.18	205,132	651,883	X: -0.20; Y: 5.50	10.03
1.41	41,152	58,157	X: -0.70; Y: 5.50	5.90	1.46	41,152	60,193	X: -0.70; Y: 5.50	5.90
3.57	189,272	675,041	X: -0.70; Y: 5.50	9.90	3.23	189,272	610,870	X: -0.70; Y: 5.50	9.90
1.40	36,826	51,430	X: -1.20; Y: 5.50	5.94	1.44	36,826	53,101	X: -1.20; Y: 5.50	5.94
3.71	180,877	670,775	X: -1.20; Y: 5.50	9.94	3.35	180,877	605,841	X: -1.20; Y: 5.50	9.94
1.51	35,494	53,458	X: -1.70; Y: 5.50	6.09	1.53	35,494	54,148	X: -1.70; Y: 5.50	6.09
3.89	177,330	690,145	X: -1.70; Y: 5.50	10.09	3.51	177,330	621,558	X: -1.70; Y: 5.50	10.09
1.76	34,271	60,207	X: -2.20; Y: 5.50	6.27	1.73	34,271	59,355	X: -2.20; Y: 5.50	6.27
4.15	173,359	718,847	X: -2.20; Y: 5.50	10.27	3.72	173,359	645,455	X: -2.20; Y: 5.50	10.27
2.18	32,949	71,800	X: -2.70; Y: 5.50	6.49	2.10	32,949	69,045	X: -2.70; Y: 5.50	6.49
4.44	170,348	756,643	X: -2.70; Y: 5.50	10.49	3.98	170,348	677,372	X: -2.70; Y: 5.50	10.49
2.77	32,022	88,742	X: -3.20; Y: 5.50	6.73	2.62	32,022	83,897	X: -3.20; Y: 5.50	6.73
4.81	167,050	803,545	X: -3.20; Y: 5.50	10.73	4.29	167,050	717,366	X: -3.20; Y: 5.50	10.73
3.59	30,821	110,598	X: -3.70; Y: 5.50	7.00	3.35	30,821	103,385	X: -3.70; Y: 5.50	7.00
5.22	164,607	859,223	X: -3.70; Y: 5.50	11.00	4.65	164,607	765,073	X: -3.70; Y: 5.50	11.00
4.61	30,015	138,360	X: -4.20; Y: 5.50	7.30	4.28	30,015	128,465	X: -4.20; Y: 5.50	7.30
5.70	162,157	923,551	X: -4.20; Y: 5.50	11.30	5.06	162,157	820,412	X: -4.20; Y: 5.50	11.30
1.75	62,942	110,166	X: 0.30; Y: 6.00	6.66	1.76	62,942	110,581	X: 0.30; Y: 6.00	6.66
3.46	229,803	794,977	X: 0.30; Y: 6.00	10.66	3.14	229,803	721,979	X: 0.30; Y: 6.00	10.66
1.59	52,561	83,518	X: -0.20; Y: 6.00	6.50	1.62	52,561	85,129	X: -0.20; Y: 6.00	6.50
3.48	212,897	741,038	X: -0.20; Y: 6.00	10.50	3.16	212,897	673,424	X: -0.20; Y: 6.00	10.50
1.45	42,509	61,831	X: -0.70; Y: 6.00	6.38	1.50	42,509	63,903	X: -0.70; Y: 6.00	6.38
3.50	199,143	697,746	X: -0.70; Y: 6.00	10.38	3.18	199,143	634,200	X: -0.70; Y: 6.00	10.38
1.39	39,302	54,538	X: -1.20; Y: 6.00	6.43	1.44	39,302	56,615	X: -1.20; Y: 6.00	6.43
3.63	190,554	692,642	X: -1.20; Y: 6.00	10.43	3.30	190,554	628,418	X: -1.20; Y: 6.00	10.43
1.52	36,927	56,091	X: -1.70; Y: 6.00	6.56	1.54	36,927	57,047	X: -1.70; Y: 6.00	6.56
3.85	184,285	708,905	X: -1.70; Y: 6.00	10.56	3.48	184,285	641,406	X: -1.70; Y: 6.00	10.56
1.74	35,615	61,854	X: -2.20; Y: 6.00	6.73	1.72	35,615	61,422	X: -2.20; Y: 6.00	6.73
4.07	180,584	735,026	X: -2.20; Y: 6.00	10.73	3.67	180,584	663,129	X: -2.20; Y: 6.00	10.73
2.10	34,358	72,302	X: -2.70; Y: 6.00	6.93	2.04	34,358	70,121	X: -2.70; Y: 6.00	6.93
4.36	176,658	770,025	X: -2.70; Y: 6.00	10.93	3.92	176,658	692,704	X: -2.70; Y: 6.00	10.93
2.65	33,080	87,551	X: -3.20; Y: 6.00	7.16	2.52	33,080	83,395	X: -3.20; Y: 6.00	7.16
4.69	173,628	813,679	X: -3.20; Y: 6.00	11.16	4.20	173,628	729,932	X: -3.20; Y: 6.00	11.16
3.36	32,154	108,135	X: -3.70; Y: 6.00	7.42	3.17	32,154	101,816	X: -3.70; Y: 6.00	7.42
5.08	170,340	866,002	X: -3.70; Y: 6.00	11.42	4.55	170,340	774,881	X: -3.70; Y: 6.00	11.42
4.31	31,015	133,769	X: -4.20; Y: 6.00	7.70	4.03	31,015	124,983	X: -4.20; Y: 6.00	7.70
5.52	167,821	926,720	X: -4.20; Y: 6.00	11.70	4.93	167,821	827,213	X: -4.20; Y: 6.00	11.70
1.76	64,541	113,757	X: 0.30; Y: 6.50	7.13	1.77	64,541	114,481	X: 0.30; Y: 6.50	7.13
3.43	237,640	814,218	X: 0.30; Y: 6.50	11.13	3.12	237,640	742,470	X: 0.30; Y: 6.50	11.13
1.62	53,847	87,192	X: -0.20; Y: 6.50	6.99	1.65	53,847	88,896	X: -0.20; Y: 6.50	6.99
3.45	221,067	761,619	X: -0.20; Y: 6.50	10.99	3.14	221,067	694,976	X: -0.20; Y: 6.50	10.99
1.49	44,187	65,856	X: -0.70; Y: 6.50	6.87	1.54	44,187	68,018	X: -0.70; Y: 6.50	6.87
3.48	206,632	719,486	X: -0.70; Y: 6.50	10.87	3.18	206,632	656,596	X: -0.70; Y: 6.50	10.87
1.42	40,619	57,842	X: -1.20; Y: 6.50	6.91	1.48	40,619	59,998	X: -1.20; Y: 6.50	6.91
3.61	197,750	713,501	X: -1.20; Y: 6.50	10.91	3.29	197,750	650,021	X: -1.20; Y: 6.50	10.91
1.54	38,163	58,646	X: -1.70; Y: 6.50	7.04	1.57	38,163	59,800	X: -1.70; Y: 6.50	7.04
3.80	191,760	727,770	X: -1.70; Y: 6.50	11.04	3.45	191,760	661,307	X: -1.70; Y: 6.50	11.04
1.73	36,726	63,474	X: -2.20; Y: 6.50	7.20	1.73	36,726	63,378	X: -2.20; Y: 6.50	7.20
4.02	187,166	751,738	X: -2.20; Y: 6.50	11.20	3.64	187,166	681,200	X: -2.20; Y: 6.50	11.20
2.06	35,417	72,804	X: -2.70; Y: 6.50	7.39	2.01	35,417	71,084	X: -2.70; Y: 6.50	7.39
4.27	183,428	784,095	X: -2.70; Y: 6.50	11.39	3.86	183,428	708,532	X: -2.70; Y: 6.50	11.39
2.53	34,357	87,092	X: -3.20; Y: 6.50	7.60	2.43	34,357	83,557	X: -3.20; Y: 6.50	7.60
4.59	179,583	824,939	X: -3.20; Y: 6.50	11.60	4.14	179,583	743,417	X: -3.20; Y: 6.50	11.60
3.20	33,153	105,982	X: -3.70; Y: 6.50	7.85	3.03	33,153	100,415	X: -3.70; Y: 6.50	7.85
4.95	176,557	874,080	X: -3.70; Y: 6.50	11.85	4.45	176,557	785,655	X: -3.70; Y: 6.50	11.85
4.04	32,247	130,240	X: -4.20; Y: 6.50	8.11	3.80	32,247	122,418	X: -4.20; Y: 6.50	8.11
5.38	173,288	931,544	X: -4.20; Y: 6.50	12.11	4.82	173,288	835,325	X: -4.20; Y: 6.50	12.11
1.78	65,892	117,258	X: 0.30; Y: 7.00	7.61	1.79	65,892	118,191	X: 0.30; Y: 7.00	7.61
3.40	245,270	833,712	X: 0.30; Y: 7.00	11.61	3.11	245,270	763,105	X: 0.30; Y: 7.00	11.61
1.65	55,427	91,184	X: -0.20; Y: 7.00	7.47	1.68	55,427	93,015	X: -0.20; Y: 7.00	7.47
3.41	229,999	783,198	X: -0.20; Y: 7.00	11.47	3.12	229,999	717,339	X: -0.20; Y: 7.00	11.47

VERIFICHE DI STABILITA'

Bishop					Fellenius				
CS	FrzRblt	FrzRes	Centro	Raggio	CS	FrzRblt	FrzRes	Centro	Raggio
	[N]	[N]	[m]	[m]		[N]	[N]	[m]	[m]
1.52	45,818	69,828	X: -0.70; Y: 7.00	7.37	1.57	45,818	72,069	X: -0.70; Y: 7.00	7.37
3.45	214,598	740,965	X: -0.70; Y: 7.00	11.37	3.16	214,598	678,781	X: -0.70; Y: 7.00	11.37
1.46	42,160	61,425	X: -1.20; Y: 7.00	7.40	1.51	42,160	63,692	X: -1.20; Y: 7.00	7.40
3.57	205,467	734,175	X: -1.20; Y: 7.00	11.40	3.27	205,467	671,461	X: -1.20; Y: 7.00	11.40
1.55	39,582	61,507	X: -1.70; Y: 7.00	7.52	1.59	39,582	62,862	X: -1.70; Y: 7.00	7.52
3.74	199,747	747,638	X: -1.70; Y: 7.00	11.52	3.41	199,747	682,060	X: -1.70; Y: 7.00	11.52
1.72	38,032	65,530	X: -2.20; Y: 7.00	7.67	1.73	38,032	65,724	X: -2.20; Y: 7.00	7.67
3.96	194,160	768,722	X: -2.20; Y: 7.00	11.67	3.60	194,160	699,445	X: -2.20; Y: 7.00	11.67
2.02	36,666	73,887	X: -2.70; Y: 7.00	7.85	1.98	36,666	72,603	X: -2.70; Y: 7.00	7.85
4.21	189,659	798,814	X: -2.70; Y: 7.00	11.85	3.82	189,659	724,861	X: -2.70; Y: 7.00	11.85
2.45	35,375	86,759	X: -3.20; Y: 7.00	8.05	2.37	35,375	83,746	X: -3.20; Y: 7.00	8.05
4.50	185,946	836,995	X: -3.20; Y: 7.00	12.05	4.07	185,946	757,479	X: -3.20; Y: 7.00	12.05
3.05	34,325	104,559	X: -3.70; Y: 7.00	8.28	2.90	34,325	99,665	X: -3.70; Y: 7.00	8.28
4.85	182,195	883,341	X: -3.70; Y: 7.00	12.28	4.38	182,195	797,395	X: -3.70; Y: 7.00	12.28
3.83	33,190	127,106	X: -4.20; Y: 7.00	8.53	3.62	33,190	120,108	X: -4.20; Y: 7.00	8.53
5.23	179,188	937,694	X: -4.20; Y: 7.00	12.53	4.71	179,188	844,412	X: -4.20; Y: 7.00	12.53
1.79	67,493	121,115	X: 0.30; Y: 7.50	8.08	1.81	67,493	122,261	X: 0.30; Y: 7.50	8.08
3.35	254,563	854,022	X: 0.30; Y: 7.50	12.08	3.08	254,563	784,526	X: 0.30; Y: 7.50	12.08
1.67	56,971	95,155	X: -0.20; Y: 7.50	7.96	1.70	56,971	97,098	X: -0.20; Y: 7.50	7.96
3.38	237,895	803,846	X: -0.20; Y: 7.50	11.96	3.11	237,895	738,879	X: -0.20; Y: 7.50	11.96
1.53	47,964	73,296	X: -0.70; Y: 7.50	7.86	1.58	47,964	75,819	X: -0.70; Y: 7.50	7.86
3.44	221,845	762,375	X: -0.70; Y: 7.50	11.86	3.16	221,845	700,804	X: -0.70; Y: 7.50	11.86
1.49	43,659	64,985	X: -1.20; Y: 7.50	7.89	1.54	43,659	67,345	X: -1.20; Y: 7.50	7.89
3.55	212,432	754,845	X: -1.20; Y: 7.50	11.89	3.26	212,432	692,806	X: -1.20; Y: 7.50	11.89
1.57	40,814	64,230	X: -1.70; Y: 7.50	8.00	1.61	40,814	65,731	X: -1.70; Y: 7.50	8.00
3.70	206,968	766,714	X: -1.70; Y: 7.50	12.00	3.39	206,968	702,067	X: -1.70; Y: 7.50	12.00
1.72	39,144	67,471	X: -2.20; Y: 7.50	8.14	1.74	39,144	67,925	X: -2.20; Y: 7.50	8.14
3.92	200,636	786,015	X: -2.20; Y: 7.50	12.14	3.58	200,636	717,899	X: -2.20; Y: 7.50	12.14
1.99	37,833	75,114	X: -2.70; Y: 7.50	8.31	1.96	37,833	74,204	X: -2.70; Y: 7.50	8.31
4.16	195,763	814,002	X: -2.70; Y: 7.50	12.31	3.79	195,763	741,526	X: -2.70; Y: 7.50	12.31
2.38	36,547	86,970	X: -3.20; Y: 7.50	8.50	2.31	36,547	84,441	X: -3.20; Y: 7.50	8.50
4.43	191,854	849,793	X: -3.20; Y: 7.50	12.50	4.02	191,854	772,122	X: -3.20; Y: 7.50	12.50
2.93	35,288	103,372	X: -3.70; Y: 7.50	8.72	2.81	35,288	99,055	X: -3.70; Y: 7.50	8.72
4.76	187,754	893,532	X: -3.70; Y: 7.50	12.72	4.31	187,754	809,844	X: -3.70; Y: 7.50	12.72
3.64	34,273	124,718	X: -4.20; Y: 7.50	8.96	3.46	34,273	118,449	X: -4.20; Y: 7.50	8.96
5.12	184,543	945,058	X: -4.20; Y: 7.50	12.96	4.63	184,543	854,494	X: -4.20; Y: 7.50	12.96
1.81	68,810	124,788	X: 0.30; Y: 8.00	8.56	1.83	68,810	126,077	X: 0.30; Y: 8.00	8.56
3.34	261,976	873,807	X: 0.30; Y: 8.00	12.56	3.07	261,976	805,332	X: 0.30; Y: 8.00	12.56
1.70	58,372	98,987	X: -0.20; Y: 8.00	8.44	1.73	58,372	101,012	X: -0.20; Y: 8.00	8.44
3.36	245,268	824,505	X: -0.20; Y: 8.00	12.44	3.10	245,268	760,332	X: -0.20; Y: 8.00	12.44
1.56	49,573	77,325	X: -0.70; Y: 8.00	8.35	1.61	49,573	79,916	X: -0.70; Y: 8.00	8.35
3.40	230,335	784,085	X: -0.70; Y: 8.00	12.35	3.14	230,335	723,143	X: -0.70; Y: 8.00	12.35
1.52	45,009	68,423	X: -1.20; Y: 8.00	8.39	1.57	45,009	70,845	X: -1.20; Y: 8.00	8.39
3.52	220,720	775,888	X: -1.20; Y: 8.00	12.39	3.24	220,720	714,526	X: -1.20; Y: 8.00	12.39
1.56	42,895	67,014	X: -1.70; Y: 8.00	8.49	1.60	42,895	68,843	X: -1.70; Y: 8.00	8.49
3.68	213,624	785,873	X: -1.70; Y: 8.00	12.49	3.38	213,624	722,077	X: -1.70; Y: 8.00	12.49
1.73	40,436	69,778	X: -2.20; Y: 8.00	8.62	1.74	40,436	70,475	X: -2.20; Y: 8.00	8.62
3.87	207,752	804,050	X: -2.20; Y: 8.00	12.62	3.55	207,752	736,974	X: -2.20; Y: 8.00	12.62
1.97	38,882	76,408	X: -2.70; Y: 8.00	8.78	1.95	38,882	75,813	X: -2.70; Y: 8.00	8.78
4.10	202,345	829,482	X: -2.70; Y: 8.00	12.78	3.75	202,345	758,377	X: -2.70; Y: 8.00	12.78
2.33	37,504	87,271	X: -3.20; Y: 8.00	8.96	2.27	37,504	85,150	X: -3.20; Y: 8.00	8.96
4.37	197,591	863,166	X: -3.20; Y: 8.00	12.96	3.98	197,591	787,191	X: -3.20; Y: 8.00	12.96
2.82	36,371	102,717	X: -3.70; Y: 8.00	9.17	2.72	36,371	98,925	X: -3.70; Y: 8.00	9.17
4.67	193,766	904,434	X: -3.70; Y: 8.00	13.17	4.25	193,766	822,792	X: -3.70; Y: 8.00	13.17
3.49	35,186	122,652	X: -4.20; Y: 8.00	9.40	3.33	35,186	117,016	X: -4.20; Y: 8.00	9.40
5.02	189,803	953,413	X: -4.20; Y: 8.00	13.40	4.56	189,803	865,330	X: -4.20; Y: 8.00	13.40
1.83	70,414	128,815	X: 0.30; Y: 8.50	9.05	1.85	70,414	130,273	X: 0.30; Y: 8.50	9.05
3.31	269,792	893,559	X: 0.30; Y: 8.50	13.05	3.06	269,792	826,138	X: 0.30; Y: 8.50	13.05
1.72	59,960	103,038	X: -0.20; Y: 8.50	8.93	1.75	59,960	105,166	X: -0.20; Y: 8.50	8.93
3.35	252,448	845,112	X: -0.20; Y: 8.50	12.93	3.10	252,448	781,680	X: -0.20; Y: 8.50	12.93
1.59	51,152	81,312	X: -0.70; Y: 8.50	8.85	1.64	51,152	83,966	X: -0.70; Y: 8.50	8.85
3.39	237,438	805,215	X: -0.70; Y: 8.50	12.85	3.14	237,438	744,863	X: -0.70; Y: 8.50	12.85
1.55	46,449	72,074	X: -1.20; Y: 8.50	8.88	1.61	46,449	74,562	X: -1.20; Y: 8.50	8.88
3.50	227,547	796,356	X: -1.20; Y: 8.50	12.88	3.23	227,547	735,632	X: -1.20; Y: 8.50	12.88
1.58	44,238	70,063	X: -1.70; Y: 8.50	8.98	1.63	44,238	72,025	X: -1.70; Y: 8.50	8.98
3.65	220,609	804,960	X: -1.70; Y: 8.50	12.98	3.36	220,609	741,999	X: -1.70; Y: 8.50	12.98
1.73	41,683	72,140	X: -2.20; Y: 8.50	9.10	1.75	41,683	73,048	X: -2.20; Y: 8.50	9.10
3.83	214,526	821,592	X: -2.20; Y: 8.50	13.10	3.52	214,526	755,555	X: -2.20; Y: 8.50	13.10
1.95	40,036	77,978	X: -2.70; Y: 8.50	9.25	1.94	40,036	77,696	X: -2.70; Y: 8.50	9.25
4.06	208,330	845,321	X: -2.70; Y: 8.50	13.25	3.72	208,330	775,482	X: -2.70; Y: 8.50	13.25
2.28	38,597	87,985	X: -3.20; Y: 8.50	9.42	2.23	38,597	86,249	X: -3.20; Y: 8.50	9.42
4.30	203,783	876,933	X: -3.20; Y: 8.50	13.42	3.94	203,783	802,517	X: -3.20; Y: 8.50	13.42
2.74	37,311	102,247	X: -3.70; Y: 8.50	9.62	2.65	37,311	98,914	X: -3.70; Y: 8.50	9.62
4.60	199,216	916,040	X: -3.70; Y: 8.50	13.62	4.20	199,216	836,301	X: -3.70; Y: 8.50	13.62
3.35	36,062	120,973	X: -4.20; Y: 8.50	9.84	3.21	36,062	115,896	X: -4.20; Y: 8.50	9.84
4.92	195,487	962,545	X: -4.20; Y: 8.50	13.84	4.48	195,487	876,714	X: -4.20; Y: 8.50	13.84

LEGENDA Verifiche di stabilita'

Approccio
Stato limite
Sisma
CS
FrzRblt

Tipo di Approccio seguito.
 Tipo di Stato Limite.
 Sisma agente nella Combinazione.
 Coefficiente di sicurezza ([NS]=Non significativo se CS maggiore o uguale a 100).
 Forza Ribaltante [N].

VERIFICHE DI STABILITA'									
Bishop					Fellenius				
CS	FrzRblt	FrzRes	Centro	Raggio	CS	FrzRblt	FrzRes	Centro	Raggio
	[N]	[N]	[m]	[m]		[N]	[N]	[m]	[m]
FrzRes		Forza Resistente [N].							
Centro		Coordinate del centro della circonferenza che delinea la superficie di scorrimento [m].							
Raggio		Raggio della circonferenza che delinea la superficie di scorrimento [m].							

VERIFICHE A SCORRIMENTO

VERIFICHE A SCORRIMENTO - Approccio 2, Combinazione (A1+M1+R3)					
Stato limite	Sisma	CS	FrzP	FrzR	
			[N]	[N]	
Sezione...					
Verifica 1	SLU	NO	3.03	8,420	25,485
Verifica 2	SLU	NO	3.03	6,477	19,604

LEGENDA Verifiche a scorrimento

Stato limite	Tipo di Stato Limite.
Sisma	Sisma agente nella Combinazione.
CS	Coefficiente di sicurezza ([NS]=Non significativo se CS maggiore o uguale a 100).
FrzP	Forza di scorrimento di Progetto [N].
FrzR	Forza Resistente a scorrimento [N].

VERIFICHE A RIBALTAMENTO

VERIFICHE A RIBALTAMENTO - Approccio 2, Combinazione (A1+M1+R3)					
Stato limite	Sisma	CS	Mrblt	Mstbl	
			[Nm]	[Nm]	
Sezione...					
Verifica 1	SLU	NO	10.93	4,922	53,808
Verifica 2	SLU	NO	10.93	3,786	41,390

LEGENDA Verifiche a ribaltamento

Stato limite	Tipo di Stato Limite.
Sisma	Sisma agente nella Combinazione.
CS	Coefficiente di sicurezza ([NS]=Non significativo se CS maggiore o uguale a 100).
Mrblt	Momento ribaltante di Progetto [Nm].
Mstbl	Momento Stabilizzante [Nm].

VERIFICHE A CARICO LIMITE

VERIFICHE A CARICO LIMITE - Approccio 2, Combinazione (A1+M1+R3)					
Stato limite	Sisma	CS	QMedP	QLim	
			[N/mm ²]	[N/mm ²]	
Sezione...					
Verifica 1	SLU	NO	24.04	0.02	0.39
Verifica 2	SLU	NO	31.26	0.01	0.39

LEGENDA Verifiche a Carico Limite

Stato limite	Tipo di Stato Limite.
Sisma	Sisma agente nella Combinazione.
CS	Coefficiente di sicurezza ([NS]=Non significativo se CS maggiore o uguale a 100).
QMedP	Tensione media di Progetto [N/mm ²].
QLim	Carico Limite [N/mm ²].

VERIFICHE A PRESSOFLESSIONE RETTA ALLO SLU

VERIFICHE A PRESSOFLESSIONE RETTA ALLO SLU							
CS _{Sup}	CS _{Inf}	Sollecitazioni				Af _{Sup}	Af _{Inf}
		N _{Sup}	My _{Sup}	N _{Inf}	My _{Inf}		
		[N]	[Nm]	[N]	[Nm]	[cm ²]	[cm ²]
Sezione...							
Paramento							
Sez. calcolo n.1 - Dis: 0.04							
-	28.04	0	0.00	17,074	-2,413.00	6.28	6.28
Sez. calcolo n.2 - Dis: 0.21							

VERIFICHE A PRESSOFLESSIONE RETTA ALLO SLU							
CS _{Sup}	CS _{Inf}	Sollecitazioni				Af _{Sup} [cm²]	Af _{Inf} [cm²]
		N _{Sup} [N]	My _{Sup} [Nm]	N _{Inf} [N]	My _{Inf} [Nm]		
-	41.60	0	0.00	14,590	-1,619.00	6.28	6.28
Sez. calcolo n.3 - Dis: 0.39	-	-	-	-	-	-	-
-	65.94	0	0.00	12,223	-1,017.00	6.28	6.28
Sez. calcolo n.4 - Dis: 0.57	-	-	-	-	-	-	-
-	NS	0	0.00	10,220	-555.00	6.28	6.28
Sez. calcolo n.5 - Dis: 0.75	-	-	-	-	-	-	-
-	NS	0	0.00	8,027	-284.00	6.28	6.28
Sez. calcolo n.6 - Dis: 0.92	-	-	-	-	-	-	-
-	NS	0	0.00	5,952	-119.00	6.28	6.28
Sez. calcolo n.7 - Dis: 1.10	-	-	-	-	-	-	-
-	NS	0	0.00	4,095	-23.00	6.28	6.28
Sez. calcolo n.8 - Dis: 1.28	-	-	-	-	-	-	-
-	NS	0	0.00	2,194	-2.00	6.28	6.28
Sez. calcolo n.9 - Dis: 1.45	-	-	-	-	-	-	-
-	-	315	0.00	315	0.00	6.28	6.28
Fondazione muro	-	-	-	-	-	-	-
Sez. calcolo n.10 - Dis: 0.00(Valle)	-	-	-	-	-	-	-
-	NS	0	7.00	0	0.00	5.09	5.09
Sez. calcolo n.11 - Dis: 0.24(Valle)	-	-	-	-	-	-	-
-	NS	0	255.00	0	0.00	5.09	5.09
Sez. calcolo n.12 - Dis: 0.48(Valle)	-	-	-	-	-	-	-
-	60.62	0	728.00	0	0.00	5.09	5.09
Sez. calcolo n.13 - Dis: 0.72(Valle)	-	-	-	-	-	-	-
-	35.62	0	1,239.00	0	0.00	5.09	5.09
Sez. calcolo n.14 - Dis: 0.96(Valle)	-	-	-	-	-	-	-
-	27.51	0	1,604.00	0	0.00	5.09	5.09
Sez. calcolo n.15 - Dis: 1.20(Valle)	-	-	-	-	-	-	-
-	26.97	0	1,636.00	0	0.00	5.09	5.09
Sez. calcolo n.16 - Dis: 1.44(Valle)	-	-	-	-	-	-	-
-	38.37	0	1,150.00	0	0.00	5.09	5.09
Sez. calcolo n.17 - Dis: 1.68(Valle)	-	-	-	-	-	-	-
-	NS	0	0.00	0	-40.00	5.09	5.09
Sez. calcolo n.18 - Dis: 1.92(Valle)	-	-	-	-	-	-	-
-	20.83	0	0.00	0	-2,118.00	5.09	5.09

LEGENDA Verifiche a pressoflessione retta allo SLU

CS	Coefficiente di sicurezza per l'armatura superiore ed inferiore ([NS]=Non significativo se CS maggiore o uguale a 100).
N	Sforzo normale per l'armatura superiore ed inferiore [N].
My	Vettore Momento intorno a Y per l'armatura superiore ed inferiore [Nm].
Af _{Sup}	Armatura Superiore Esecutiva [cm²].
Af _{Inf}	Armatura Inferiore Esecutiva [cm²].
NOTE	Per il paramento: sup=armatura a valle; inf=armatura a monte Per la fondazione: sup=armatura superiore; inf=armatura inferiore

VERIFICHE A PRESSOFLESSIONE RETTA ALLO SLE

VERIFICHE A PRESSOFLESSIONE RETTA ALLO SLE								
Trazione calcestruzzo			Compressione calcestruzzo			Trazione acciaio		
σ ct [N/mm²]	N [N]	My [N-m]	σ cc [N/mm²]	N [N]	My [N-m]	σ at [N/mm²]	N [N]	My [N-m]
Sezione...								
Paramento								
Sez. calcolo n.1 - Dis: 0.04								
AA= PCA	CA=FQR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm	CA=QPR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm						
0.067	13,132	-1,856	-0.150	13,132	-1,856	0.791	13,132	-1,856
Sez. calcolo n.2 - Dis: 0.21								
AA= PCA	CA=FQR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm	CA=QPR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm						
0.038	11,222	-1,245	-0.108	11,222	-1,245	0.417	11,222	-1,245
Sez. calcolo n.3 - Dis: 0.39								
AA= PCA	CA=FQR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm	CA=QPR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm						
0.016	9,401	-782	-0.075	9,401	-782	0.151	9,401	-782
Sez. calcolo n.4 - Dis: 0.57								
AA= PCA	CA=FQR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm	CA=QPR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm						
0.000	7,860	-426	-0.050	7,860	-426	0.000	0	0
Sez. calcolo n.5 - Dis: 0.75								
AA= PCA	CA=FQR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm	CA=QPR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm						
0.000	0	0	-0.032	6,174	-218	0.000	0	0
Sez. calcolo n.6 - Dis: 0.92								
AA= PCA	CA=FQR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm	CA=QPR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm						
0.000	0	0	-0.020	4,578	-91	0.000	0	0
Sez. calcolo n.7 - Dis: 1.10								
AA= PCA	CA=FQR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm	CA=QPR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm						
0.000	0	0	-0.011	3,149	-18	0.000	0	0
Sez. calcolo n.8 - Dis: 1.28								
AA= PCA	CA=FQR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm	CA=QPR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm						
0.000	0	0	-0.005	1,687	-1	0.000	0	0
Sez. calcolo n.9 - Dis: 1.45								
AA= PCA	CA=FQR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm	CA=QPR ε sm=0.00000 Ae=0.0 cm² sm=0 mm wk=0.00 mm						
0.000	0	0	0.000	0	0	0.000	0	0

Trazione calcestruzzo			Compressione calcestruzzo			Trazione acciaio		
σ_{ct} [N/mm ²]	N	My	σ_{cc} [N/mm ²]	N	My	σ_{at} [N/mm ²]	N	My
	[N]	[N·m]		[N]	[N·m]		[N]	[N·m]
Fondazione muro								
Sez. calcolo n.10 - Dis: 0.00(Valle)								
AA= PCA	CA=FQR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²	sm=0 mm	wk=0.00 mm	CA=QPR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²
0.000	0	5	0.000	0	5	0.005	0	5
Sez. calcolo n.11 - Dis: 0.24(Valle)								
AA= PCA	CA=FQR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²	sm=0 mm	wk=0.00 mm	CA=QPR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²
0.017	0	196	-0.017	0	196	0.210	0	196
Sez. calcolo n.12 - Dis: 0.48(Valle)								
AA= PCA	CA=FQR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²	sm=0 mm	wk=0.00 mm	CA=QPR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²
0.048	0	560	-0.048	0	560	0.600	0	560
Sez. calcolo n.13 - Dis: 0.72(Valle)								
AA= PCA	CA=FQR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²	sm=0 mm	wk=0.00 mm	CA=QPR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²
0.081	0	953	-0.081	0	953	1.021	0	953
Sez. calcolo n.14 - Dis: 0.96(Valle)								
AA= PCA	CA=FQR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²	sm=0 mm	wk=0.00 mm	CA=QPR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²
0.105	0	1,233	-0.105	0	1,233	1.321	0	1,233
Sez. calcolo n.15 - Dis: 1.20(Valle)								
AA= PCA	CA=FQR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²	sm=0 mm	wk=0.00 mm	CA=QPR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²
0.107	0	1,258	-0.107	0	1,258	1.347	0	1,258
Sez. calcolo n.16 - Dis: 1.44(Valle)								
AA= PCA	CA=FQR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²	sm=0 mm	wk=0.00 mm	CA=QPR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²
0.075	0	884	-0.075	0	884	0.947	0	884
Sez. calcolo n.17 - Dis: 1.68(Valle)								
AA= PCA	CA=FQR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²	sm=0 mm	wk=0.00 mm	CA=QPR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²
0.003	0	-30	-0.003	0	-30	0.032	0	-30
Sez. calcolo n.18 - Dis: 1.92(Valle)								
AA= PCA	CA=FQR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²	sm=0 mm	wk=0.00 mm	CA=QPR	$\varepsilon_{sm}=0.00000$	Ae=0.0 cm ²
0.138	0	-1,629	-0.138	0	-1,629	1.745	0	-1,629

AA	Identificativo dell'aggressività dell'ambiente: [PCA] = Poco aggressivo - [MDA] = Moderatamente aggressivo - [MLA] = Molto aggressivo.
CA	Identificativo della Combinazione di Azione: [QPR] = Quasi Permanente - [FQR] = Frequente - [RAR] = Rara.
ε sm	Deformazione media nel calcestruzzo.
Ae	Area efficace del calcestruzzo teso.
sm	Distanza media tra le fessure.
wk	Apertura massima delle fessure.
σ ct, N, My	Valori, rispettivamente della tensione massima di trazione nel calcestruzzo e delle componenti della sollecitazione agenti che l'hanno generata, riferite all'asse baricentrico della sezione trasversale(N) ed al sistema baricentrico x, y della sezione trasversale.
σ cc, N, My	Valori, rispettivamente della tensione massima di compressione nel calcestruzzo e delle componenti della sollecitazione agenti che l'hanno generata, riferite all'asse baricentrico della sezione trasversale(N) ed al sistema baricentrico x, y della sezione trasversale.
σ at, N, My	Valori, rispettivamente della tensione massima di trazione nell'acciaio e delle componenti della sollecitazione agenti che l'hanno generata, riferite all'asse baricentrico della sezione trasversale(N) ed al sistema baricentrico x, y della sezione trasversale.

VERIFICHE A TAGLIO PER PRESSOFLESSIONE RETTA ALLO SLU															
CS+	CS-	Tx+	Tx-	Vcc+	Vcc-	Vwd+	Vwd-	Nd+	Nd-	Vwp+	Vwp-	ctgθ+	ctgθ	AfTe+	AfTe-
		[N]	[N]	[N]	[N]	[N]	[N]	[N]	[N]	[N]	[N]			[cm²/cm]	[cm²/cm]
Sezione...															
Paramento															
Sez. calcolo n.1 - Dis: 0.04															
-	21.27	0	-6,187	129,273	131,578	0	0	0	17,074	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.2 - Dis: 0.21															
-	28.87	0	-4,546	129,273	131,242	0	0	0	14,590	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.3 - Dis: 0.39															
-	41.47	0	-3,157	129,273	130,923	0	0	0	12,223	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.4 - Dis: 0.57															
-	51.10	0	-2,557	129,273	130,652	0	0	0	10,220	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.5 - Dis: 0.75															
-	84.26	0	-1,547	129,273	130,356	0	0	0	8,027	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.6 - Dis: 0.92															
-	NS	0	-790	129,273	130,076	0	0	0	5,952	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.7 - Dis: 1.10															
-	NS	0	-506	129,273	129,825	0	0	0	4,095	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.8 - Dis: 1.28															
-	NS	0	-127	129,273	129,569	0	0	0	2,194	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.9 - Dis: 1.45															
-	-	0	0	129,273	129,273	0	0	0	0	0	0	0.00	0.00	0.0000	0.0000
Fondazione muro															
Sez. calcolo n.10 - Dis: 0.00(Valle)															
NS	-	312	0	113,311	113,311	0	0	0	0	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.11 - Dis: 0.24(Valle)															
69.30	-	1,635	0	113,311	113,311	0	0	0	0	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.12 - Dis: 0.48(Valle)															
51.91	-	2,183	0	113,311	113,311	0	0	0	0	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.13 - Dis: 0.72(Valle)															
57.90	-	1,957	0	113,311	113,311	0	0	0	0	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.14 - Dis: 0.96(Valle)															

VERIFICHE A TAGLIO PER PRESSOFLESSIONE RETTA ALLO SLU															
CS+	CS-	Tx+	Tx-	Vcc+	Vcc-	Vwd+	Vwd-	Nd+	Nd-	Vwp+	Vwp-	ctg⊕+	ctg⊖	AfTe+	AfTe-
		[N]	[N]	[N]	[N]	[N]	[N]	[N]	[N]	[N]	[N]			[cm²/cm]	[cm²/cm]
NS	-	957	0	113,311	113,311	0	0	0	0	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.15 - Dis: 1.20(Valle)															
-	NS	0	-819	113,311	113,311	0	0	0	0	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.16 - Dis: 1.44(Valle)															
-	33.64	0	-3,368	113,311	113,311	0	0	0	0	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.17 - Dis: 1.68(Valle)															
-	16.93	0	-6,692	113,311	113,311	0	0	0	0	0	0	0.00	0.00	0.0000	0.0000
Sez. calcolo n.18 - Dis: 1.92(Valle)															
-	10.50	0	-10,791	113,311	113,311	0	0	0	0	0	0	0.00	0.00	0.0000	0.0000

LEGENDA Verifiche a taglio per pressoflessione retta allo SLU

CS+, CS-

Coefficienti di sicurezza relativi alle sollecitazioni "Tx+" e "Tx-" : [NS] = Non Significativo - Per valori di CS maggiori o uguali a 100.

Tx+, Tx-

Valori massimo e minimo della sollecitazione di taglio.

Vcc+, Vcc-

Valori massimo e minimo del taglio ultimo, per conglomerato compresso.

Vwd+, Vwd-

Contributi dell'acciaio al taglio ultimo dovuto alle staffe, relativi alle sollecitazioni "Tx+" e "Tx-".

Nd+, Nd-

Sforzo normale.

Vwp+, Vwp-

Contributo acciaio al Taglio ultimo dovuto ai ferri piegati, relativi alle sollecitazioni "Tx+" e "Tx-".

ctg⊕+, ctg⊖

ctg(⊖) utilizzato nel calcolo di Vcc, Vwd e Vwp.

AfTe+, AfTe-

Aree di ferro per il taglio in un centimetro, relativi alle sollecitazioni "Tx+" e "Tx-".